

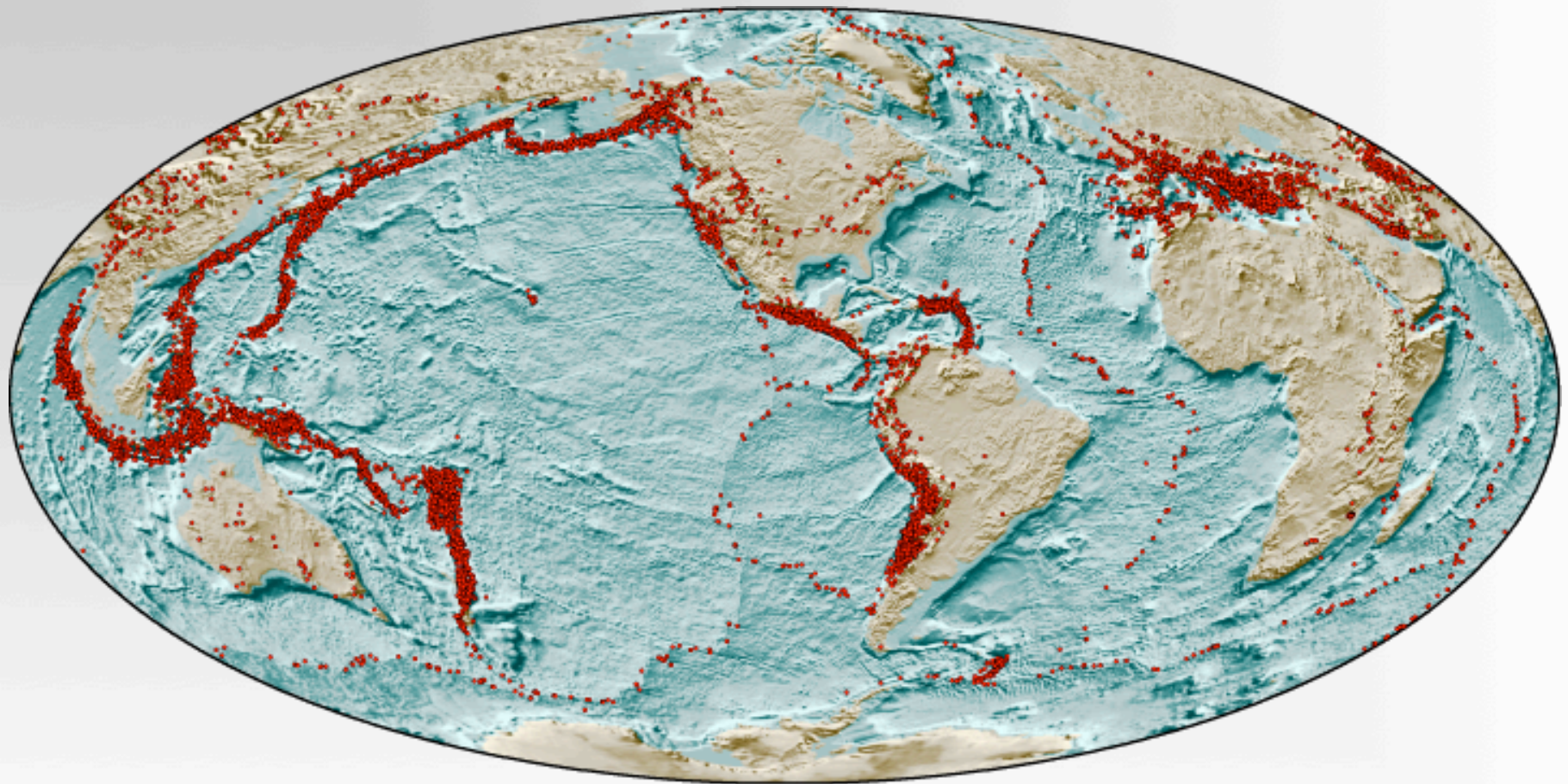
Rheology of the brittle-plastic transition

Role of fabric and phyllosilicates



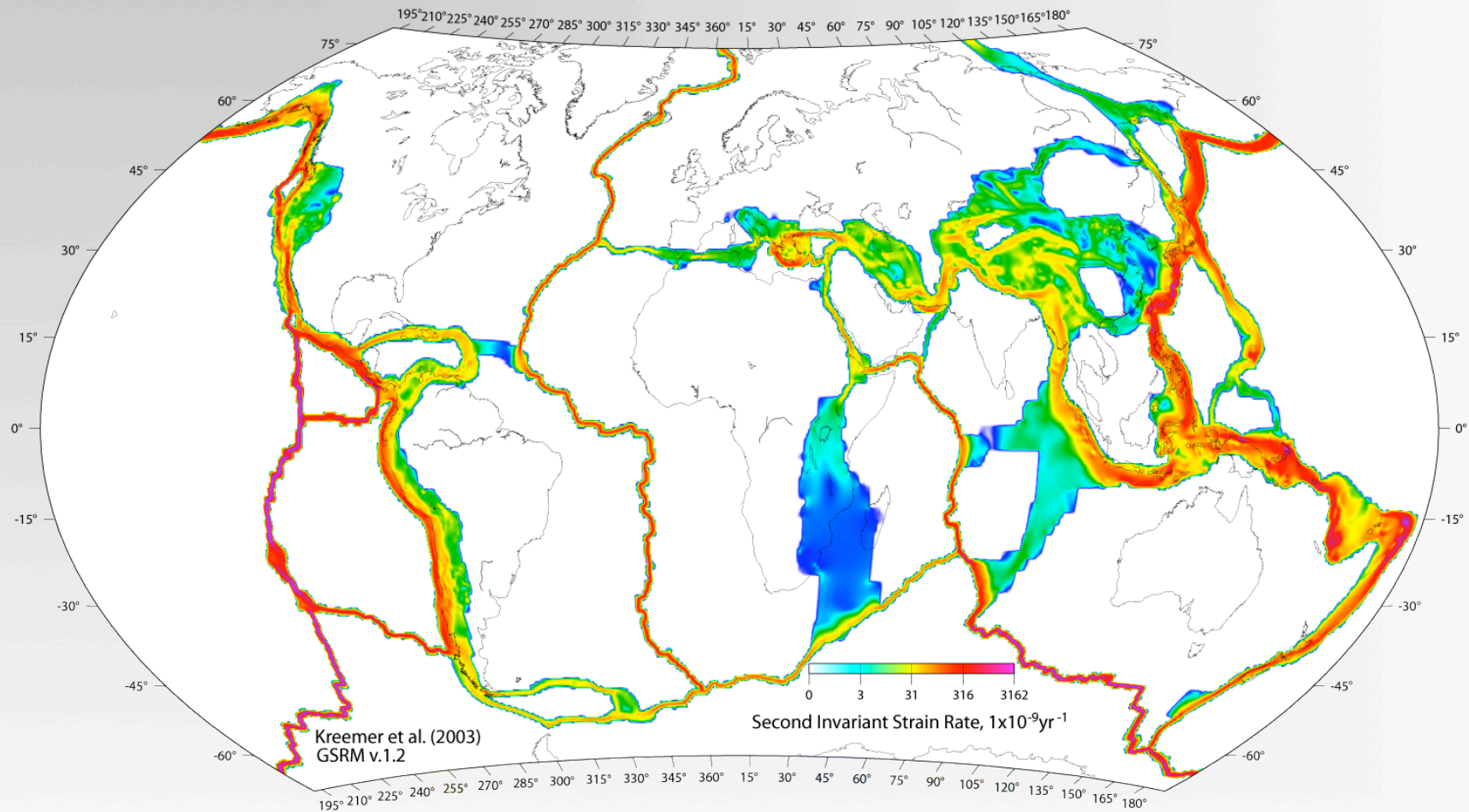
Laurent G.J. Montési
University of Maryland

Global Seismicity



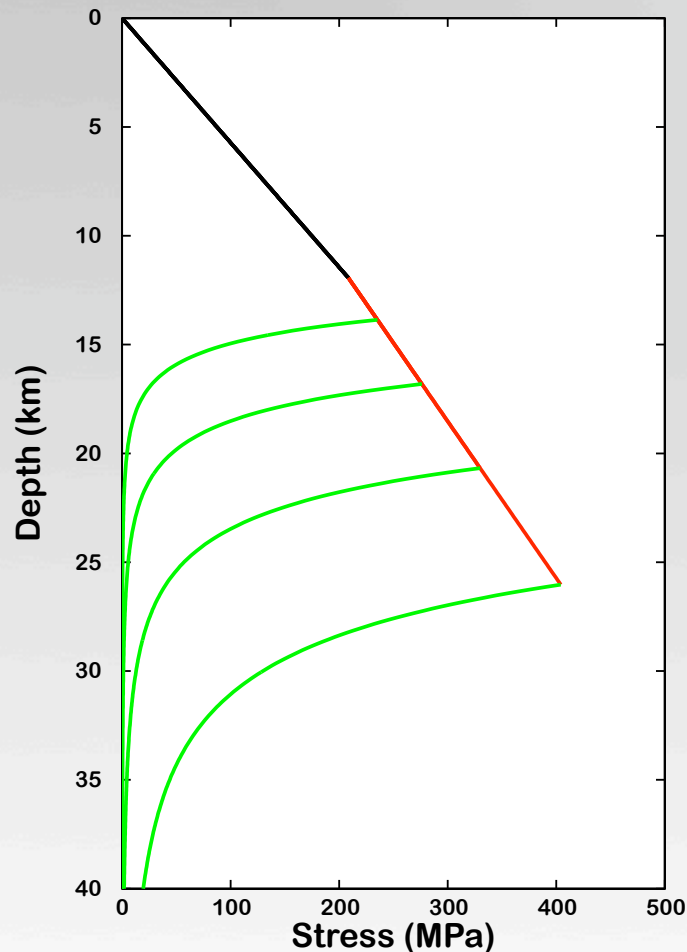
IRIS catalogue, $M > 2.0$, 01-01-2006 to 01-10-2006

World Strain Rate Map



Kremer et al., 2000, 2003

Brittle-Plastic transition



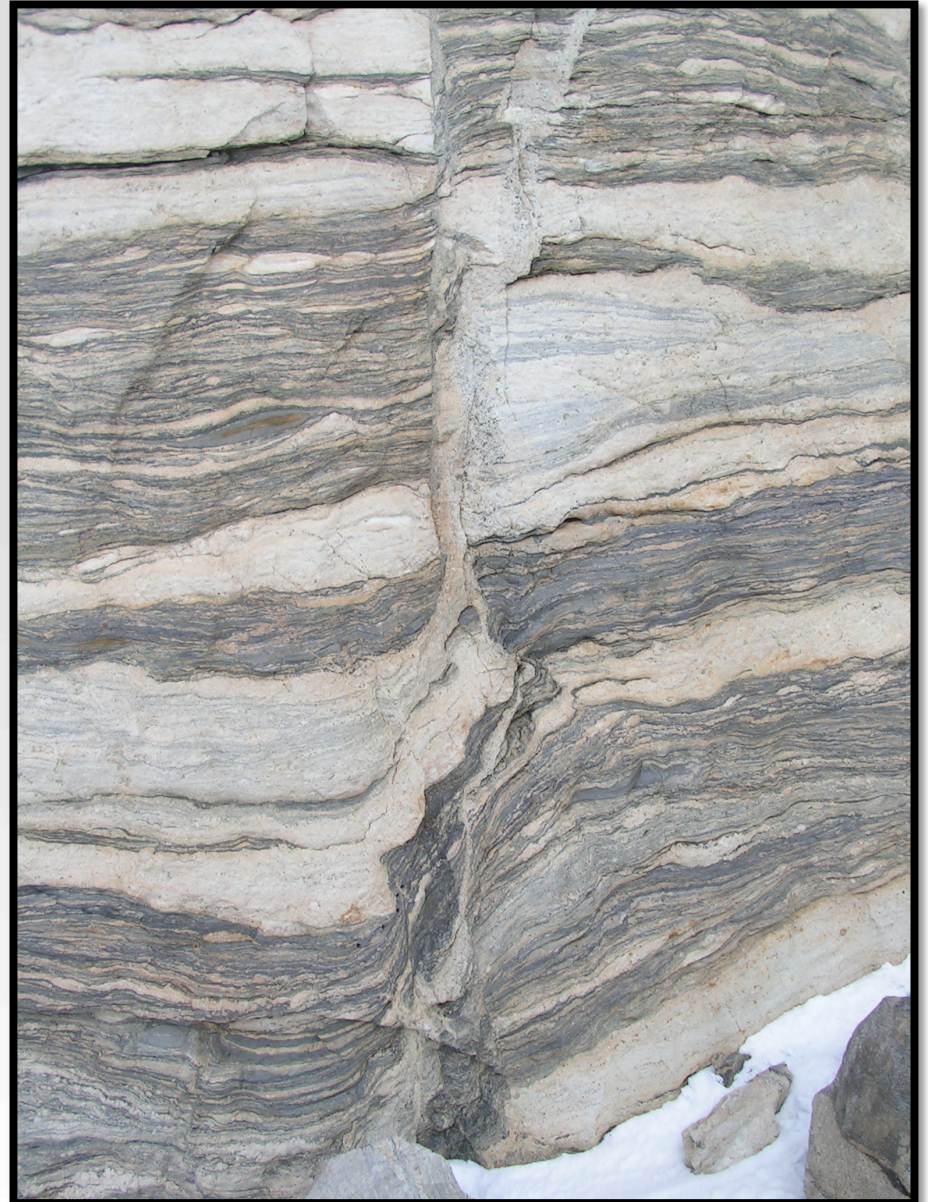
- Brittle law
 - Dominated by cracks
 - Strength increases with depth (Pressure effect)
- Plastic rheology
 - Intracrystalline deformation
 - Strength decreases with depth (Temperature effect)
 - Strain rate dependent

Brittle and plastic shear zones

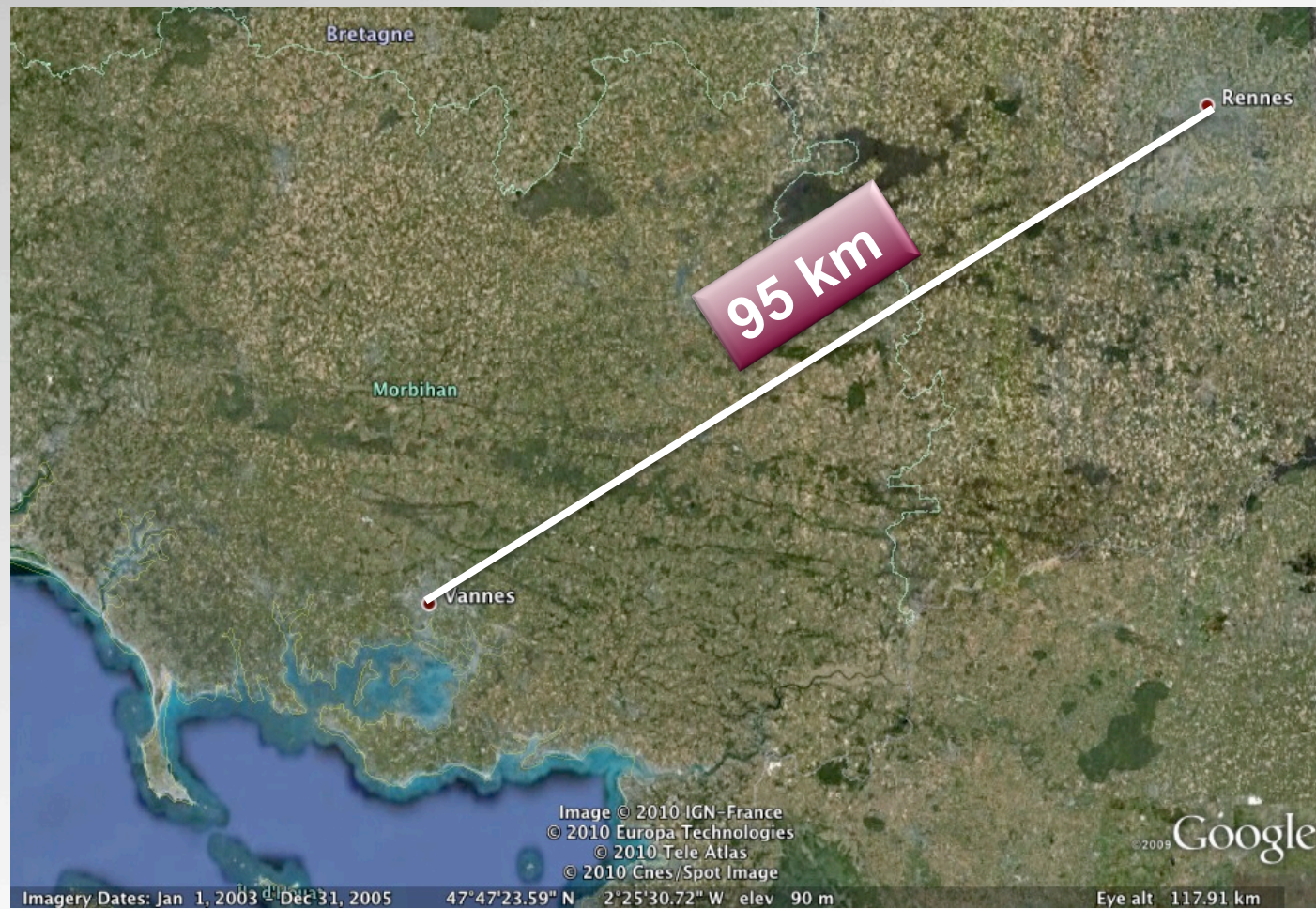


**Small brittle fault
Monterosa Massif, Italy**

**Shear zone in migmatite
Fosdick Mountains
West Antarctica (F. Korhonen)**



South Armorican ...



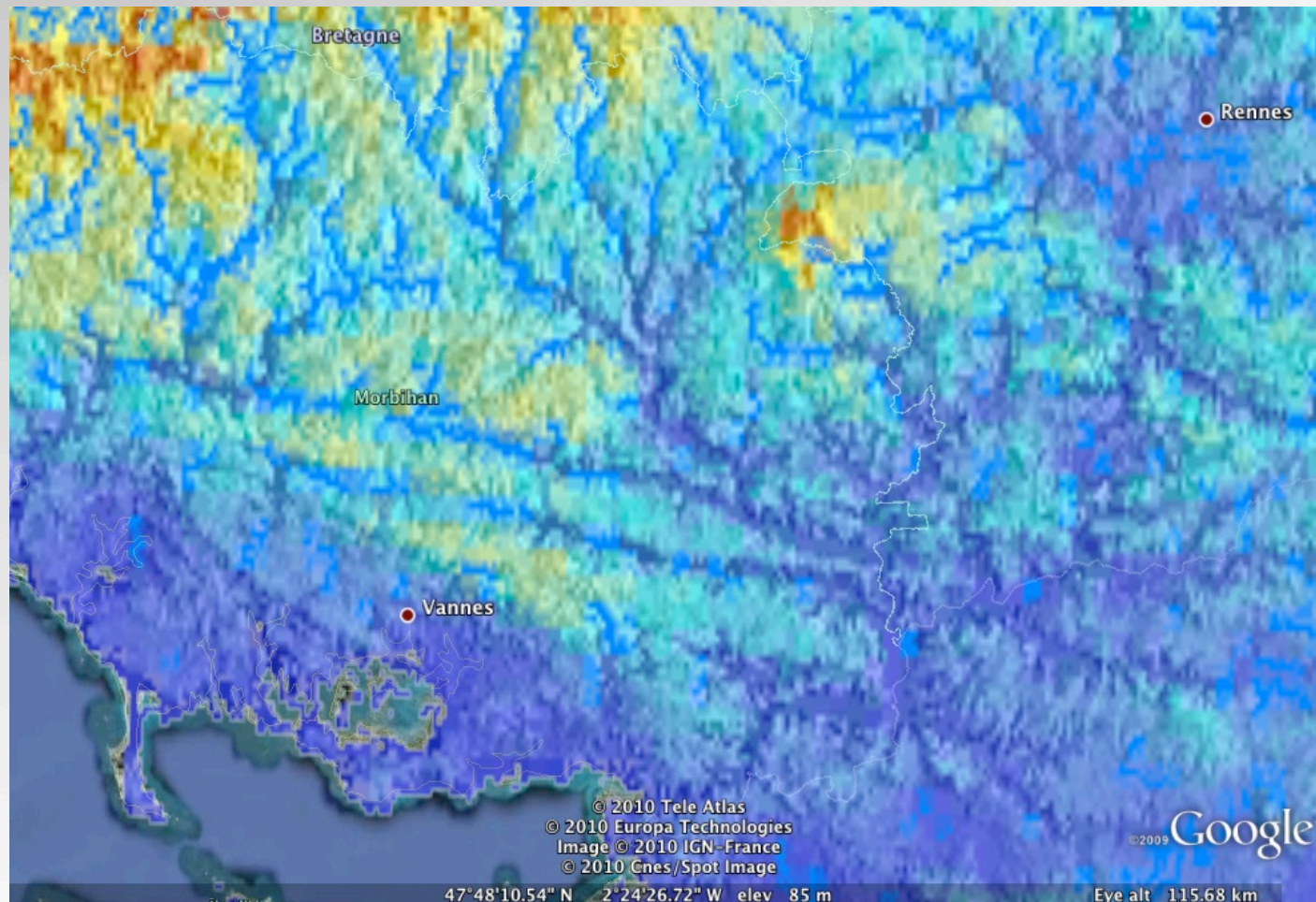
South Armorican Shear Zone ...



Google Earth KMZ from:

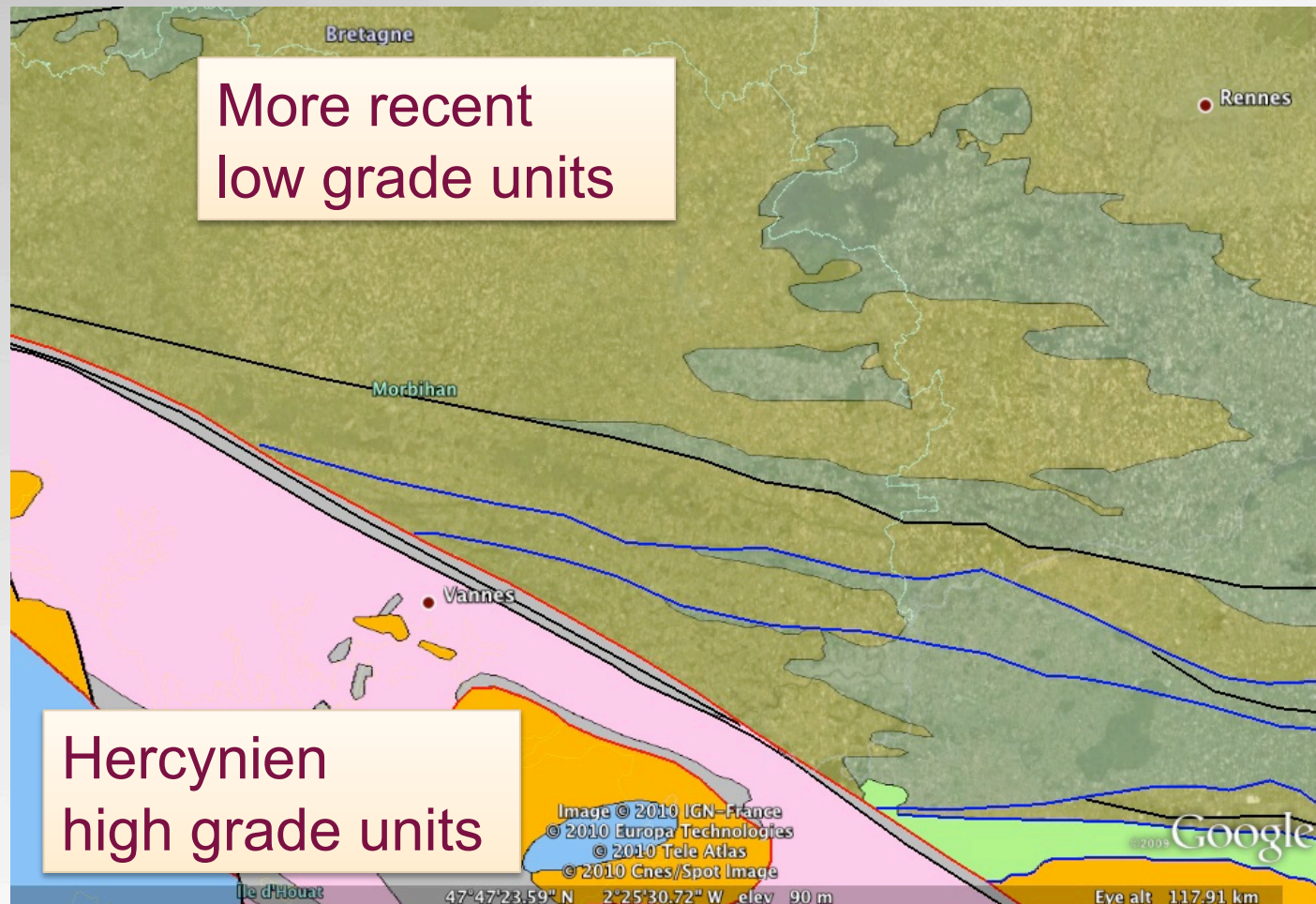
http://perso.univ-rennes1.fr/frederic.gueydan/Kit_MA.htm

South Armorican Shear Zone ...



DTM and Google Earth KMZ from:
http://perso.univ-rennes1.fr/frederic.gueydan/Kit_MA.htm

... a lithospheric-scale structure



Google Earth KMZ from:

http://perso.univ-rennes1.fr/frederic.gueydan/Kit_MA.htm

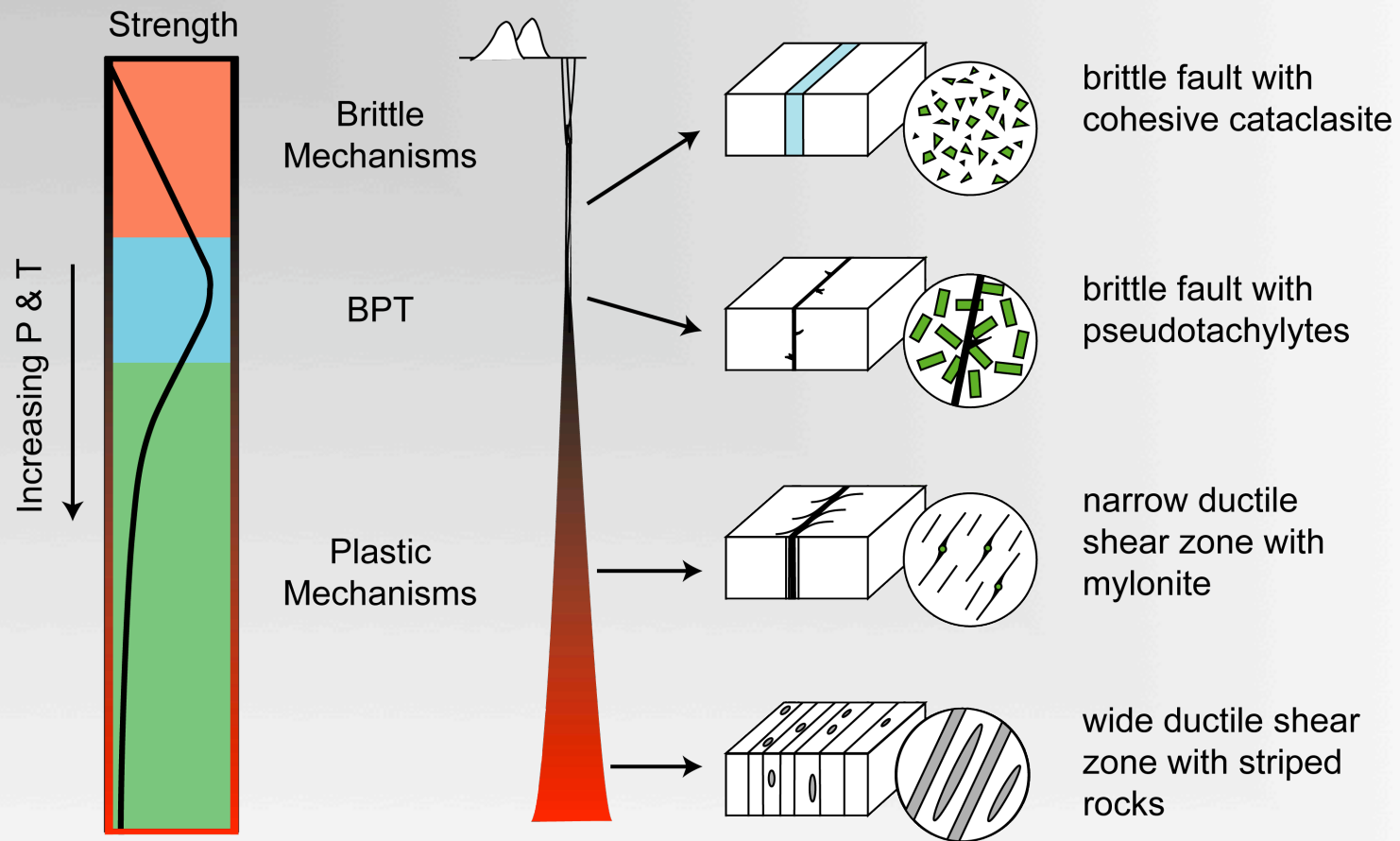
Shear zone structure

- Requires change in state or environment
 - Temperature
 - Grain size
 - Interconnection of weak phase
 - Abundance of weak phase
- On Earth, weak phase is often hydrated
 - Mica, serpentine



L-S tectonites, South American Shear Zone
F. Gueydan, personal communication, 2006

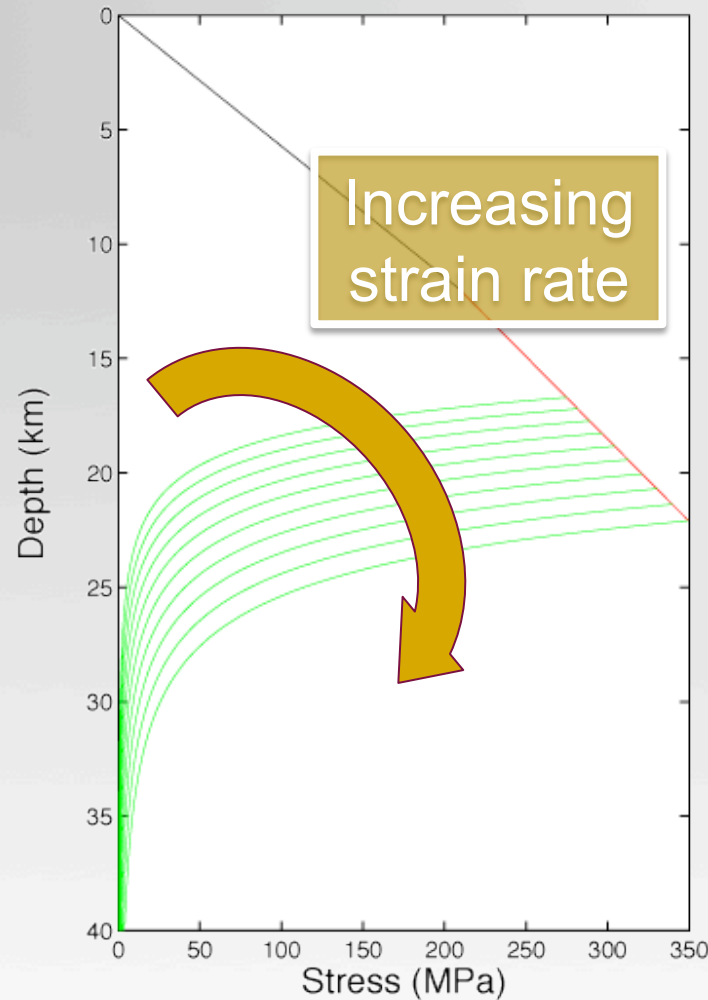
Shear zone profile



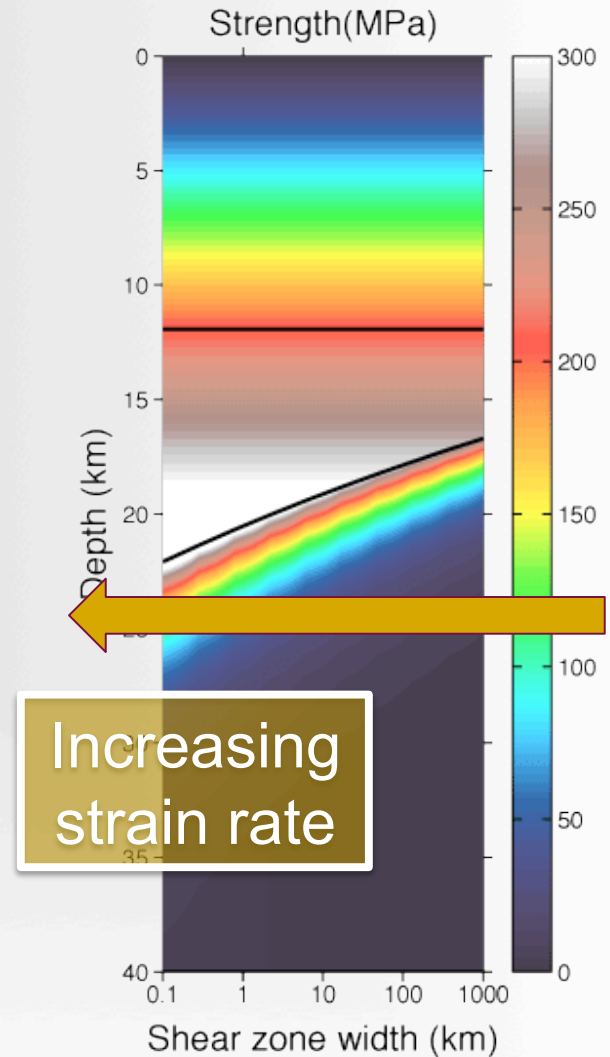
Modified from Passchier & Trouw 1998

Visualizing shear zone strength

- Strength envelope
 - Impose strain rate
- Constant velocity strength map
 - Impose velocity across the shear zone
 - 35 mm/yr over 1km $\Leftrightarrow 10^{-12} \text{ s}^{-1}$

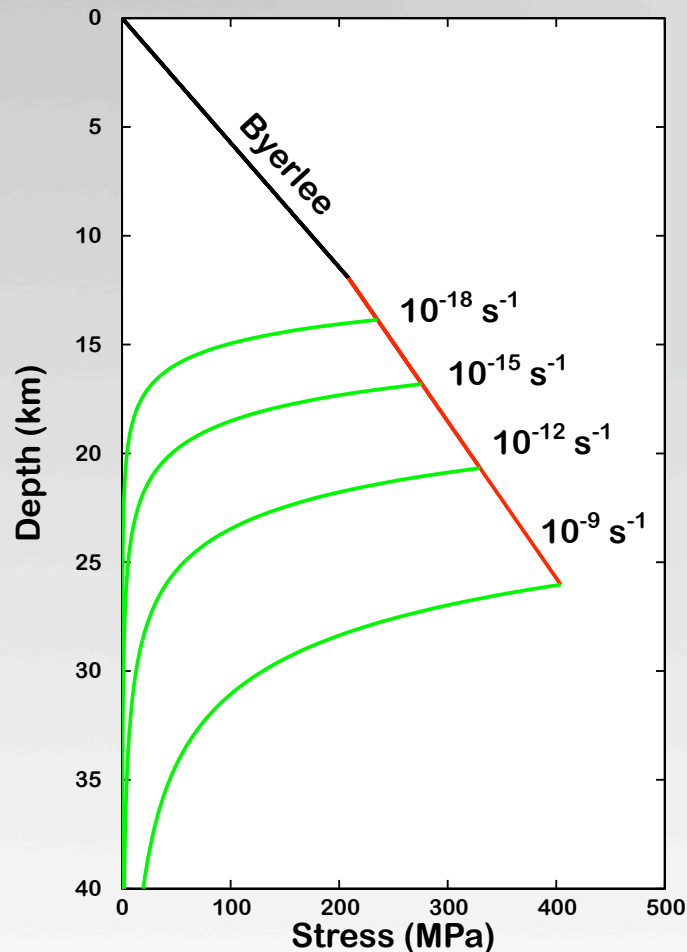


Strength profile



Strength Map

Standard strength envelope



- “Byerlee” friction

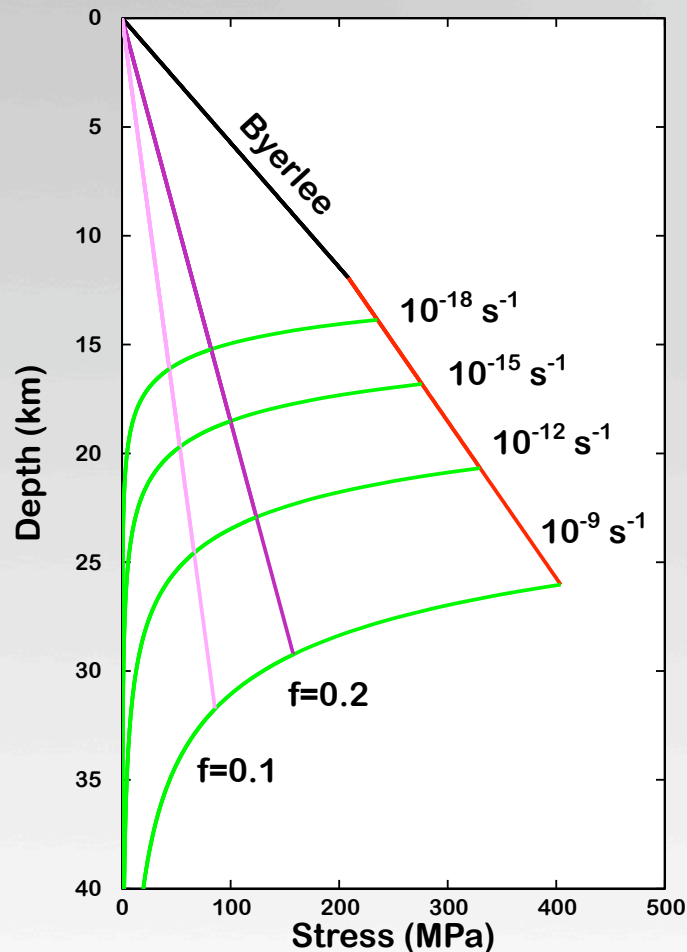
$$\tau = C + f \sigma_n$$

- Wet anorthite dislocation creep (Rybacki and Dresen 2000)

$$\sigma_{II} = A \sigma^n d^{-m} f_{H_2O}^r \exp\left(\frac{Q - PV}{RT}\right)$$

- Half space cooling, $30^\circ/\text{km}$ at the surface, 1350°C at infinity

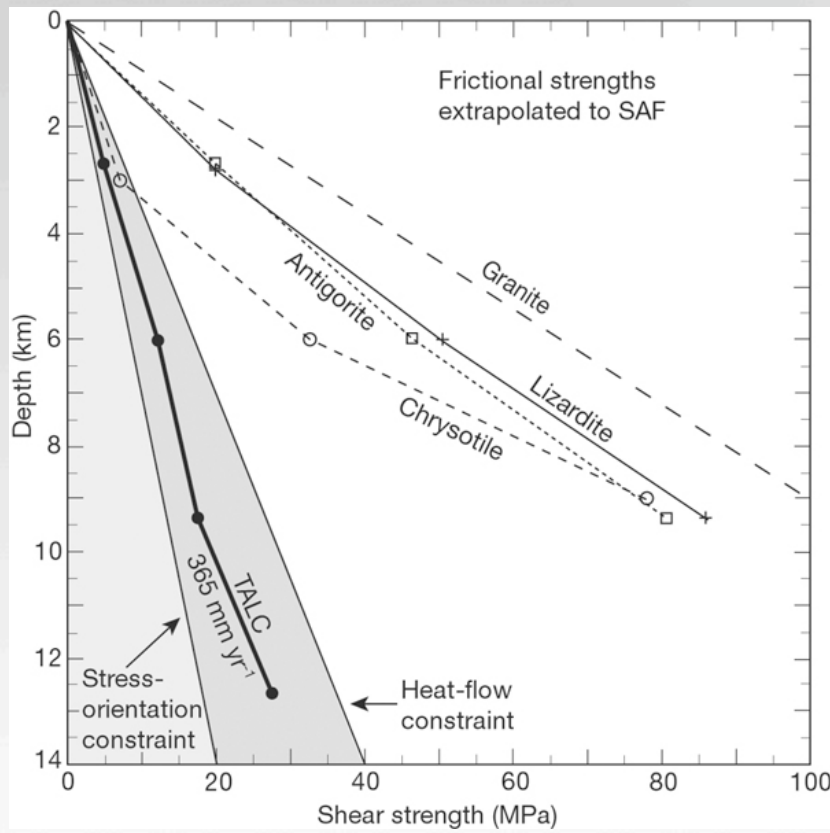
Reduced friction



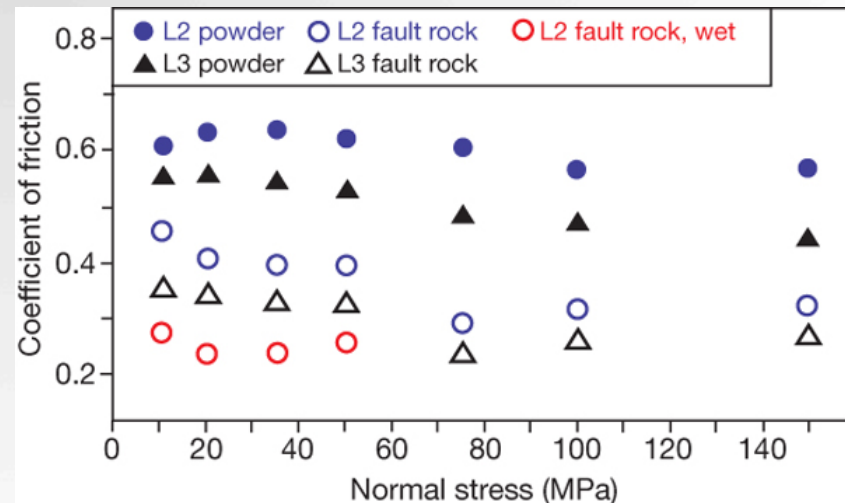
- Inherently weak fault material
 - Talc @ SAFOD (Moore & Rymer, 2007)
- High pore fluid pressure
 - quasi lithostatic
- Dynamic effects
 - Near friction-less sliding at high speed (Di Toro et al., 2004, 2006)
 - Flash heating (Segall & Rice 2006; Rice, 2006)

Natural fault samples

- Talc recovered from SAFOD
- Friction coefficient: 0.25



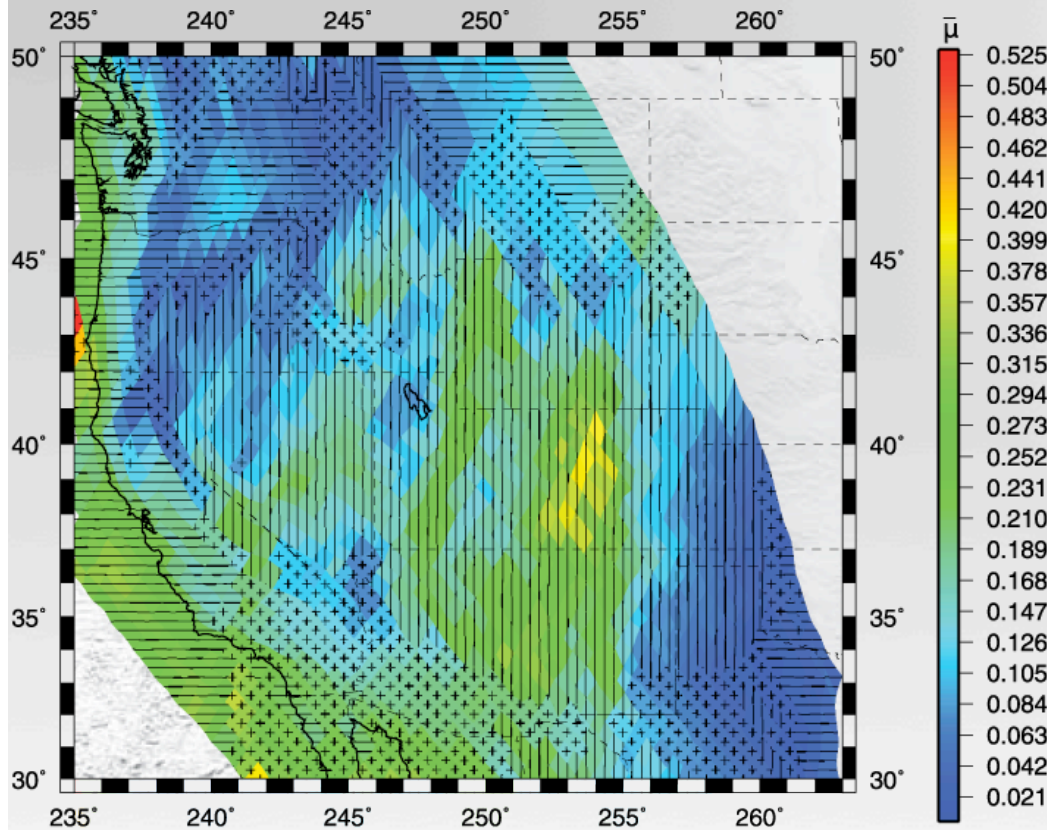
- Frictional properties of fault rocks and powders made from them
- Fault weakness related to foliated fabric



Moore and Rymer, 2007

Collettini et al., 2009

Geodynamic evidence for weak faults



- Geodynamic modeling of stress orientation and tectonic style

- Klein et al., 2009
- 20-40 MPa average viscosity, dominated by seismogenic depths
- Coefficient of friction of 0.2 or less even with $\lambda=0.7$ (“wet” crust)

- Slip and stress inversions

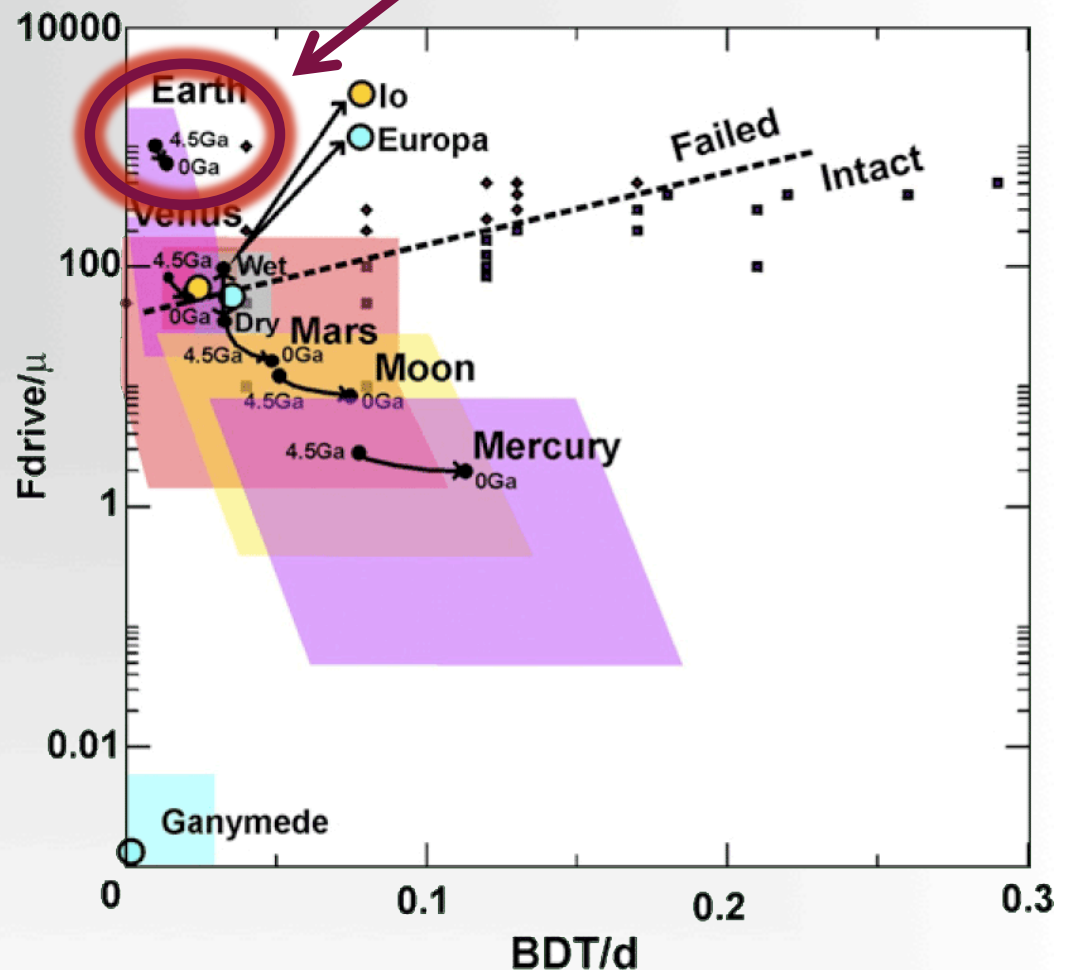
- Carena & Moder, 2010
- Coefficient of friction between 0.05 and 0.2,

Flesch et al., 2007
Klein et al., 2009

A plate tectonic recipe

- Vigorous convection
- Failure in the lithosphere
 - Yield strength $< \sim 3$ MPa (Solomatov, 2004)
 - Effective coefficient of friction: 0.15 (O'Neill et al. 2007)

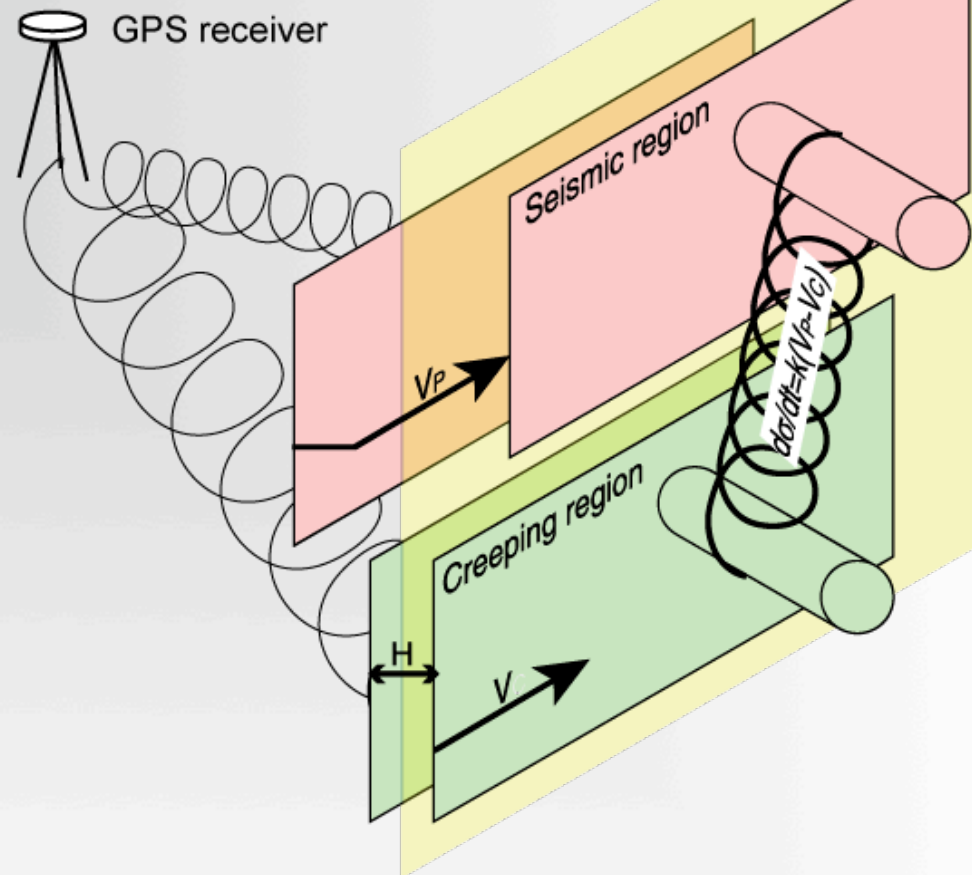
Weakened arbitrarily



O'Neill, Jellinek, and Lenardic, 2007

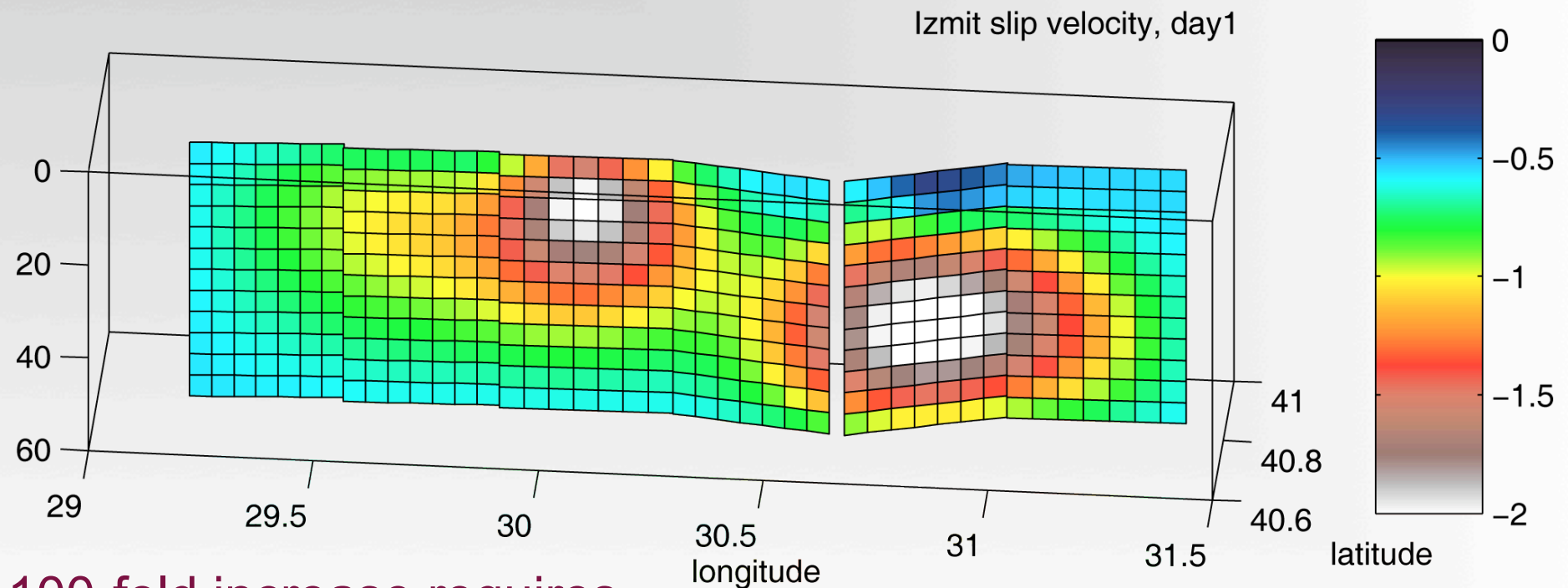
Conceptual model for postseismic creep

- Sudden motion on fault loads elastically nearby shear zone
- Shear zone accelerates
- When stress is released, shear zone decelerates



Change in shear zone velocity

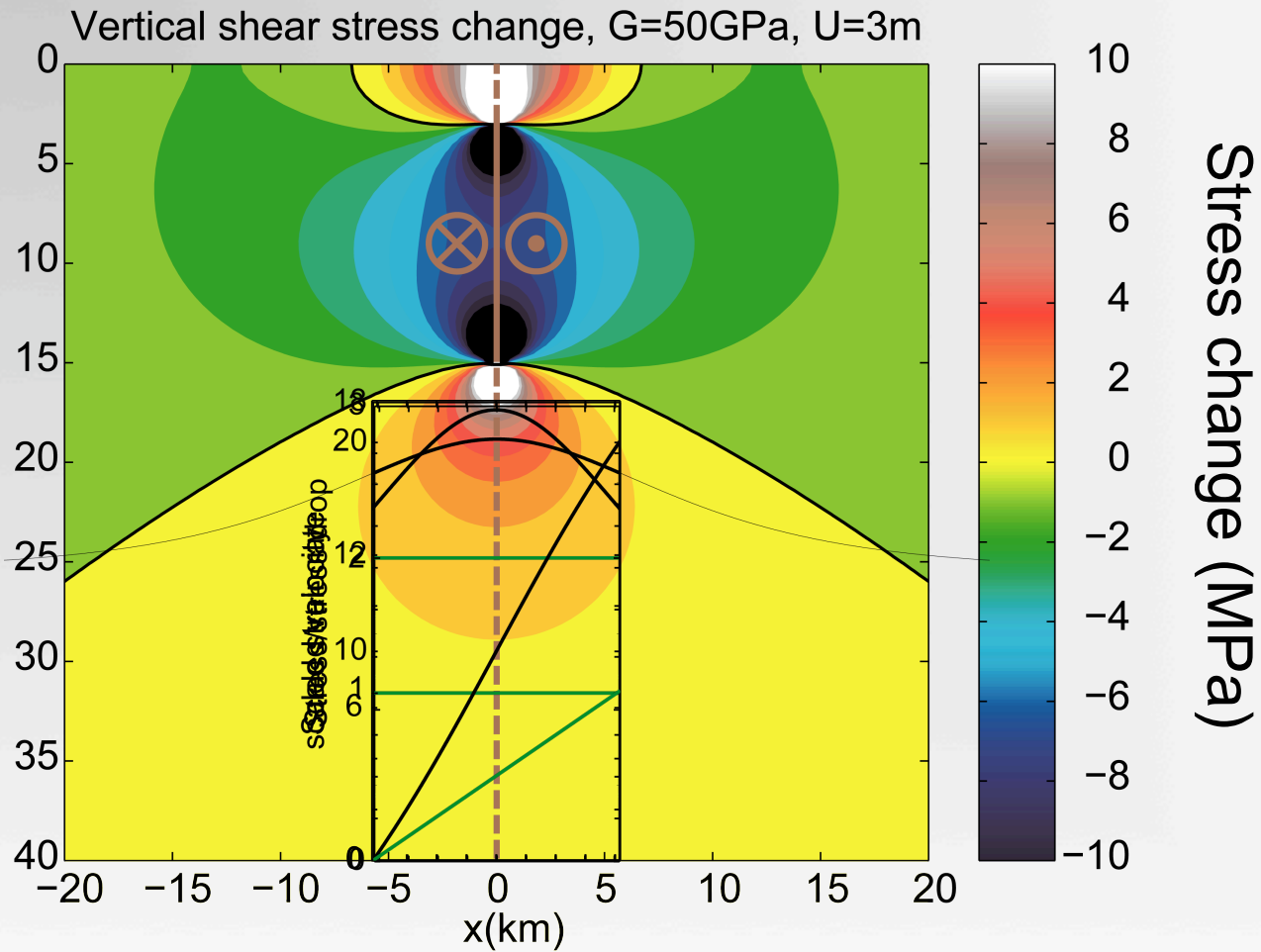
- North Anatolian Fault interseismic velocity: 25 mm/yr (McClusky et al., 2001)
- Post-Izmit slip rate: up to 2 m/yr



100-fold increase requires
initial stress comparable to stress drop

Bürgmann et al., 2002

Transient velocity increase

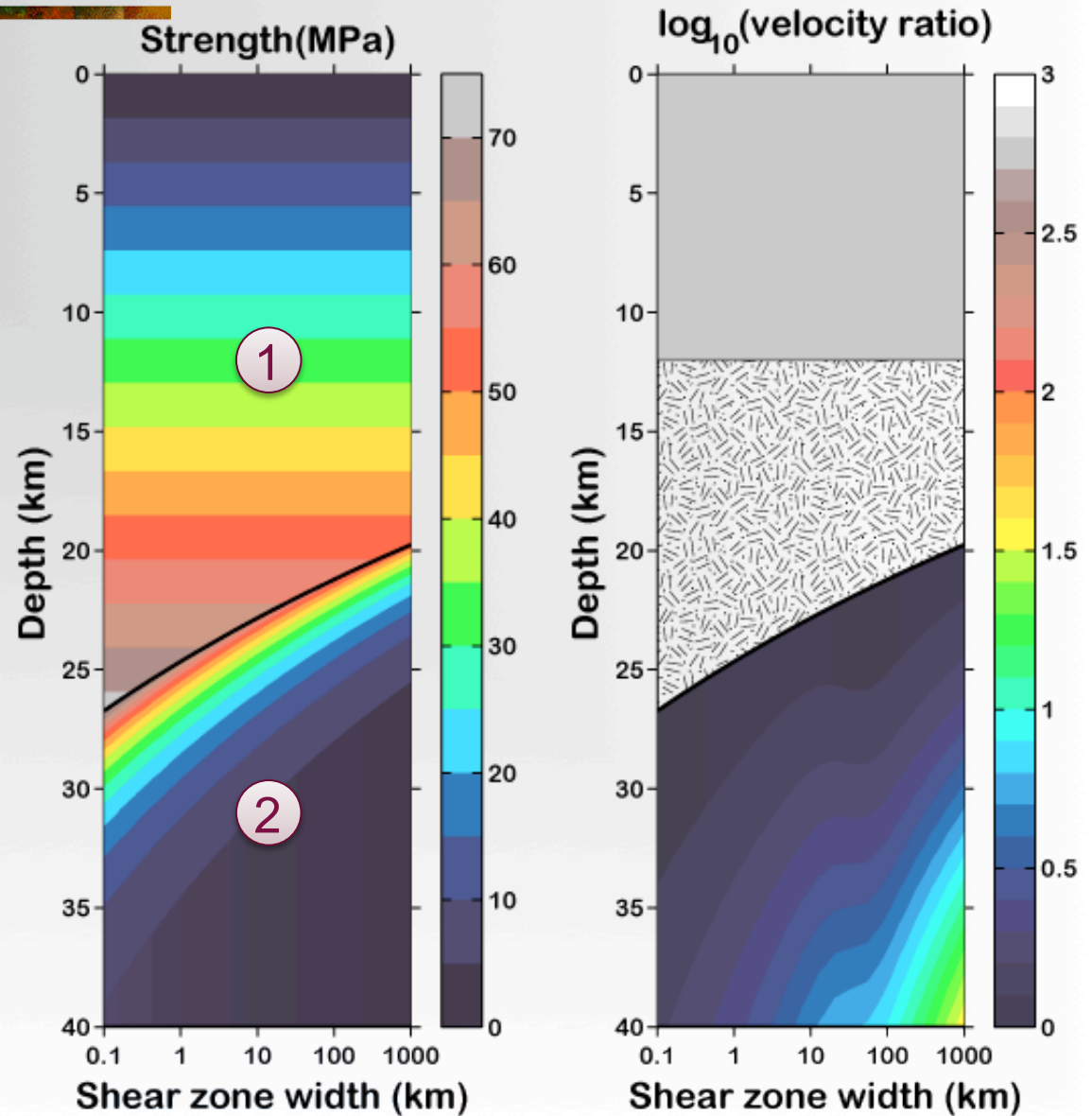


Feldspar dislocation creep

- Anorthite flow law (Rybacky and Dresen, 2000)
 - 0.07 wt% H₂O: “wet” conditions
 - Earthquake to 12 km depth, 5m slip
 - 30 K/km geotherm
- Shear zone is too strong: no response to earthquake

① Brittle ($f=0.1$)

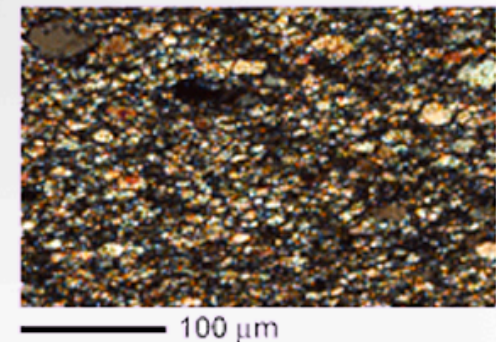
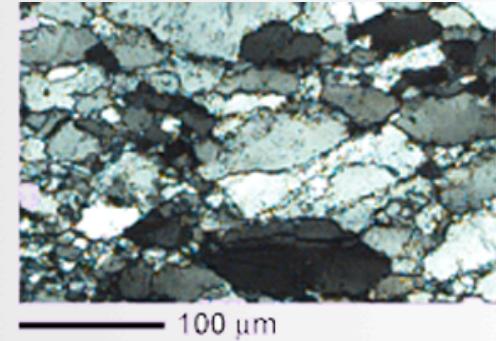
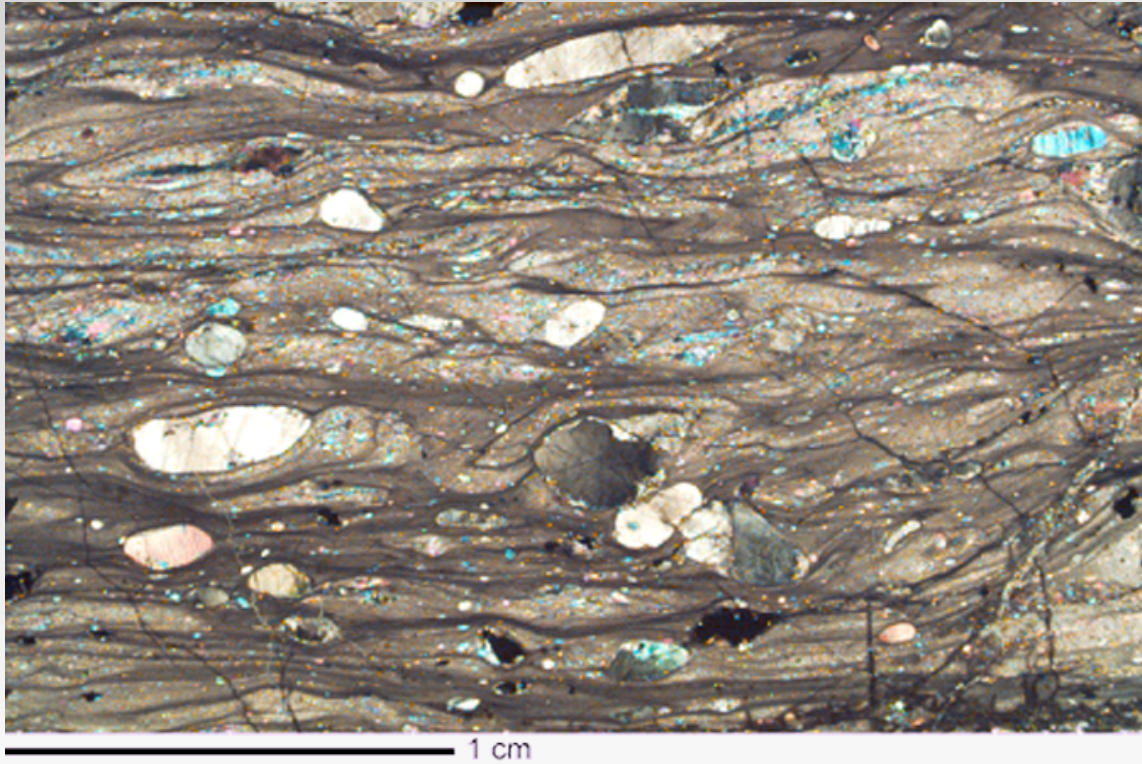
② Dislocation creep



Grain Size Reduction

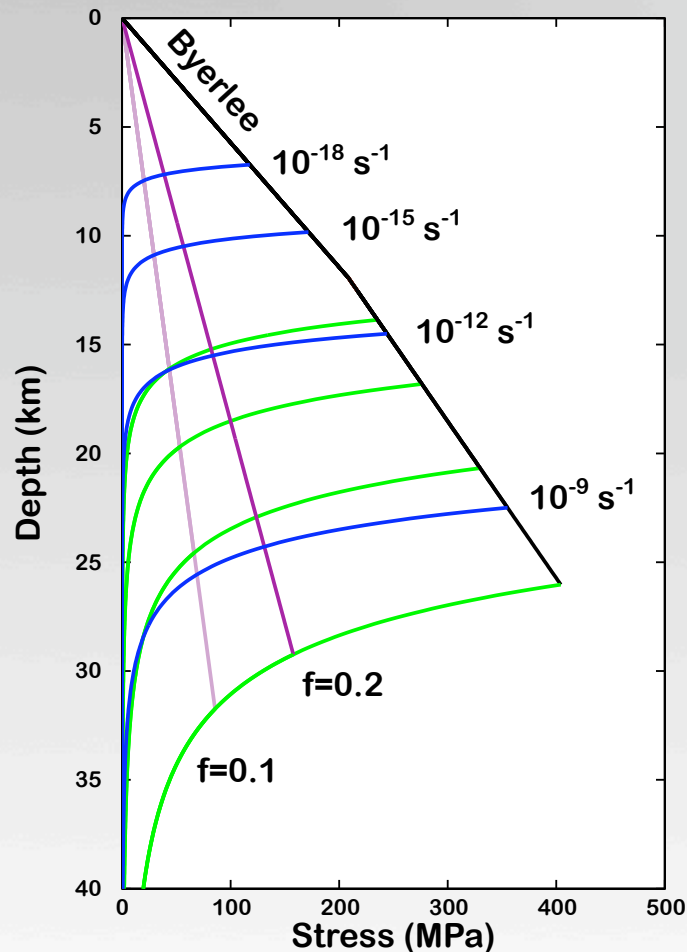
- Mylonite in oceanic peridotite, Shaka Fracture zone

Shear direction
→
←



Warren and Hirth, 2006

Grain size reduction



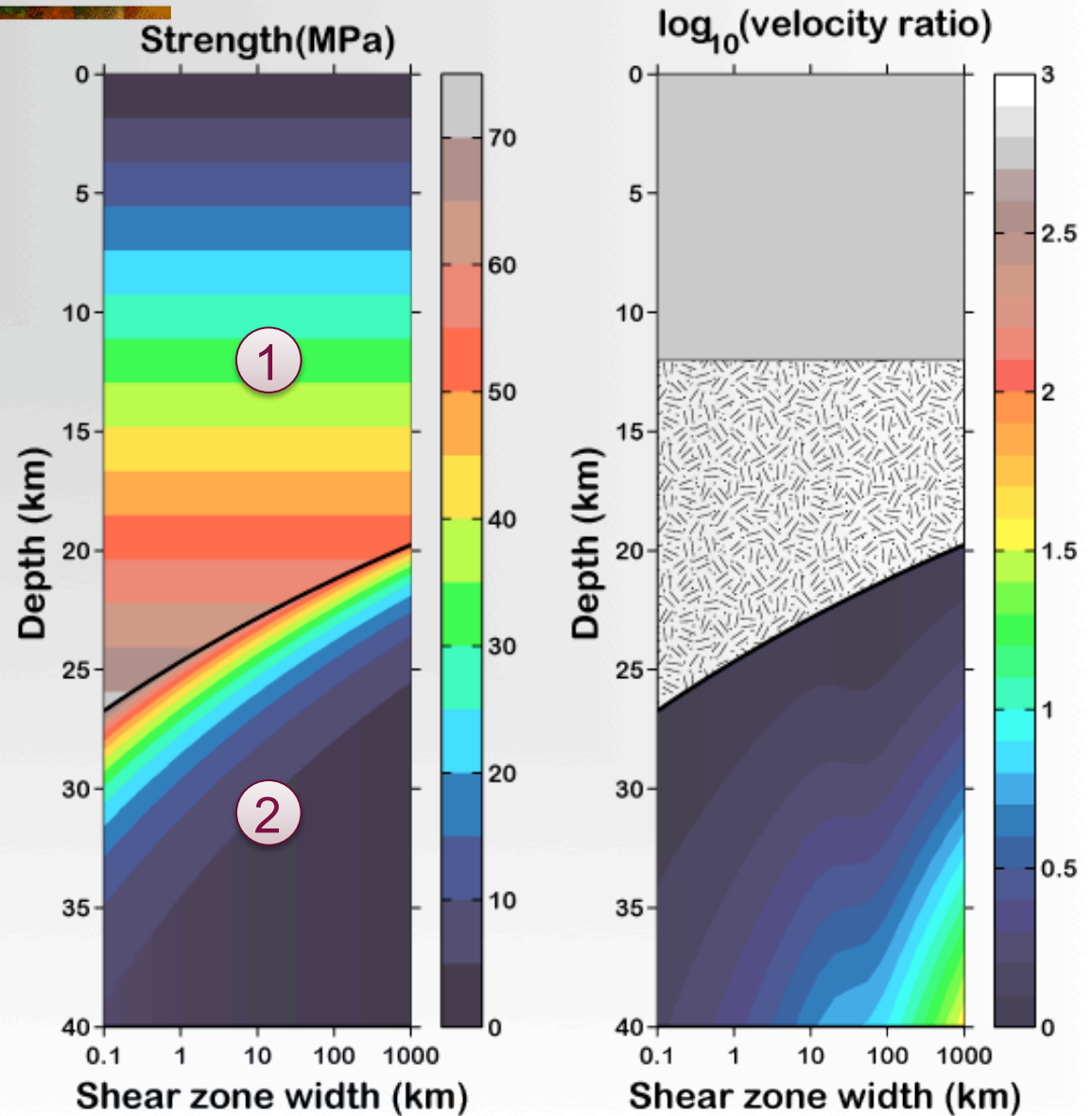
- Byerlee" friction
- Wet anorthite rheology (Rybacki and Dresen 2000)
 - Dislocation creep
 - Diffusion creep 10 microns grain size
- Surface geotherm $30^\circ/\text{km}$
- Strain rate 10^{-9} to 10^{-18} s^{-1}

Feldspar dislocation creep

- Anorthite flow law (Rybacky and Dresen, 2000)
 - 0.07 wt% H₂O: “wet” conditions
 - Earthquake to 12 km depth, 5m slip
 - 30 K/km geotherm
- Shear zone is too strong: no response to earthquake

① Brittle ($f=0.1$)

② Dislocation creep

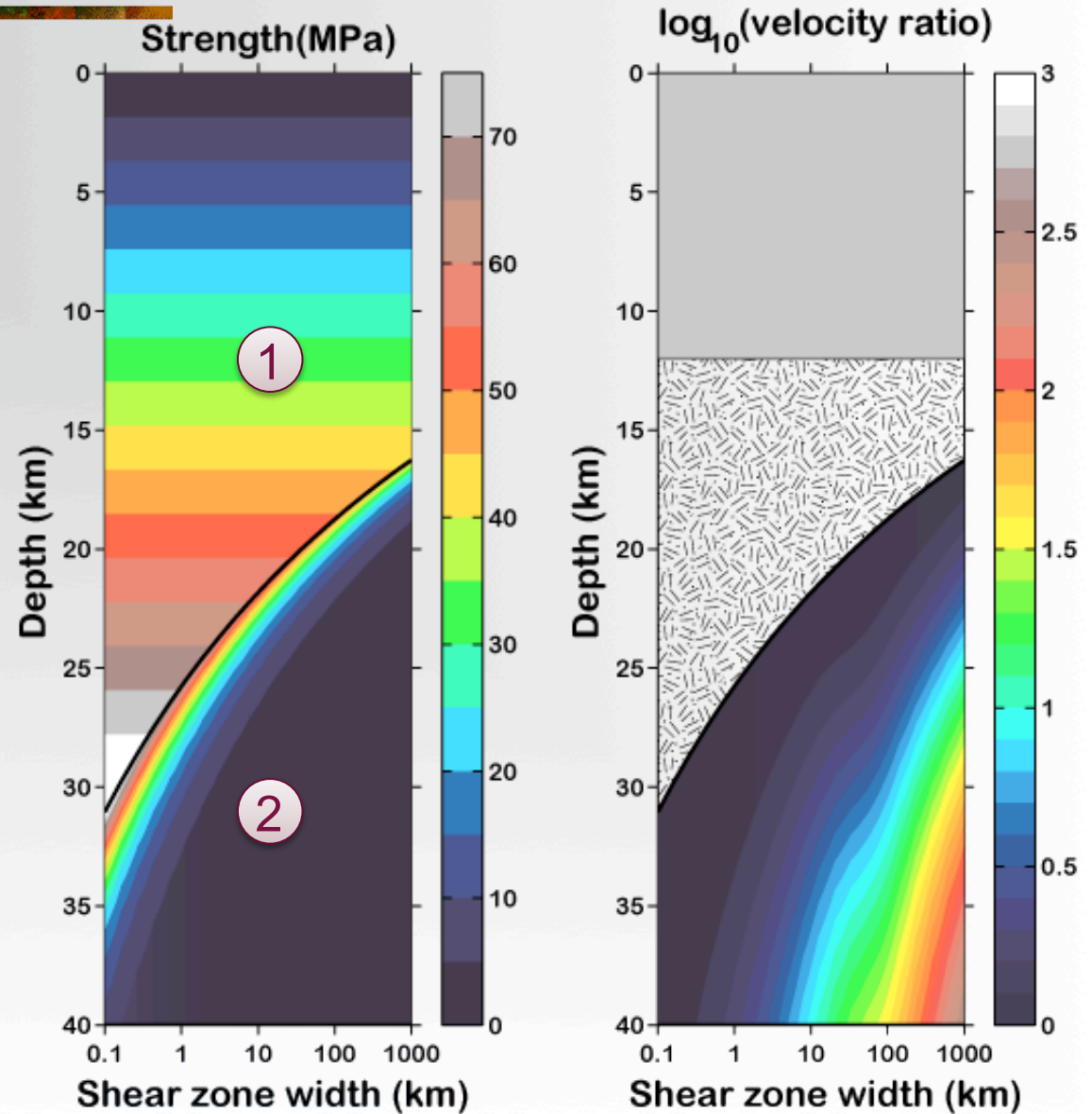


Feldspar (100 μm grain size)

- Anorthite flow law (Rybacky and Dresen, 2000)
 - 0.07 wt% H_2O : “wet” conditions
 - Earthquake to 12 km depth, 5m slip
 - 30 K/km geotherm
- Shear zone is still too strong

① Brittle ($f=0.1$)

② Diffusion creep

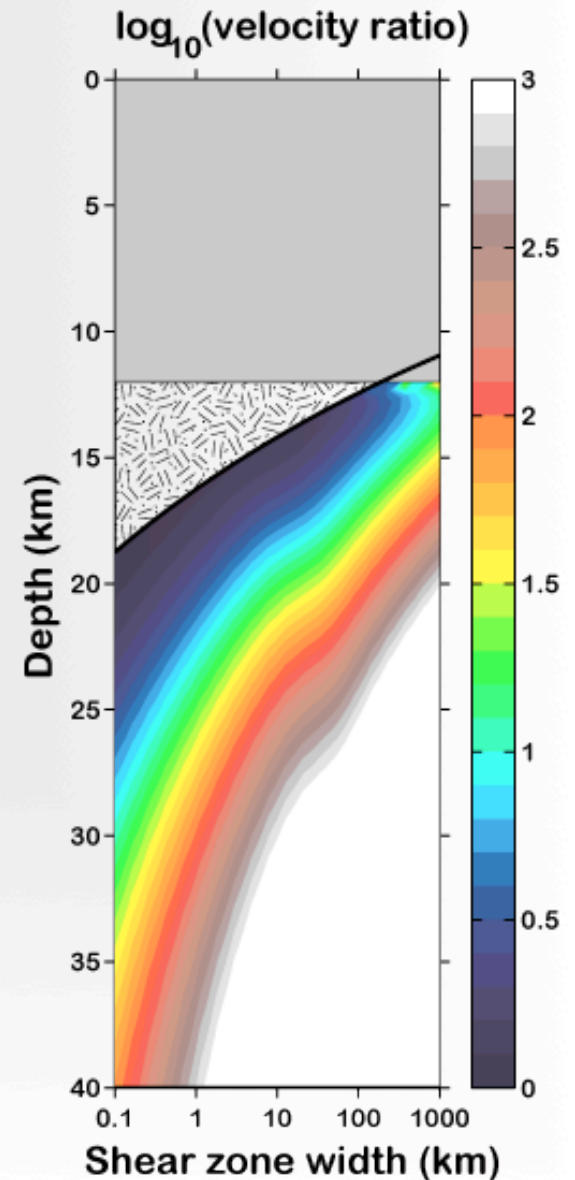
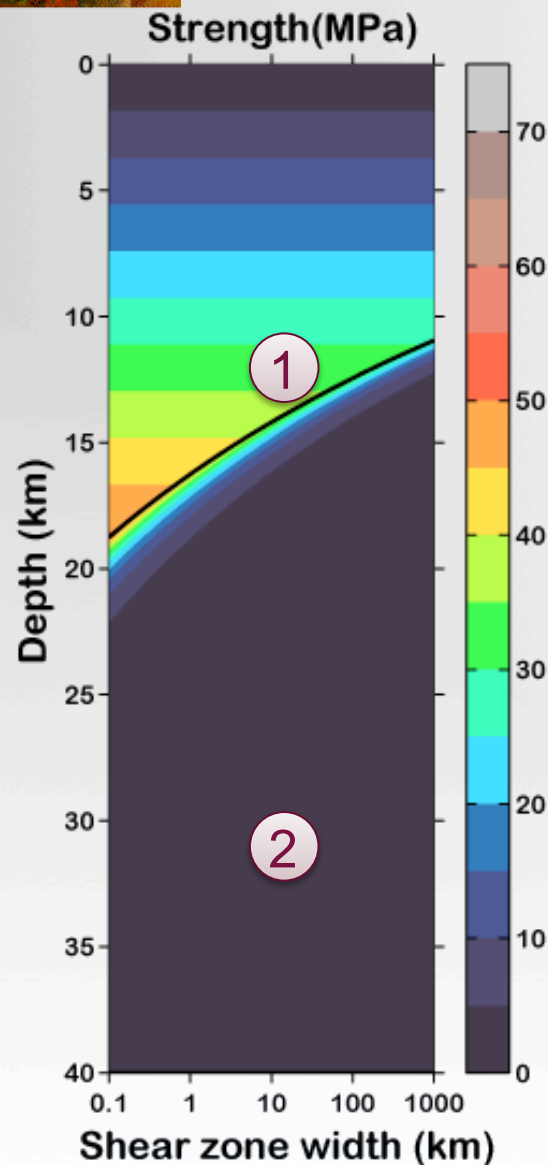


Feldspar (10 μm grain size)

- Anorthite flow law (Rybacky and Dresen, 2000)
 - 0.07 wt% H_2O : “wet” conditions
 - Earthquake to 12 km depth, 5m slip
 - 30 K/km geotherm
- Deep postseismic creep in wide shear zones only

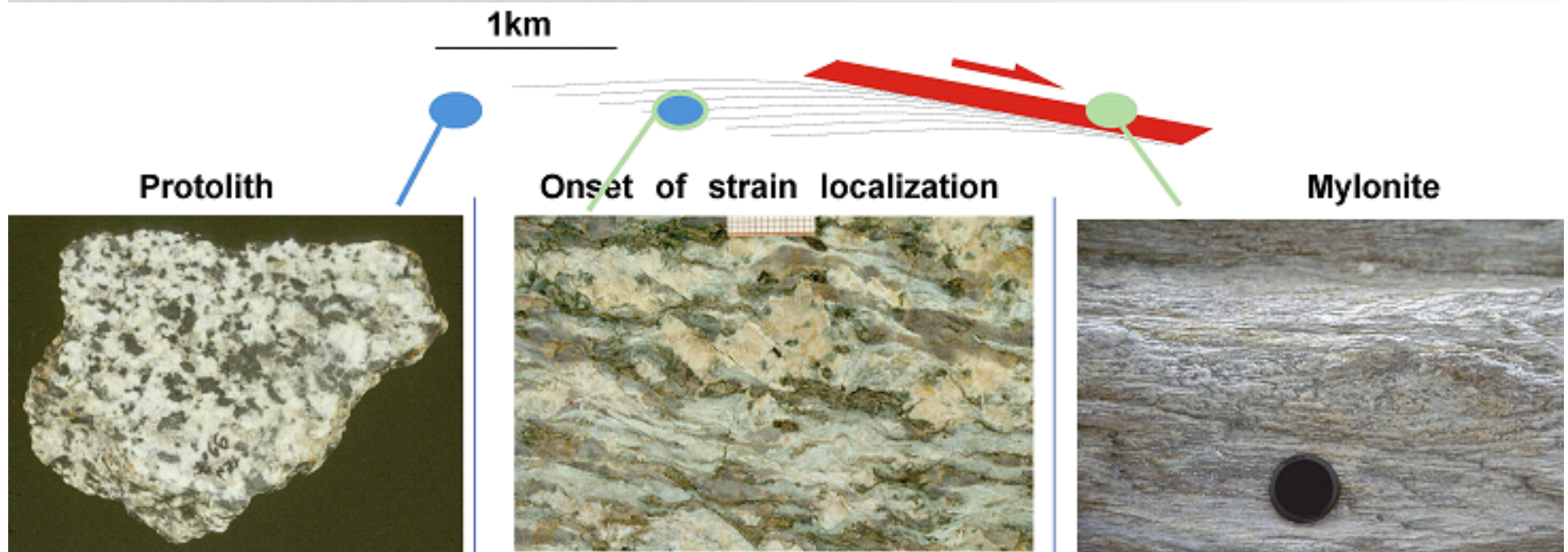
① Brittle ($f=0.1$)

② Diffusion creep



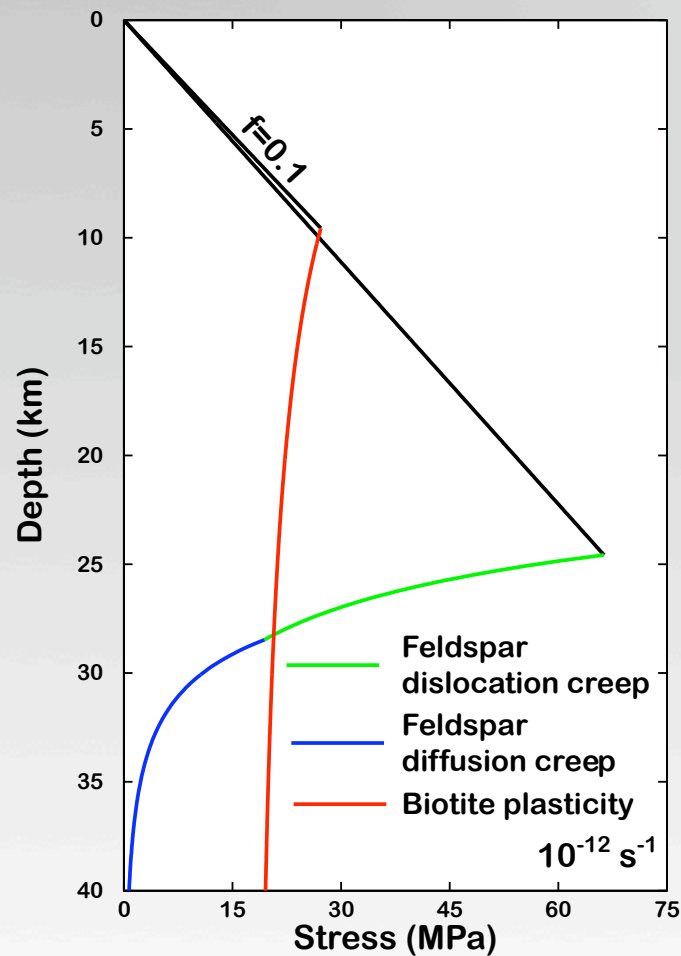
Fabric development and metamorphism

- Tenda Massif, Corsica (granitoid)
- Initial localization: fracturing of Feldspar
- Mylonite development: Feldspar-to-mica reaction



Gueydan et al., JGR, 2003

Mica rheology



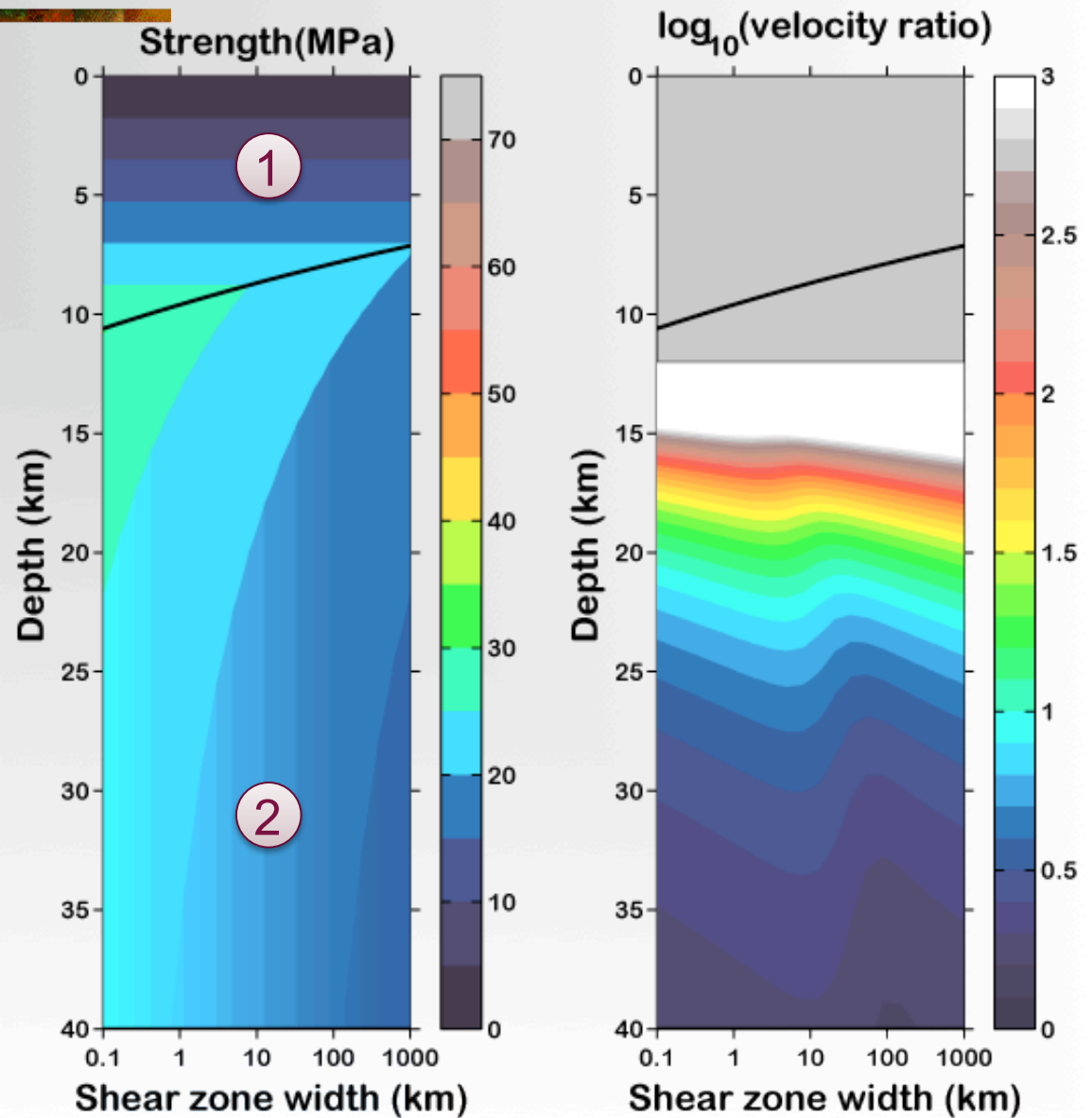
- Kronenberg, 1990
- Biotite aggregate
 - Low activation energy
 - High stress exponent
 - Power law may not be the most appropriate rheology

Biotite shear zone

- Biotite flow law (Kronenberg, 1990)
 - Highly nonlinear
 - Little temperature dependence
- Shallow postseismic creep
- Mica acts as strength control

① Brittle ($f=0.1$)

② Biotite dislocation creep

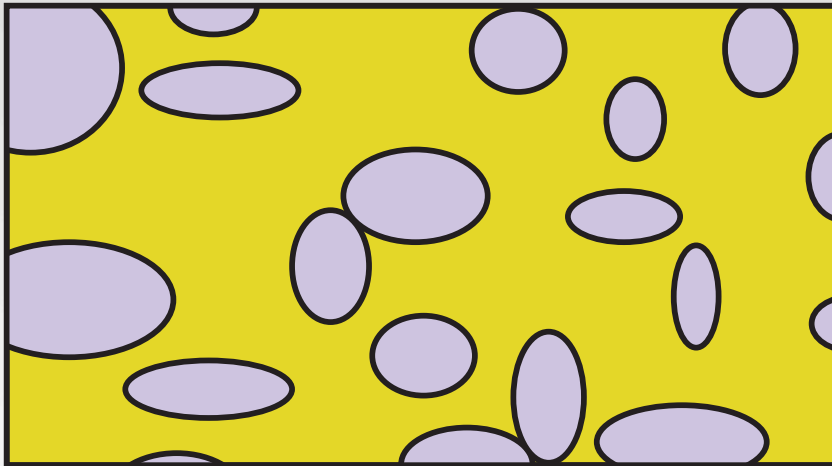


End-member mixture models

Constant strain rate

Appropriate of well-mixed aggregate, with strain incompatibility

Protolith

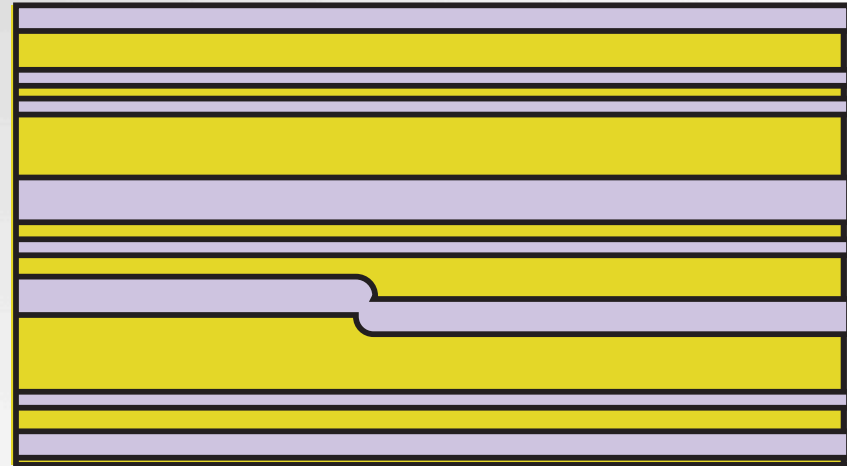


$$\sigma_d = (1 - C)(\dot{\epsilon}/A_a)^{n_a} + C(\dot{\epsilon}/A_b)^{n_b}$$

Constant stress

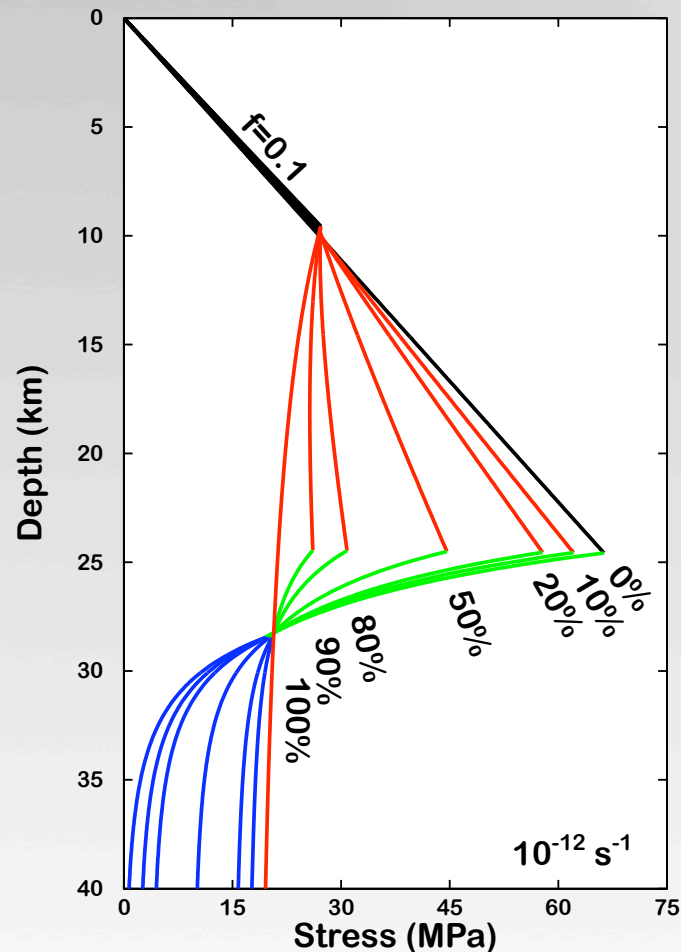
Appropriate for layered fabric, with phase separation

Shear zone



$$\dot{\epsilon} = (1 - C)A_a\sigma_c^{n_a} + CA_b\sigma_c^{n_b}$$

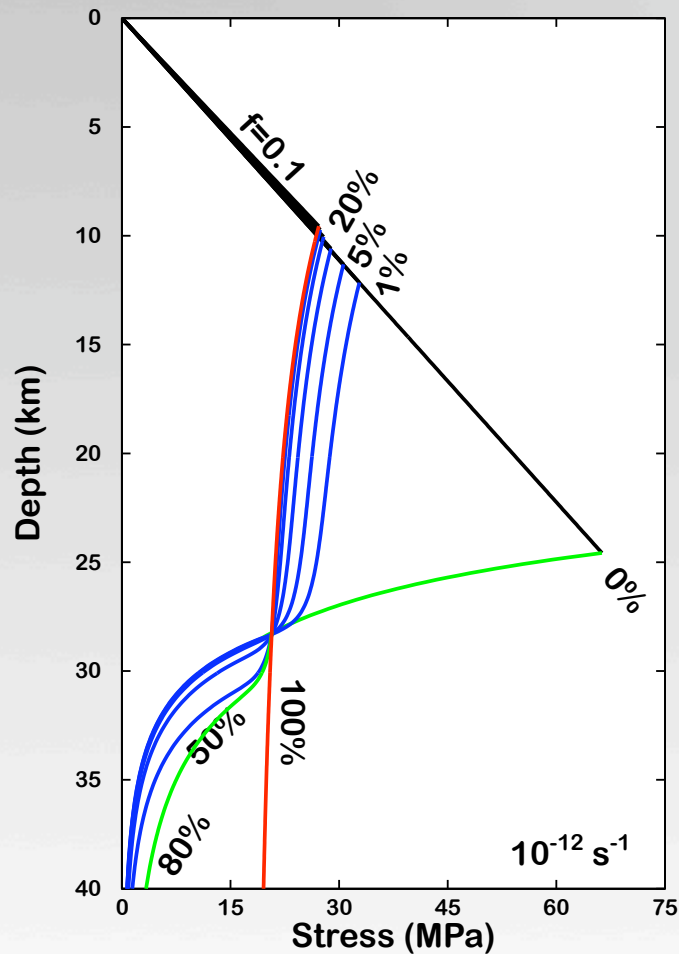
Mixing model: constant strain rate



- Appropriate if strain incompatibility, or homogeneous mixture
- Dominated by strong phase (feldspar)
- Weakening needs high mica content

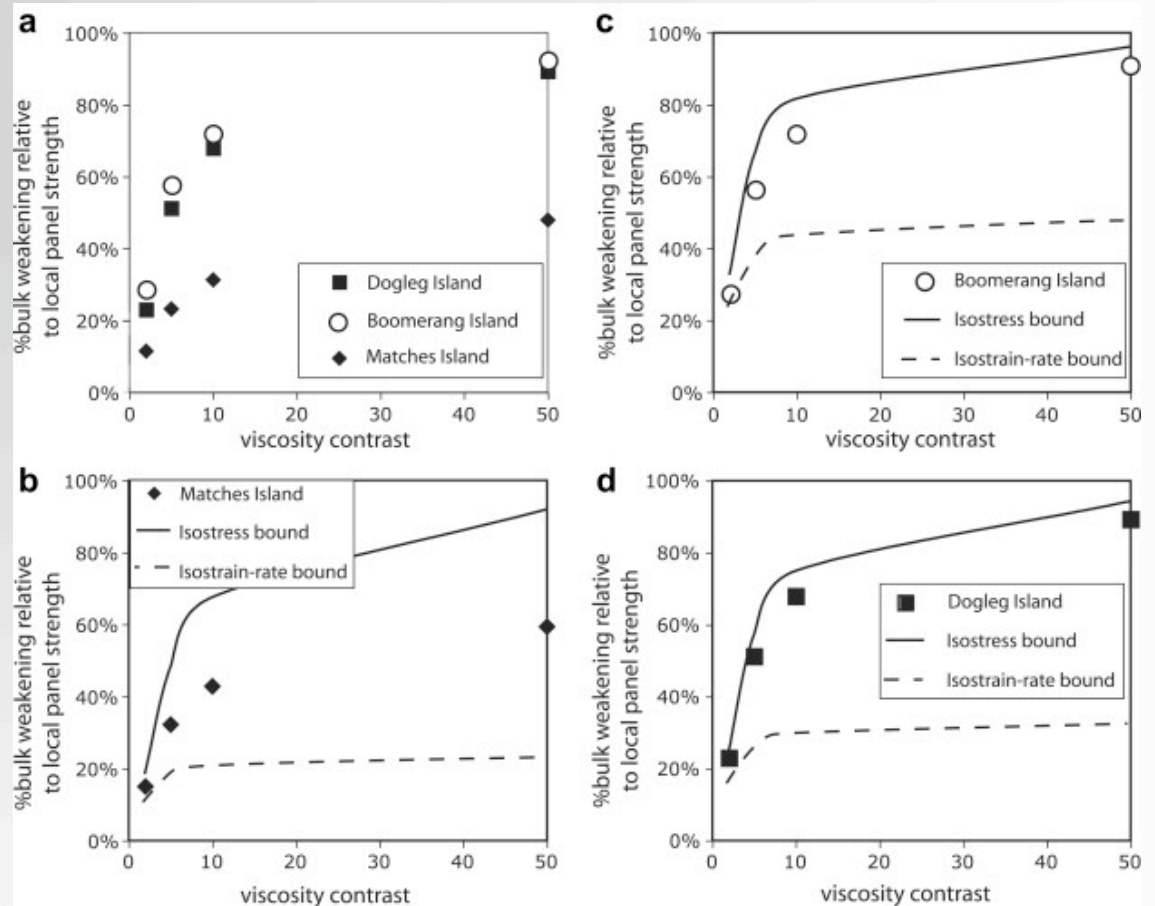
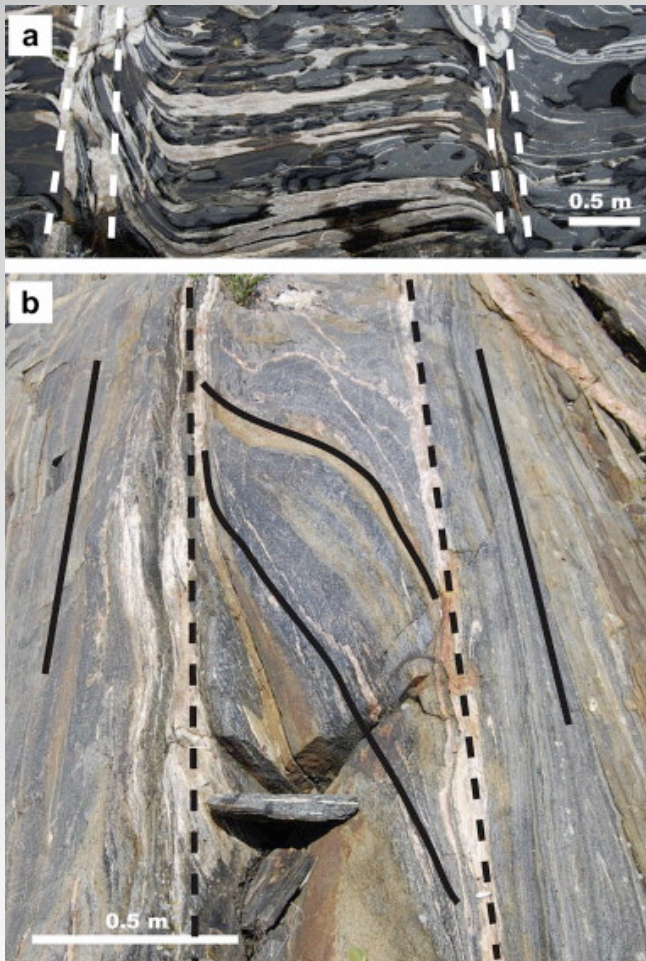
	Biotite	Feldspar
—	brittle	brittle
—	plastic	brittle
—	plastic	dislocation creep
—	plastic	diffusion creep

Mixing model: constant stress



- Appropriate if phase separation, layering
- Dominated by weak phase
- Weakening even for small amounts of
- Almost insensitive to the amount of mica

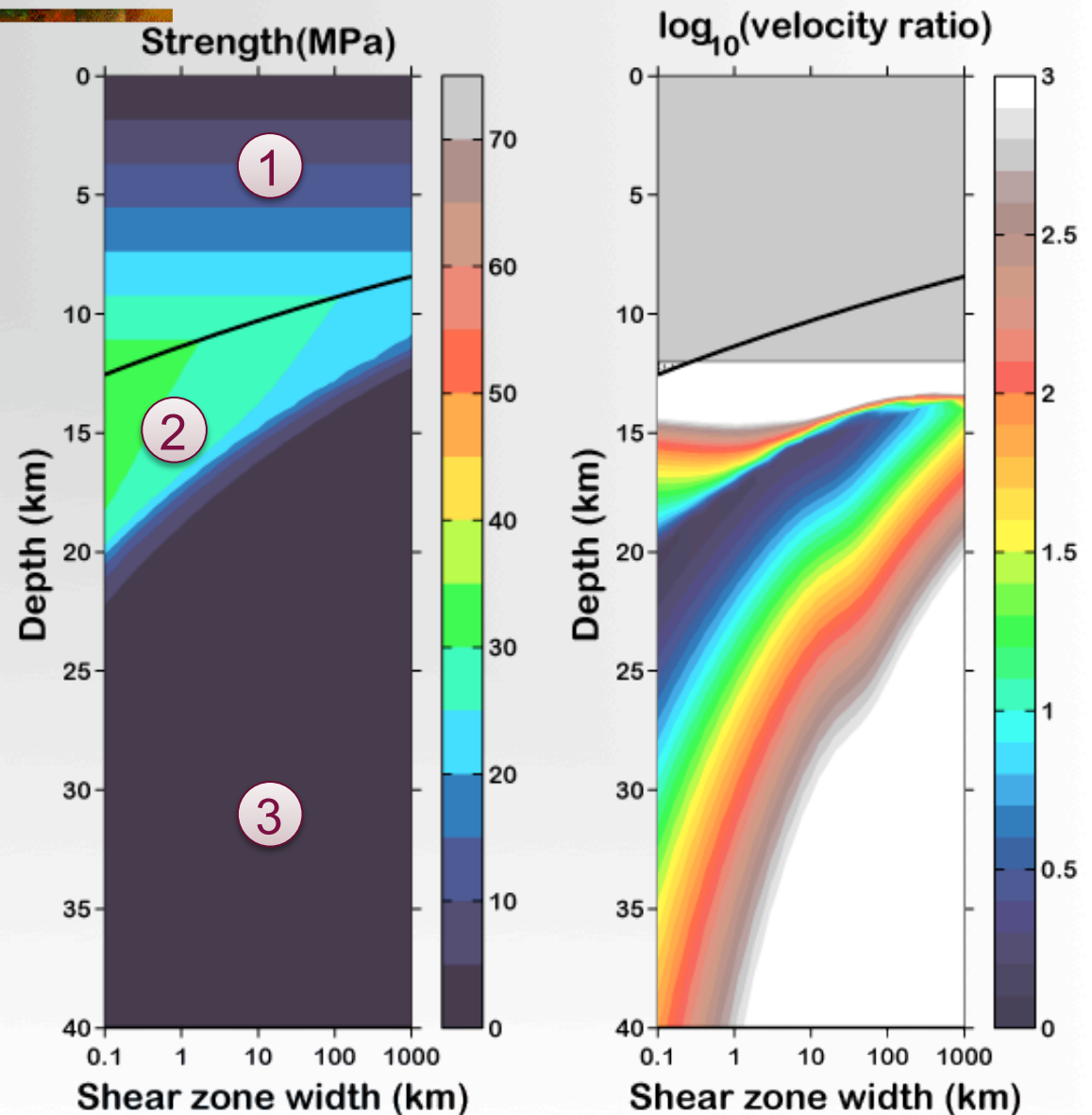
Strength contrast in shear zones



Biotite/feldspar foliated shear zone

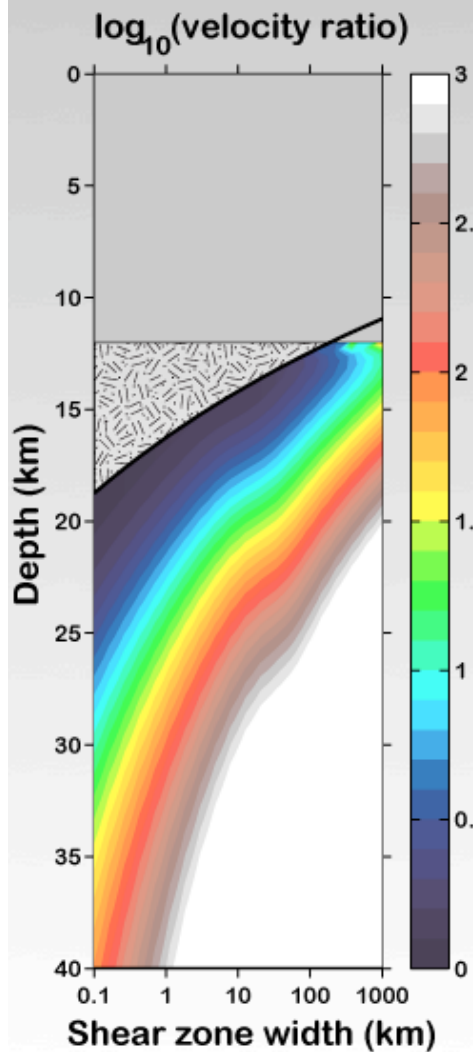
- 95 % feldspar (10 μm grain size) and 5% biotite
- Perfect foliation
- Two-level response
 - Near BPT: biotite control
 - At depth: Grain size reduction

- ① Brittle ($f=0.1$)
- ② Biotite-dominated plastic creep
- ③ Feldspar-dominated plastic creep



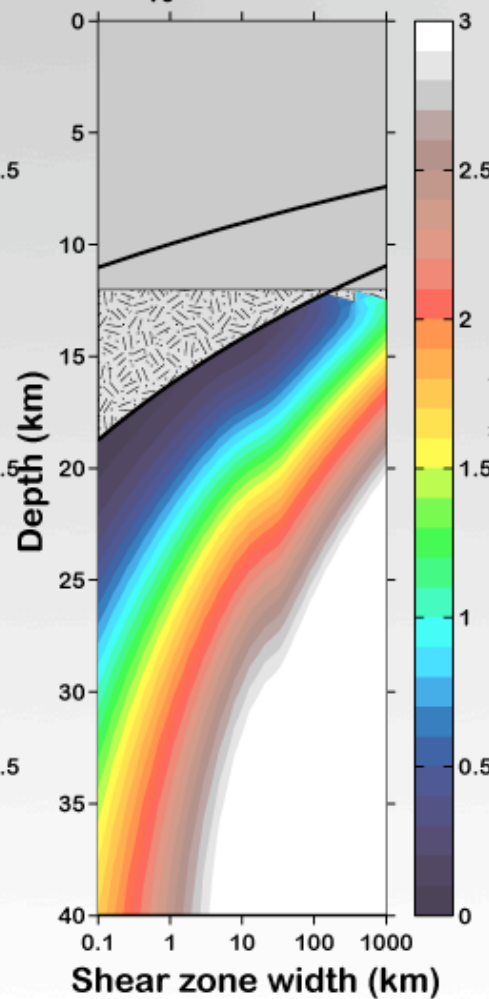
Effect of fabric ($10\mu\text{m}$ grain size)

100% Feldspar



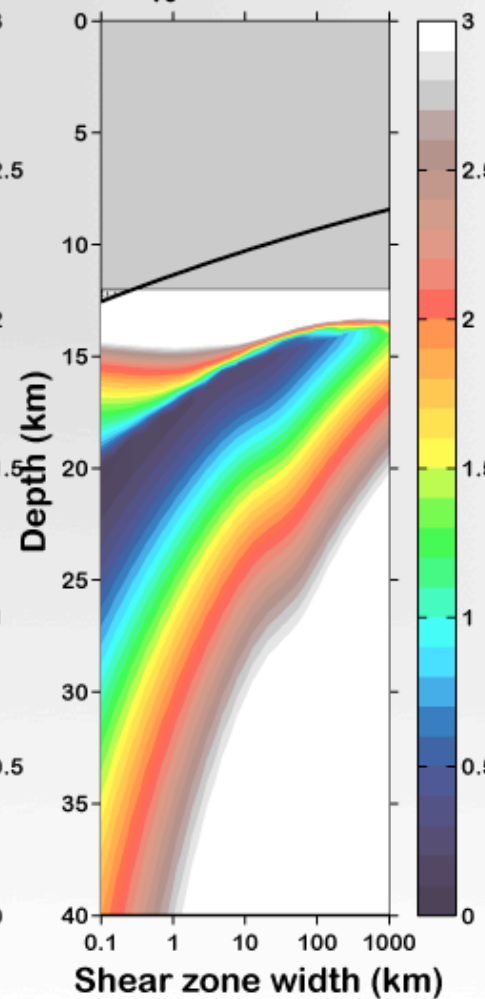
95% Fd, 05% Bi

Constant rate
 $\log_{10}(\text{velocity ratio})$

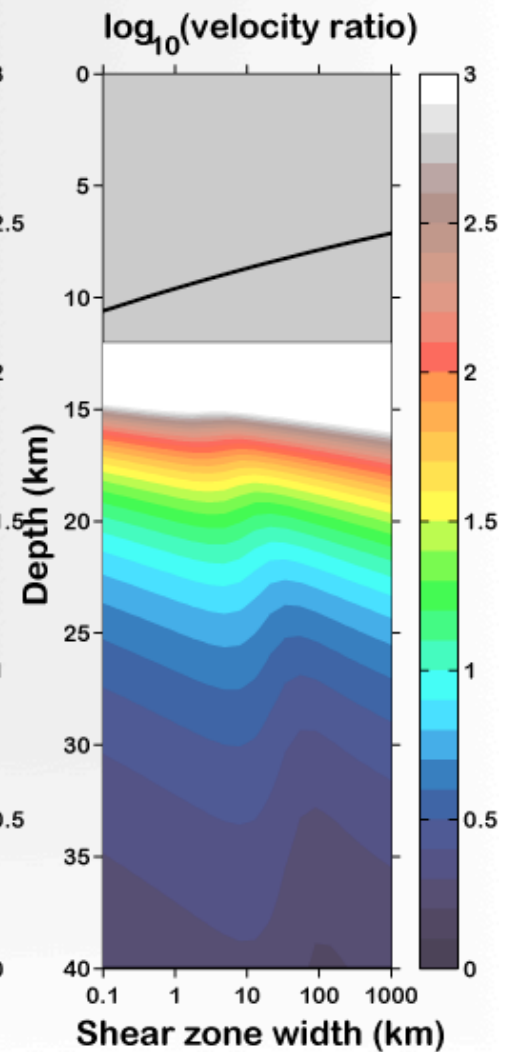


95% Fd, 05% Bi

Constant stress
 $\log_{10}(\text{velocity ratio})$

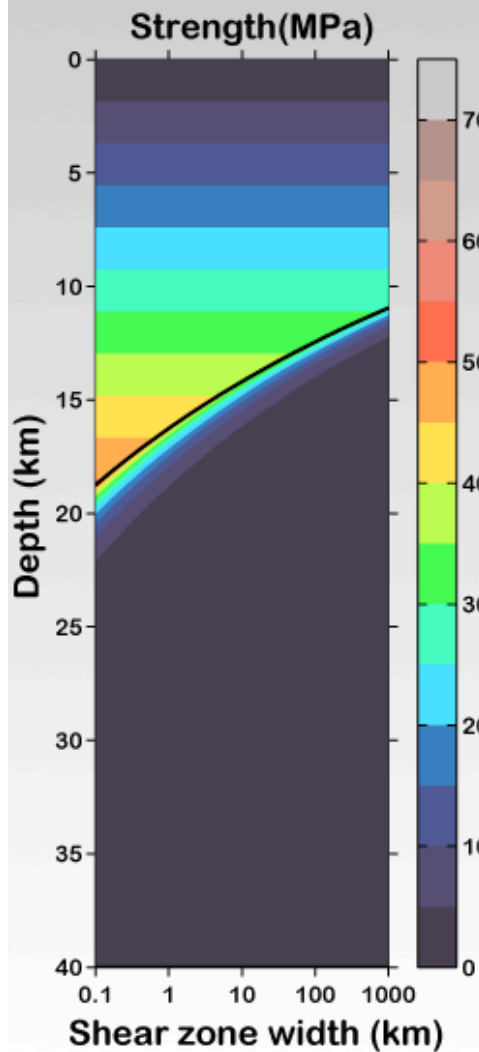


100% Biotite



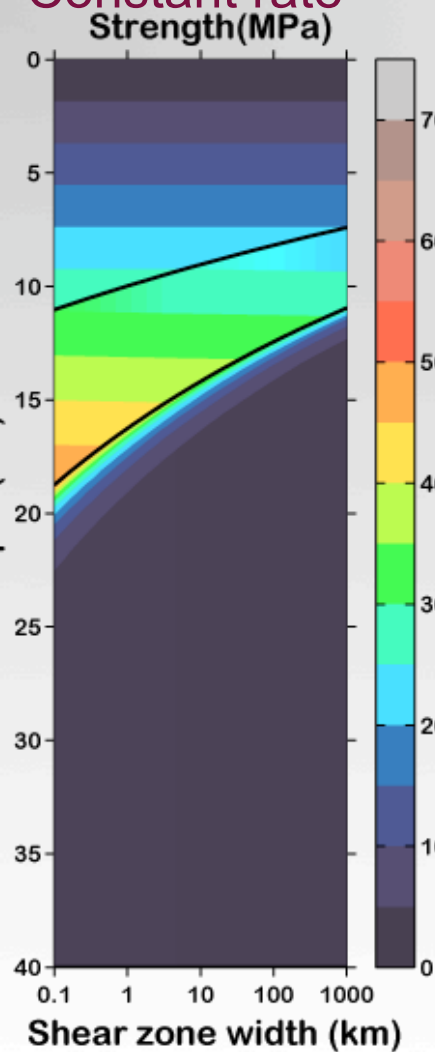
Effect of fabric ($10\mu\text{m}$ grain size)

100% Feldspar



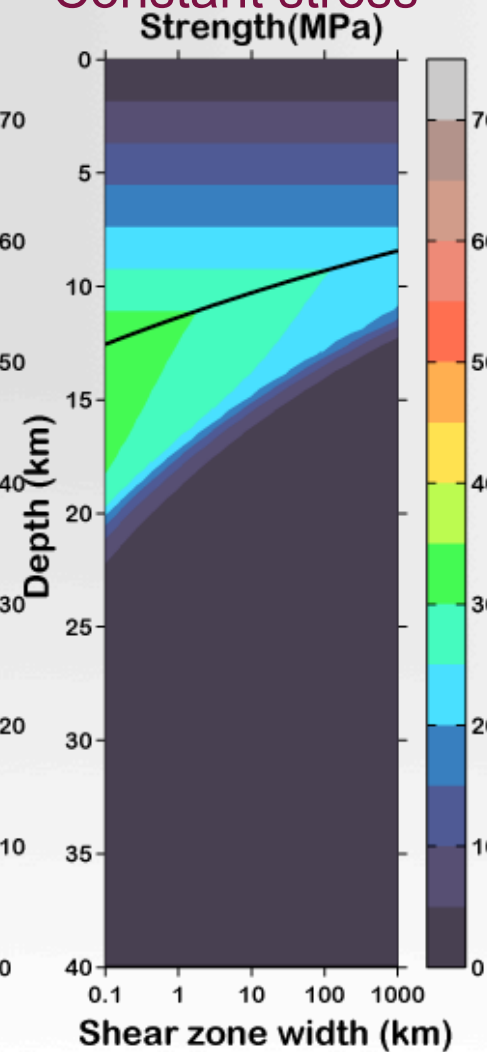
95% Fd, 05% Bi

Constant rate

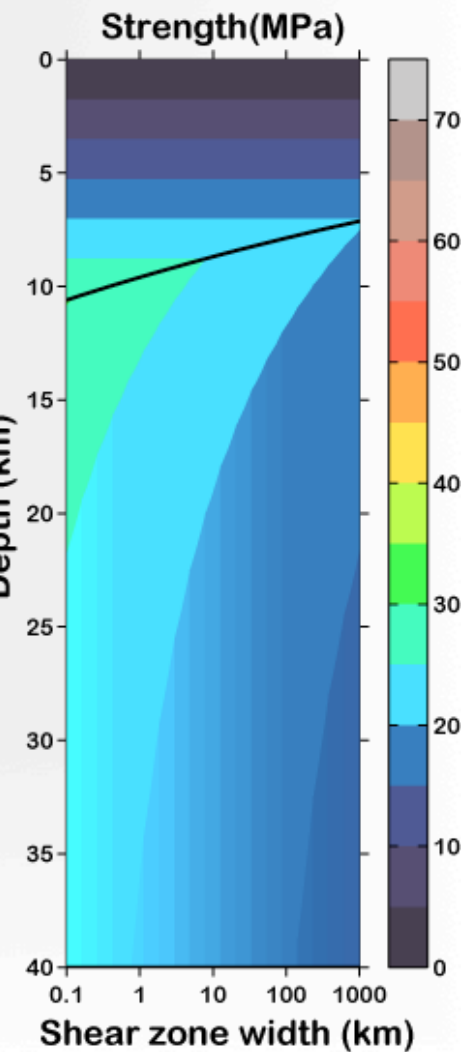


95% Fd, 05% Bi

Constant stress

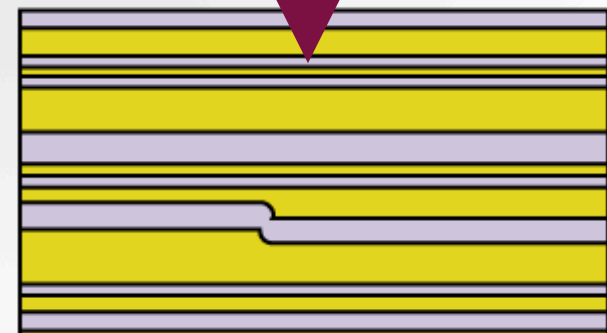
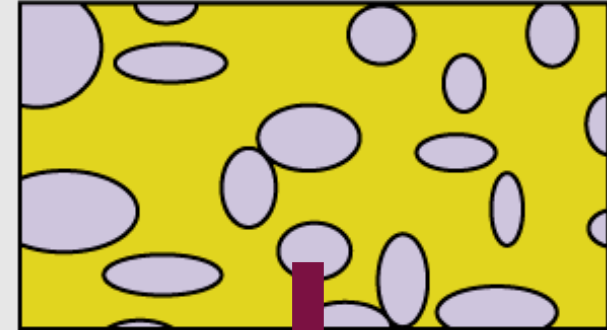


100% Biotite

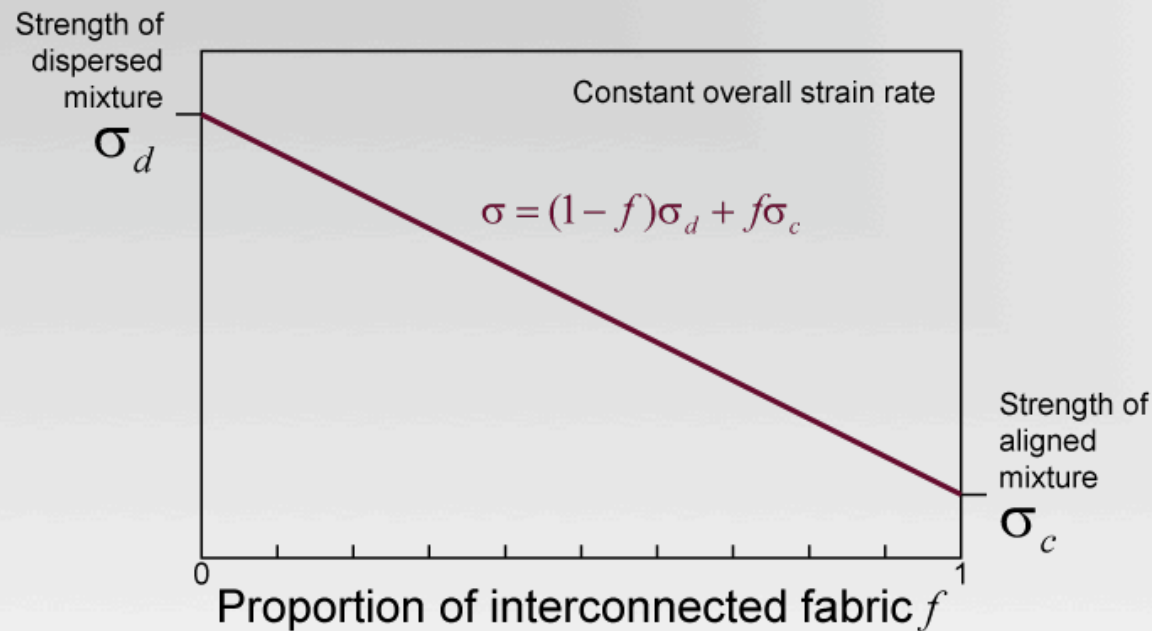


Mixture Model

Protolith



Shear zone

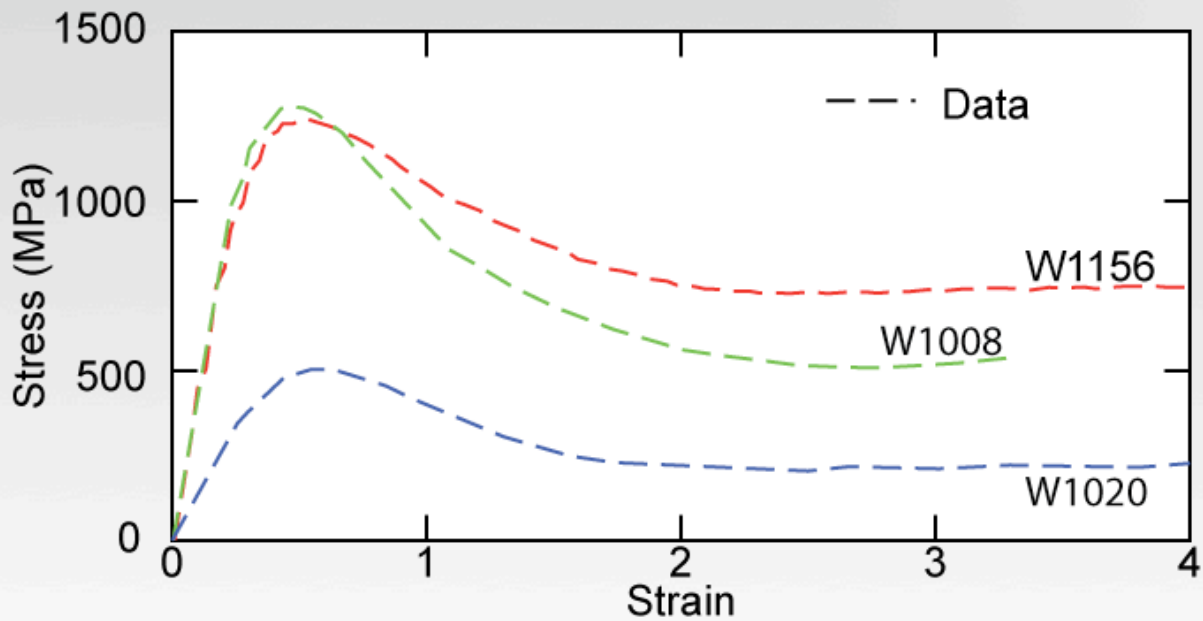


Interconnected: $\dot{\epsilon} = (1-C)A_a\sigma_c^{n_a} + CA_b\sigma_c^{n_b}$

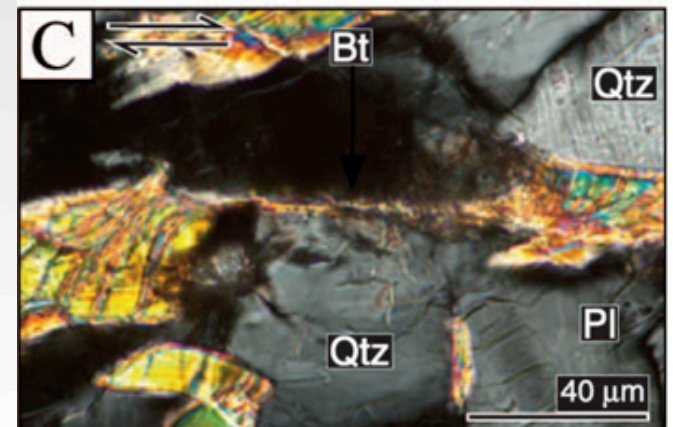
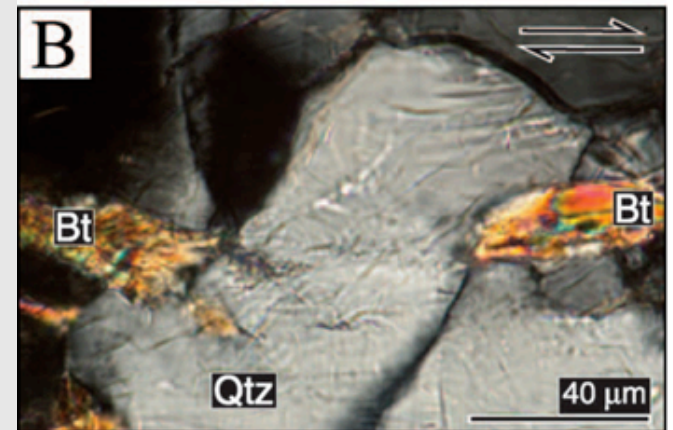
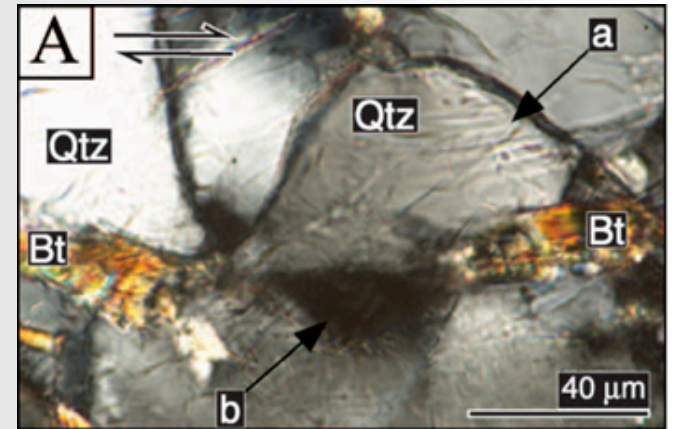
Dispersed: $\sigma_d = (1-C)(\dot{\epsilon}/A_a)^{1/n_a} + C(\dot{\epsilon}/A_b)^{1/n_b}$

Foliation Development

- Lab experiments on Gneiss Minuti
- Cracking of quartz and feldspar grains between biotite



Holyoke and Tullis, 2006



Fabric evolution

- Two-level mixing rheology

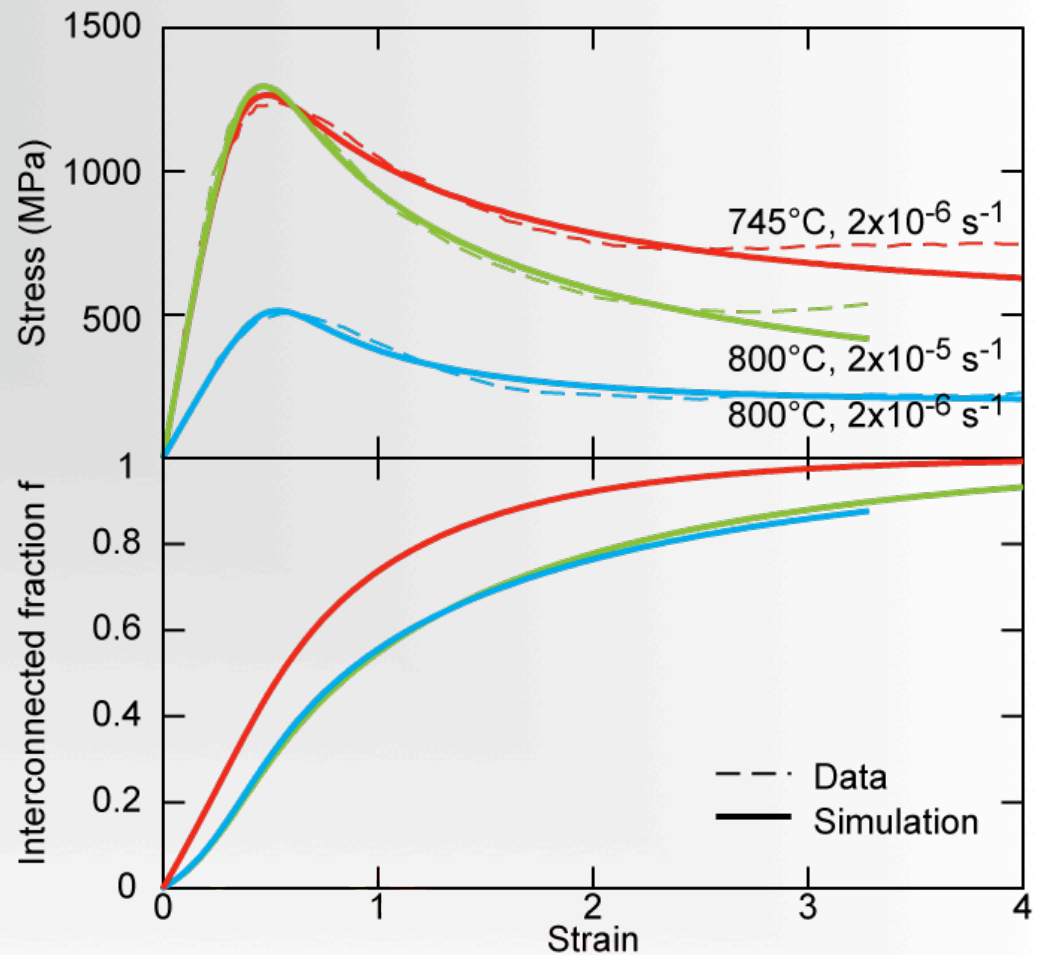
$$\sigma = (1 - f)\sigma_d + f\sigma_c$$

- Elastic loading

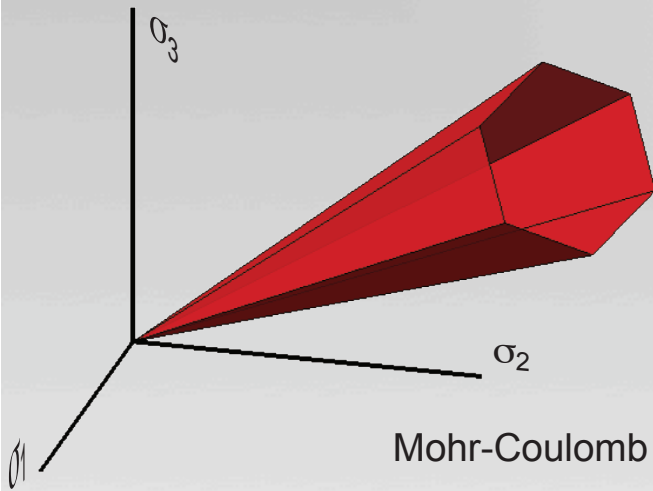
$$d\sigma/dt = KH(\epsilon_p - \dot{\epsilon}_s)$$

- Connection rate linked to probability of failure

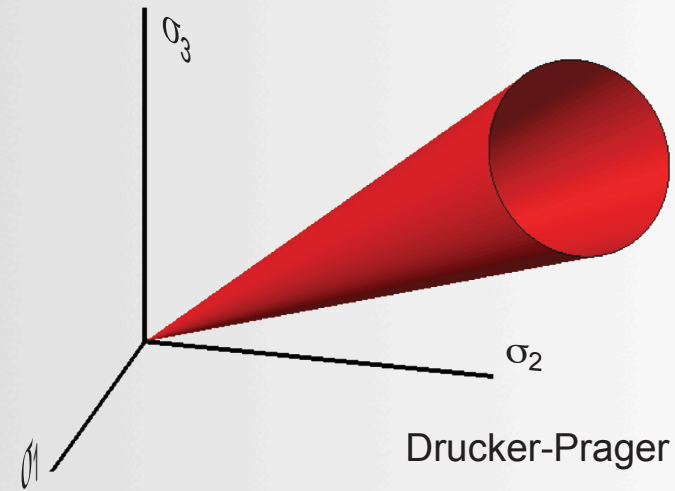
$$\frac{df}{d\epsilon} = R(1 - f) \frac{1}{2} \left[1 + \operatorname{erf} \left(\frac{\sigma - \sigma_y}{\chi\sqrt{2}} \right) \right]$$



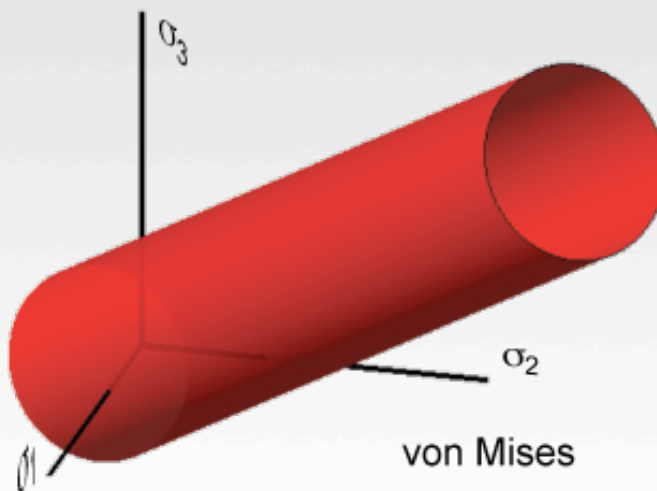
Yield surfaces



Fault surfaces

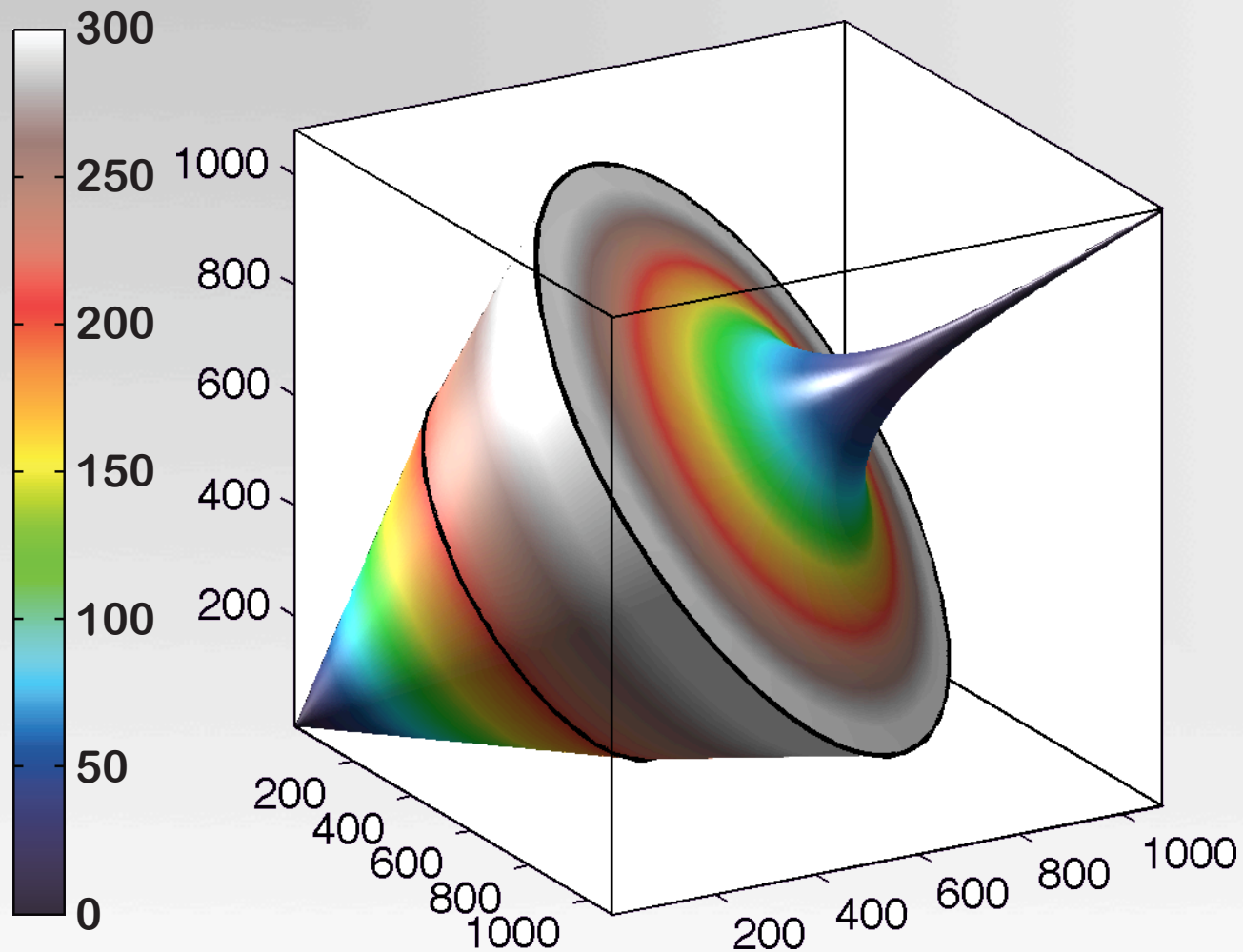


Fault continuum (in PyLith)



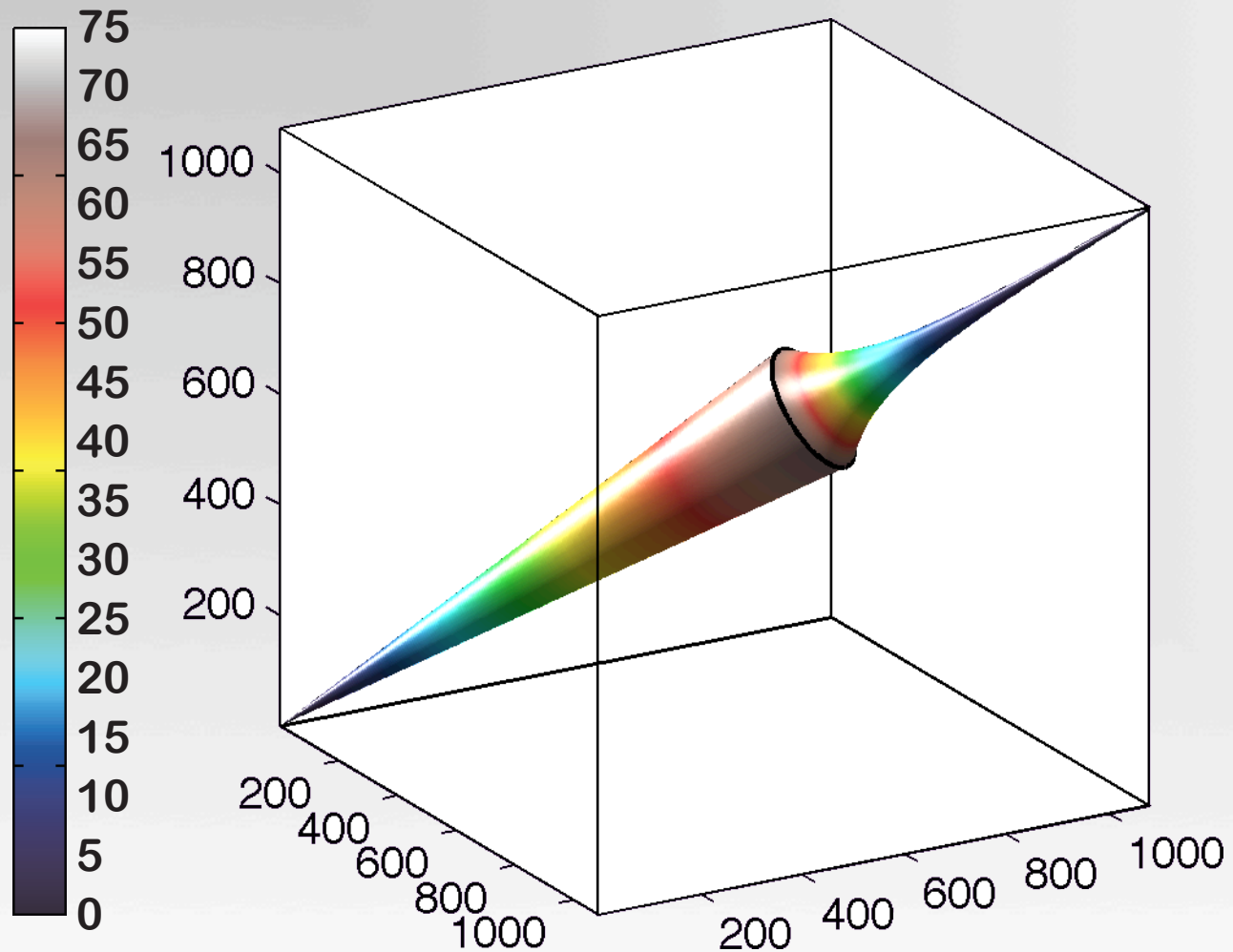
For plasticity
(depends on Temperature,
environment, strain rate)

3D yield envelope (standard)



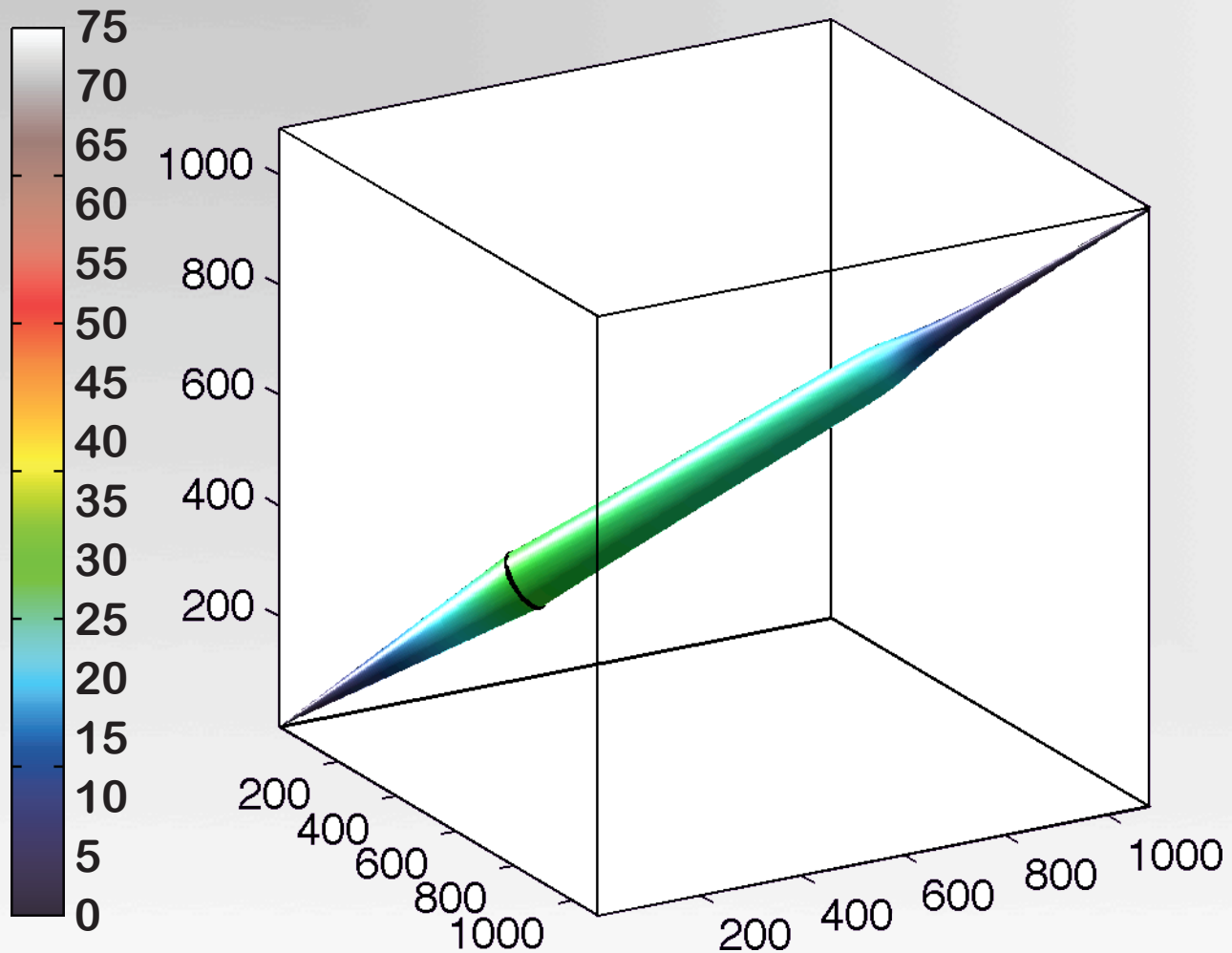
- Byerlee's law
- Feldspar dislocation creep

3D yield envelope (reduced friction)



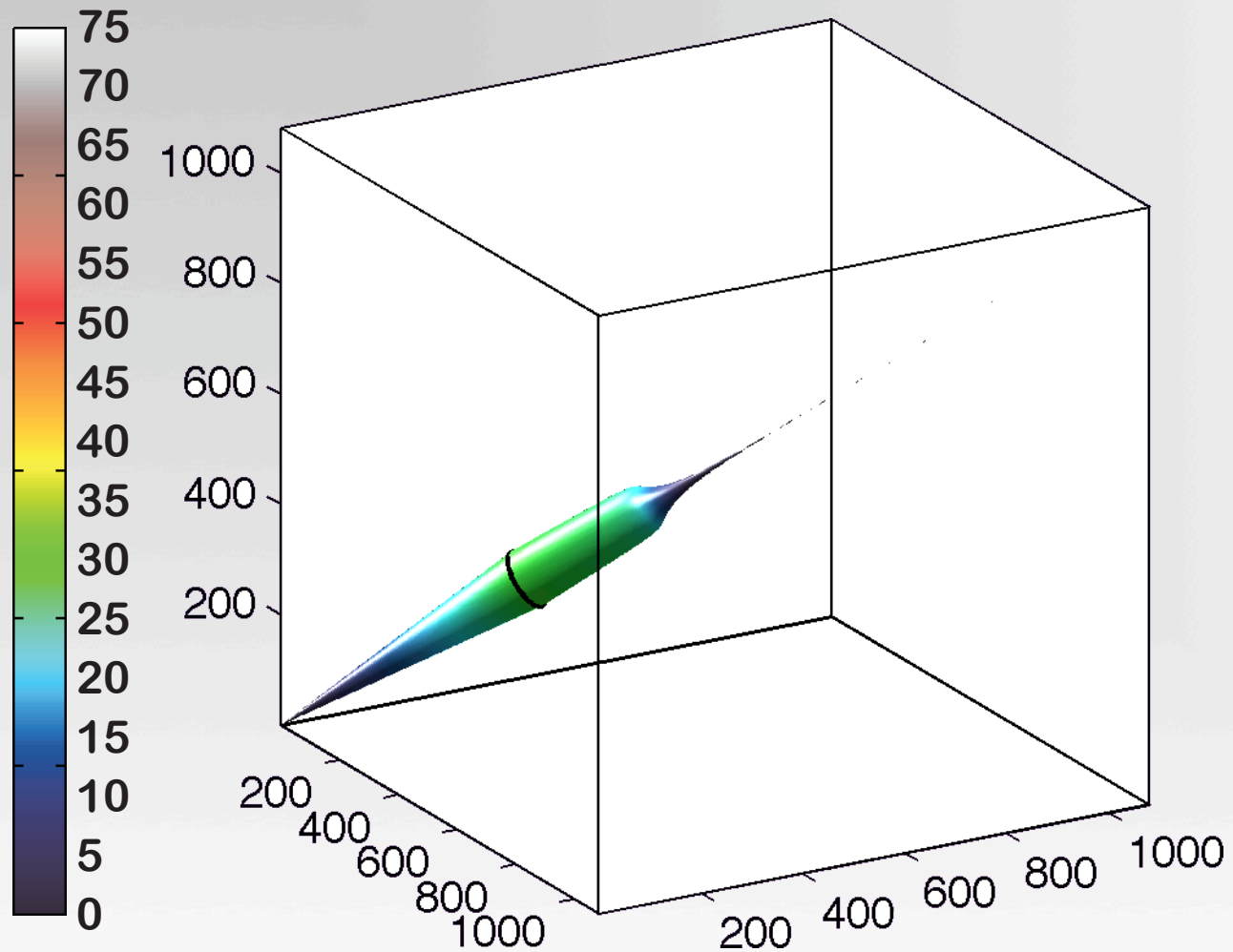
- Friction with $f=0.1$
- Feldspar dislocation creep

3D yield envelope (include mica)



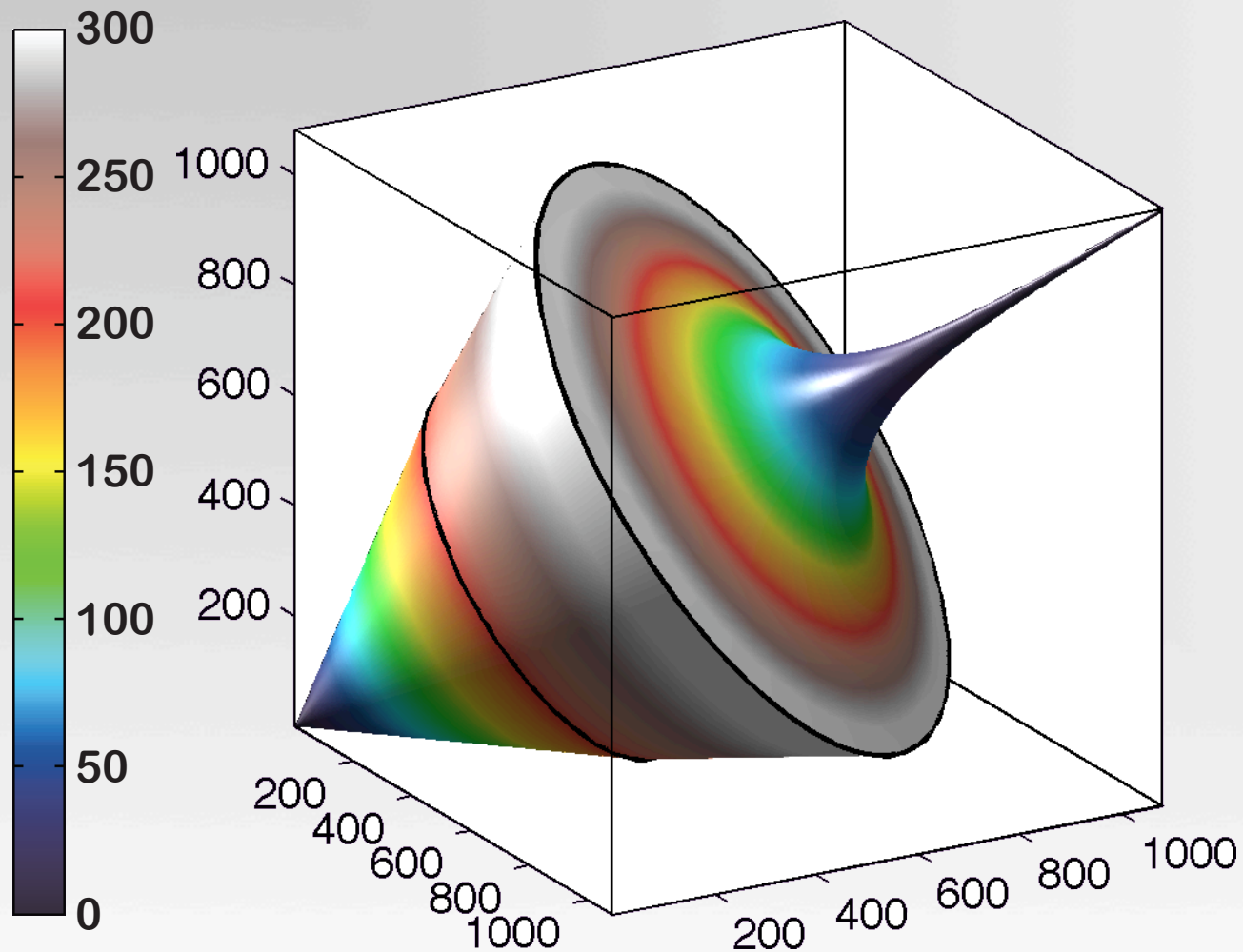
- Friction with $f=0.1$
- 95% Feldspar dislocation creep
- 5% Biotite
- Constant stress mixing

3D yield envelope (reduce grain size)



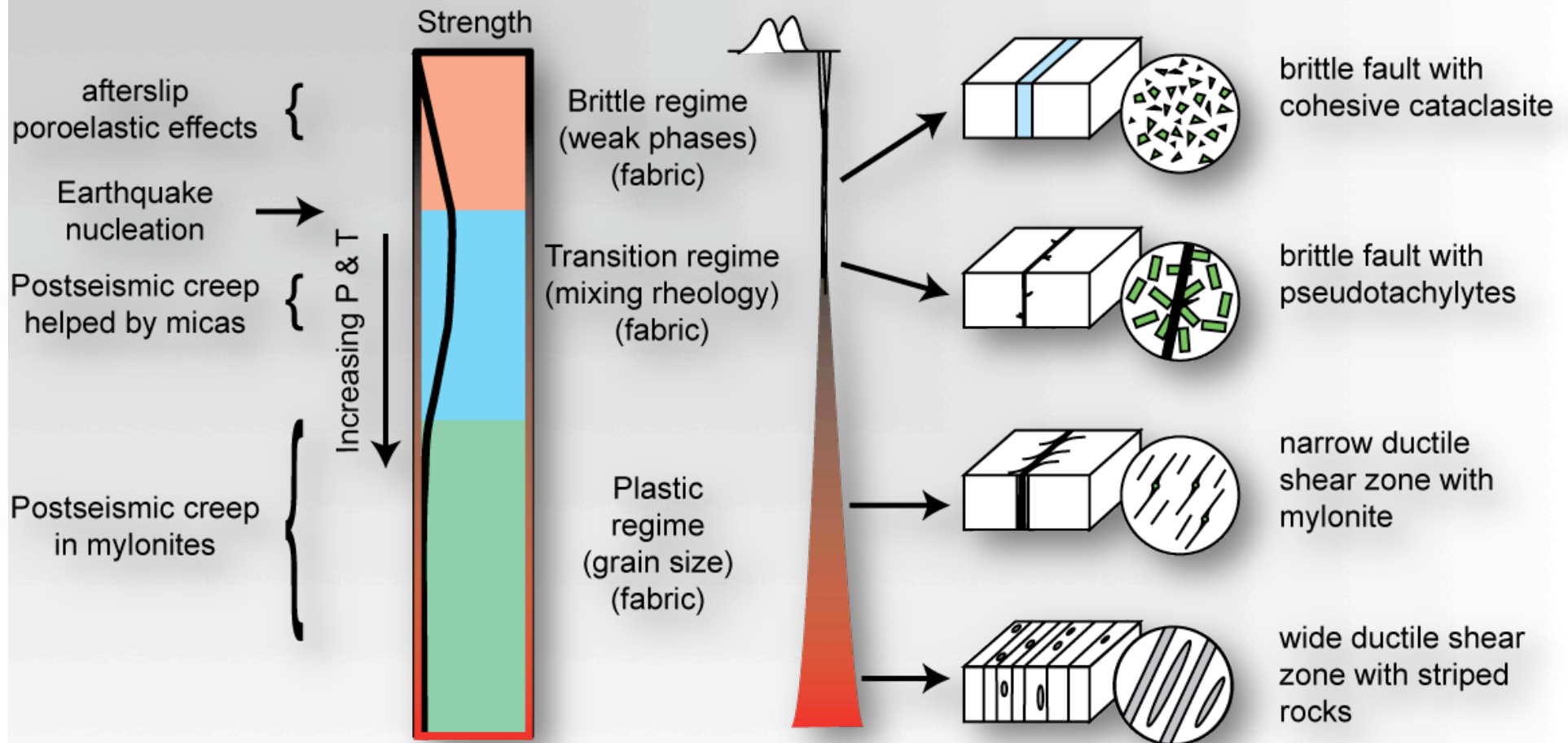
- Friction with $f=0.1$
- 95% Feldspar diffusion and dislocation creep with $10\mu\text{m}$ grain size
- 5% Biotite
- Constant stress mixing

3D yield envelope (standard)



- Byerlee's law
- Feldspar dislocation creep

A weaker view of the crust...



Modified from Passchier & Trouw 1998