

#### **I. Introduction**

sic approach, we adopt a simple kinematic backslip model | that is taken from our existing network in Chile/Peru. (Savage, 1983). This study differs from most (but not all - e.g., see Segall, 2002) analogous studies in that we use **3. Plate Interface Geometry** a Bayesian approach wherein we ask not for a single optimum model, but rather for a posteriori estimates of the range of allowable model parameters. This approach also allows us to explicitly define physically plausible a priori information on data uncertainties and model parameters, as opposed to assuming everything follows Gaussian sta-

The Bayesian approach inherently depends on an ability to routinely compute millions of forward models that are consistent with a priori constraints and available geodetic measurements. Such computations are now viable with available computational resources. We apply this methodology to invert for a series of synthetic cases motivated by the desire to understand the state of inter-seismic coupling in the Chilean-Peruvian subduction margin between 16 and 24 S.







ocation of CTO (Caltech Tectonics oservatory) continuous GPS sites inalled beginning 2005 and sites installed IPGP. The picture is for PTRE.

#### **(2. cGPS measurements (cont)**

Our primary goal is to characterize the extent of apparent | GPS data will provide constraints for the inter-seismic velocity he coupled zone is defined by its upper and lower boundaries, We generate synthetic data (with noise) using the model plate coupling on the subduction zone megathrust with the field. Continuous GPS (cGPS) measurements can provide preeach parameterized using cubic splines. The knots of these splines in panel (a), where the upper and lower boundaries of eventual goal of understanding variations in fault zone rheare our model parameters along with the background plate velocology. In this initial study, in order to demonstrate the barepresent the depths of the coupling zone boundaries. For a given synthetic data using all 3 components of the GPS data (see model we define a mask for depth (see hatched area in the figure) panel b) as well as only the horizontal components (see



3D triangulated surface modeling the plate interface between the Nazca and South American plates. The surface is obtained using earthquake catalogs of relocated seismicity (ISC, Eng- 6. A priori information dahl and Villaseñor, etc), seismic reflection profiles (ANCORP || Typically, with a Bayesian approach one can easily implement plate interface.



We use a Back-slip model (Savage, 1983) to represent the inter-seismic strain accumulation at the plate interface. In this initial approach we use a constant back-slip at the coupled zone ignoring the possible existence of a transition zone. We assume an elastic half space (Okada, 1985) in order to calculate Greens functions.

# **A Bayesian Approach for Inter-plate Coupling Models in Subduction Zones**

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### **4. Model Parameterization (cont)**



#### **5. Inverse Method**

We implement a Markov Chain Monte Carlo, Metropolis - Hastings (1970) algorithm for the inversion. The algorithm samples Triangulated surface fitted the a-posteriori probability density function of the parameters of the model:  $s_a V_{Nz_N}$ ,  $s_a V_{Nz_E}$  (components of the plate velocity vector), DL, and DU, (i-th knot of the splines defining the lower and upper boundary of the inter-seismic interplate coupled zone, respectively).

Lines; Krabbenhoft et al 2004(shown here); etc) and any other a-priori constraints such as limiting the range of any given patype of data that can be used to constrain the geometry of the rameter. In our case, the entire coupled zone must lie between seafloor (trench) depth and a maximum depth (80 km in our case). In the absence of data and any other constrains, the a-priori PDF for each knot would be a boxcar function. However, an advantage of the Bayesian approach, lies in that we can also describe a-priori information in terms of relationships (or rules) between parameters. For instance, with the coupled zone parameterization described above (4), the upper boundary must by definition always be above the lower boundary (e.g.:  $DU_i \leq DL_i$ ). The net impact of such a constraint, is that even in the absence of data, the prior distribution on the upper and lower boundary is not flat (or a boxcar). In our case, the resulting priors are triangular in shape.





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### **7a. Inversion with synthetic data**

and 50 km respectively. We perform inversions using this and we calculate the for- panel c). We show the a-posteriori PDF of the model paward model using only rameters for the upper boundary (blue) and lower boundthe Green's functions that ary (red) of the coupled zone compared to input model corresponds to triangular (black). Note how the uncertainties of the lower bound fault patches within the ary increase substantially when we invert without using the vertical component of the GPS data.

# **7b. Inversion with synthetic data**

We perform a checkerboard style test inverting the synthetic data shown in panel (a), where the black shaded area indicates the locked region. The results of the inversion are shown in panel (b).

Note that the target model is being predicted by the inversion process at the region where the GPS network is ||plify the problem and for computational expediency. densest (0 km < N < 200 km). Also notice that since shown here, only the a-priori probability density function is recovered at the edges of the model (N=-400 km and N=1000 km).

#### a) Synthetic Model and GPS Data





The uncertainty of the model parameters have a high dependence on the spatial distribution of the GPS network. This dependence becomes clear analyzing the a-posteri- Slip Rate on the San Andreas Fault System". International Geori probability density functions of the parameters of the ology Review, Vol.44, 2002, p.62-82. model. This perspective can help when planning deployment of new instruments.









**b)** Inversion using 3 components (E,N,U) of GPS stations

# **8. What is next?**

We are building a Bayesian inversion environment that allow us to estimate the range of allowable parameters in geodetic fault models. In particular, we have focussed on inter-plate coupling in subduction zones.

At present, we have made many assumptions to both sim-

there is no data at the edges of the model, for all tests Moving to more complicated elastic structures will be trivial as it simply requires building a bank of Green's | | functions from a finite element code (e.g., PyLith). (Question: When will PyLith be able to do this efficiently?!) Similarly, we can easily expand the complexity of the parameterization to include transition zones and resolve for the Euler vector instead of the background plate velocity. This increase in number of model parameters will result on a greater computational burden that can be offset by use of a parallel sampler.

> Our immediate near term goal is to apply this approach to available campaign and continuous GPS observations for Northern Chile and Southern Peru.

Eventually, we expect to apply this Bayesian approach not simply to kinematic models (e.g., backslip) but to models parameterized in terms of spatially variable fault zone rheological constants.

# 9. Acknowlegdement

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# **10. References**

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