

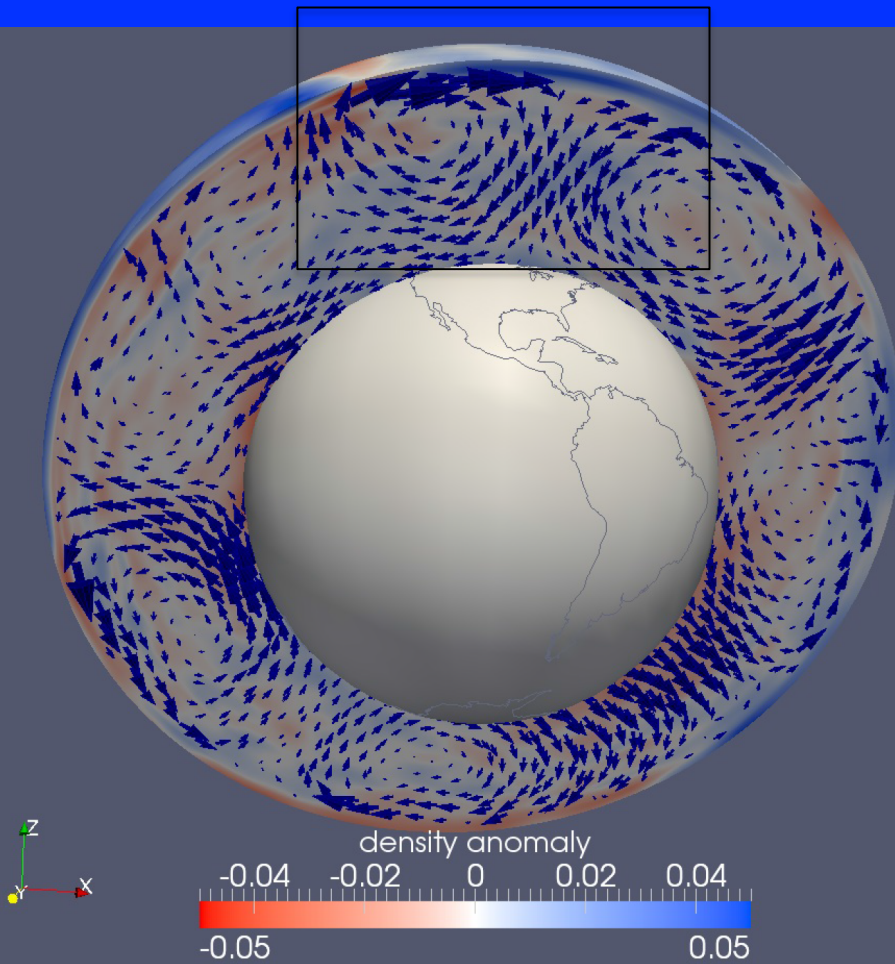
Dynamics of Lithosphere-Mantle Coupling: Global Stress and Plate Motions

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Global Modeling of Lithosphere Stress and Plate Motion

- What is the total stress energy in the plate tectonic system?
- How much arises from GPE of the lithosphere and how much from coupling with mantle?
- What are the implications for strength profiles and possible role of weakening mechanisms?
- Calibration of present-day forces places important constraints on models that address geologic time scale evolution with feedbacks

Force Balance Equations in spherical coordinates

$$\frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} (r^2 \sigma_{\varphi\varphi}) + \frac{1}{\cos^2\theta} \frac{\partial}{\partial\theta} (r^2 \sigma_{\varphi\theta} \cos^2\theta) + \frac{\partial}{\partial r} (r^3 \sigma_{\varphi r}) = 0 \quad (1)$$

$$\begin{aligned} \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} (r^2 \sigma_{\varphi\theta}) + \frac{1}{2} \frac{\partial}{\partial\theta} (r^2 [\sigma_{\theta\theta} + \sigma_{\varphi\varphi}]) \\ + \frac{1}{2\cos^2\theta} \frac{\partial}{\partial\theta} (r^2 \cos^2\theta [\sigma_{\theta\theta} - \sigma_{\varphi\varphi}]) \\ + \frac{\partial}{\partial r} (r^3 \sigma_{\theta r}) = 0 \end{aligned} \quad (2)$$

$$\begin{aligned} \frac{1}{r\cos\theta} \frac{\partial\sigma_{\varphi r}}{\partial\varphi} + \frac{1}{r\cos\theta} \frac{\partial}{\partial\theta} (\cos\theta \sigma_{\theta r}) + \frac{1}{r} (2\sigma_{rr} - \sigma_{\varphi\varphi} - \sigma_{\theta\theta}) \\ + \frac{\partial\sigma_{rr}}{\partial r} - \rho g = 0 \end{aligned} \quad (3)$$

Vertically integrating (1) and (2) and substituting: $\sigma_{ij} = \tau_{ij} + \frac{1}{3} \sigma_{kk} \delta_{ij}$

$$\begin{aligned}
 & \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right) - \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{rr} \mathbf{dr} \right) \\
 & \quad + \frac{1}{\cos^2\theta} \frac{\partial}{\partial\theta} \left(\cos^2\theta \int_{r_L}^{r_0} r^2 \tau_{\varphi\theta} \mathbf{dr} \right) \\
 & = - \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \sigma_{rr} \mathbf{dr} \right) - r_0^3 \tau_{\varphi r}(r_0) + r_L^3 \tau_{\varphi r}(r_L) \quad (4)
 \end{aligned}$$

and

$$\begin{aligned}
 & \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{\varphi\theta} \mathbf{dr} \right) + \frac{1}{2} \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \tau_{\theta\theta} \mathbf{dr} + \int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right) \\
 & \quad + \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \tau_{rr} \mathbf{dr} \right) \\
 & \quad + \frac{1}{2\cos^2\theta} \frac{\partial}{\partial\theta} \left(\cos^2\theta \left[\int_{r_L}^{r_0} r^2 \tau_{\theta\theta} \mathbf{dr} - \int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right] \right) \\
 & = - \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \sigma_{rr} \mathbf{dr} \right) - r_0^3 \tau_{\theta r}(r_0) + r_L^3 \tau_{\theta r}(r_L) \quad (5)
 \end{aligned}$$

[8] The approximation that we make, which could be called the approximation that underlies the “thin sheet” approach, is that the gradients of $\sigma_{\varphi r}$ and $\sigma_{\theta r}$ in equation (3) are negligibly small as is the term $\frac{1}{r} (2\sigma_{rr} - \sigma_{\varphi\varphi} - \sigma_{\theta\theta})$ compared to ρg . Hence, equation (3) can be approximated as

$$\sigma_{rr} = - \int_r^{r_0} \rho g dr, \quad (6)$$

so that the GPE equation is given by

$$\begin{aligned} \int_{r_L}^{r_0} r^2 \sigma_{rr} dr &= - \int_{r_L}^{r_0} r^2 \left[\int_r^{r_0} \rho g dr' \right] dr \\ &= - \int_{r_L}^{r_0} \rho g \left[\int_{r_L}^{r'} r^2 dr \right] dr' \\ &= - \int_{r_L}^{r_0} \frac{1}{3} \rho g (r'^3 - r_L^3) dr' \end{aligned} \quad (7)$$

Global Modeling of Lithosphere Stress and Plate Motion

- Lithosphere calculations:
 - Depth integrated 3-D force balance equations in a lithosphere shell
 - Solved using finite element global method
 - Weak formulation
 - Higher order elements in quadrilateral grid (Code written by A.J. Haines)
 - Internal body forces (GPE), and basal traction boundary conditions (Mantle Convection)

Method Applied Regionally and Globally

- **Applied to Western U.S. and Central Asia without basal tractions:**

- Flesch, L. M., W. E. Holt, A. J. Haines, and B. Shen-Tu (2000), The dynamics of the Pacific-North America plate boundary zone in the Western U. S., *Science*, 287, 834-836, 2000.
- Flesch, L.M., Haines, A. J., and W. E. Holt (2001), The dynamics of the India-Eurasia Collision Zone, *J. Geophys. Res.*, 106, 16,435-16,460, 2001.

- **Applied globally with contribution from lithosphere only:**

- Ghosh, A., W. E. Holt, and L. M. Flesch (2009), Contribution of Gravitational Potential Energy Differences to the Global Stress Field, *Geophys. Jour. Int.*, doi: 10.1111/j.1365-246X.2009.04326.x

- **Applied globally with mantle flow and lithosphere contributions:**

- Ghosh, A., W. E. Holt, L. Wen, A. J. Haines, and L. M. Flesch (2008), Joint modeling of lithosphere and mantle dynamics elucidating lithosphere-mantle coupling, *Geophys. Res. Lett.*, 35, L16309, doi:10.1029/2008GL034365
- Ghosh, A., and W. E. Holt (2012), Plate Motions and Stresses from Global Dynamic Models (2012), *Science*, 335, doi:10.1126/science.1214209,
- Ghosh, A., W. E. Holt, and L. M. Wen (2013), Predicting the lithospheric stress field and plate motions by joint modeling of lithosphere and mantle dynamics, *J. Geophys. Res: Solid Earth*, 118, doi:10.1029/2012JB009516.

Vertically integrating (1) and (2) and substituting: $\sigma_{ij} = \tau_{ij} + \frac{1}{3} \sigma_{kk} \delta_{ij}$

$$\begin{aligned} & \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right) - \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{rr} \mathbf{dr} \right) \\ & \quad + \frac{1}{\cos^2\theta} \frac{\partial}{\partial\theta} \left(\cos^2\theta \int_{r_L}^{r_0} r^2 \tau_{\varphi\theta} \mathbf{dr} \right) \\ & = - \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \sigma_{rr} \mathbf{dr} \right) - r_0^3 \tau_{\varphi r}(r_0) + r_L^3 \tau_{\varphi r}(r_L) \quad (4) \end{aligned}$$

and

$$\begin{aligned} & \frac{1}{\cos\theta} \frac{\partial}{\partial\varphi} \left(\int_{r_L}^{r_0} r^2 \tau_{\varphi\theta} \mathbf{dr} \right) + \frac{1}{2} \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \tau_{\theta\theta} \mathbf{dr} + \int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right) \\ & \quad + \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \tau_{rr} \mathbf{dr} \right) \\ & \quad + \frac{1}{2\cos^2\theta} \frac{\partial}{\partial\theta} \left(\cos^2\theta \left[\int_{r_L}^{r_0} r^2 \tau_{\theta\theta} \mathbf{dr} - \int_{r_L}^{r_0} r^2 \tau_{\varphi\varphi} \mathbf{dr} \right] \right) \\ & = - \frac{\partial}{\partial\theta} \left(\int_{r_L}^{r_0} r^2 \sigma_{rr} \mathbf{dr} \right) - r_0^3 \tau_{\theta r}(r_0) + r_L^3 \tau_{\theta r}(r_L) \quad (5) \end{aligned}$$

Minimize Functional, I , with respect to Lagrange multipliers

$$\begin{aligned}
 I = & \iint \frac{1}{\mu} \left[\bar{\tau}_{\varphi\varphi}^2 + 2\bar{\tau}_{\varphi\theta}^2 + \bar{\tau}_{\theta\theta}^2 + (\bar{\tau}_{\varphi\varphi} + \bar{\tau}_{\theta\theta})^2 \right] \cos\theta d\varphi d\theta \\
 & + \iint \left\{ 2\lambda_\varphi \left[\frac{1}{\cos\theta} \frac{\partial \bar{\tau}_{\varphi\varphi}}{\partial \varphi} + \frac{1}{\cos\theta} \frac{\partial}{\partial \varphi} (\bar{\tau}_{\varphi\varphi} + \bar{\tau}_{\theta\theta}) \right. \right. \\
 & \left. \left. + \frac{1}{\cos^2\theta} \frac{\partial}{\partial \theta} (\cos^2\theta \bar{\tau}_{\varphi\theta}) + \frac{1}{\cos\theta} \frac{\partial \bar{\sigma}_{rr}}{\partial \varphi} - r_L^3 \sigma_{\varphi r}(r_L) \right] \right. \\
 & + 2\lambda_\theta \left[\frac{1}{\cos\theta} \frac{\partial \bar{\tau}_{\varphi\theta}}{\partial \varphi} + \frac{3}{2} \frac{\partial}{\partial \theta} (\bar{\tau}_{\theta\theta} + \bar{\tau}_{\varphi\varphi}) \right. \\
 & \left. + \frac{1}{2\cos^2\theta} \frac{\partial}{\partial \theta} (\cos^2\theta [\bar{\tau}_{\theta\theta} - \bar{\tau}_{\varphi\varphi}]) \right. \\
 & \left. \left. + \frac{\partial \bar{\sigma}_{rr}}{\partial \theta} - r_L^3 \sigma_{\theta r}(r_L) \right] \right\} \cos\theta d\varphi d\theta
 \end{aligned}$$

Relation between deviatoric stress and Lagrange multipliers

$$\bar{\tau}_{\varphi\varphi} = \mu \left(\frac{1}{\cos\theta} \frac{\partial\lambda_{\varphi}}{\partial\varphi} - \lambda_{\theta}\tan\theta \right),$$

$$\bar{\tau}_{\theta\theta} = \mu \frac{\partial\lambda_{\theta}}{\partial\theta},$$

$$\bar{\tau}_{\varphi\theta} = \frac{\mu}{2} \left(\frac{\partial\lambda_{\varphi}}{\partial\theta} + \frac{1}{\cos\theta} \frac{\partial\lambda_{\theta}}{\partial\varphi} + \lambda_{\varphi}\tan\theta \right).$$

Relation with deviatoric stress and Lagrange multipliers is the same as the relation between strain rate and velocities

Lagrange multipliers are zero along the boundaries (circular rings at 88° N, 88° S)

Substitute expressions in for deviatoric stress and minimize J functional with respect to Lagrange multipliers. This provides solution to force balance equations.

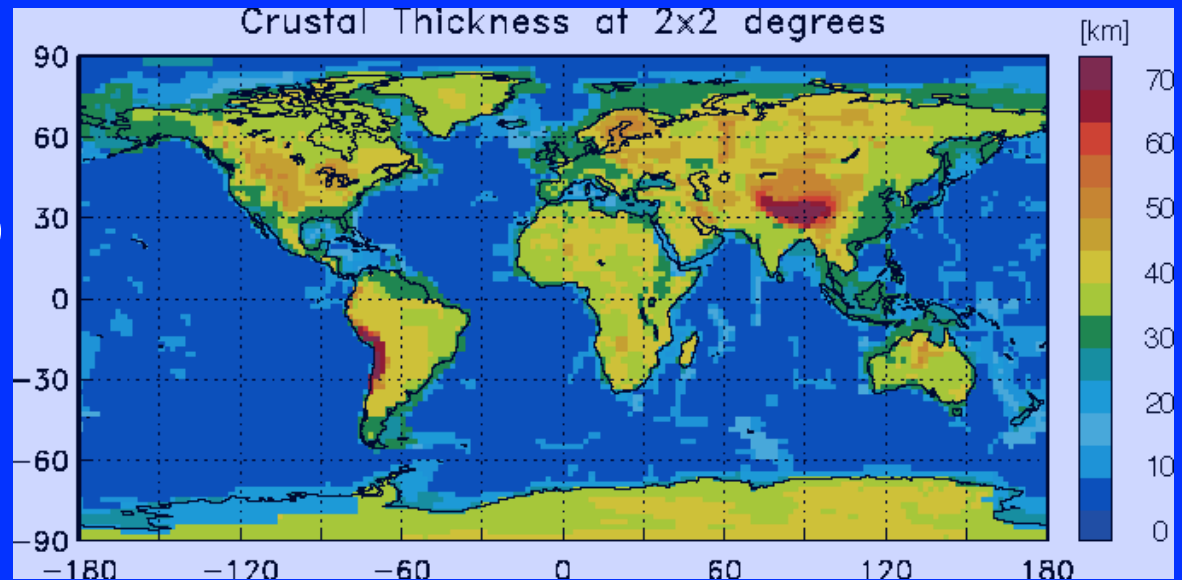
$$J = \iint \left\{ \left[\begin{pmatrix} \bar{\tau}_{\varphi\varphi} \\ \bar{\tau}_{\theta\theta} \\ \bar{\tau}_{\varphi\theta} \end{pmatrix} - \begin{pmatrix} \Phi_{\varphi\varphi}^{obs} \\ \Phi_{\theta\theta}^{obs} \\ \Phi_{\varphi\theta}^{obs} \end{pmatrix} \right]^T \right. \\ \left. \tilde{V}^{-1} \left[\begin{pmatrix} \bar{\tau}_{\varphi\varphi} \\ \bar{\tau}_{\theta\theta} \\ \bar{\tau}_{\varphi\theta} \end{pmatrix} - \begin{pmatrix} \Phi_{\varphi\varphi}^{obs} \\ \Phi_{\theta\theta}^{obs} \\ \Phi_{\varphi\theta}^{obs} \end{pmatrix} \right] \right\} \cos\theta d\varphi d\theta.$$

The potentials are composed of horizontal integrals of the body force equivalents

Constraints for Effective Forces

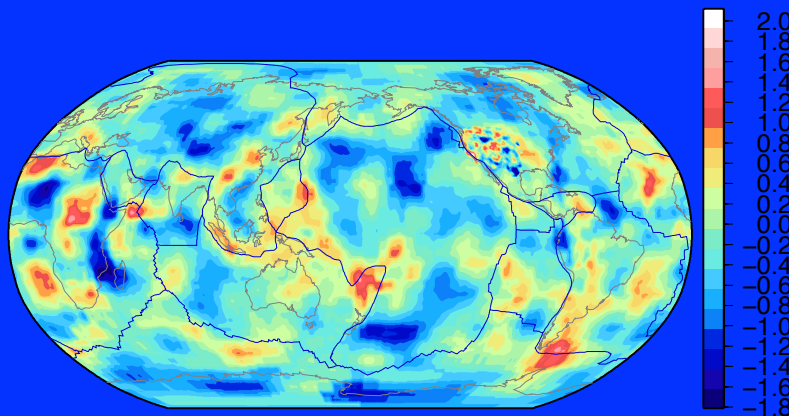
Density structure:

- Crust 2.0 in lithosphere; also cooling plate model [Stein & Stein, 1992].

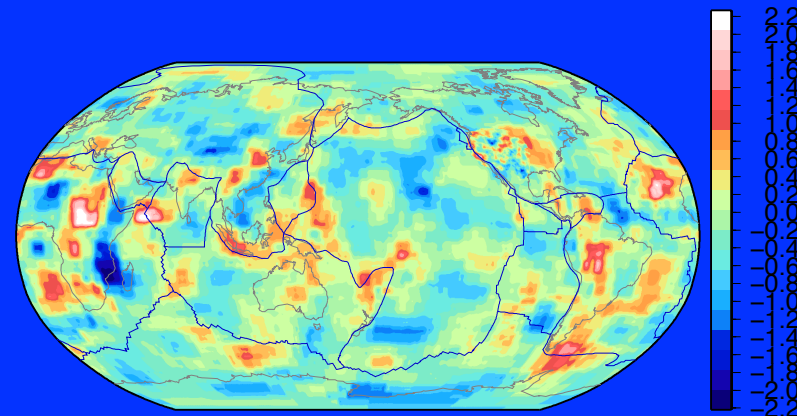


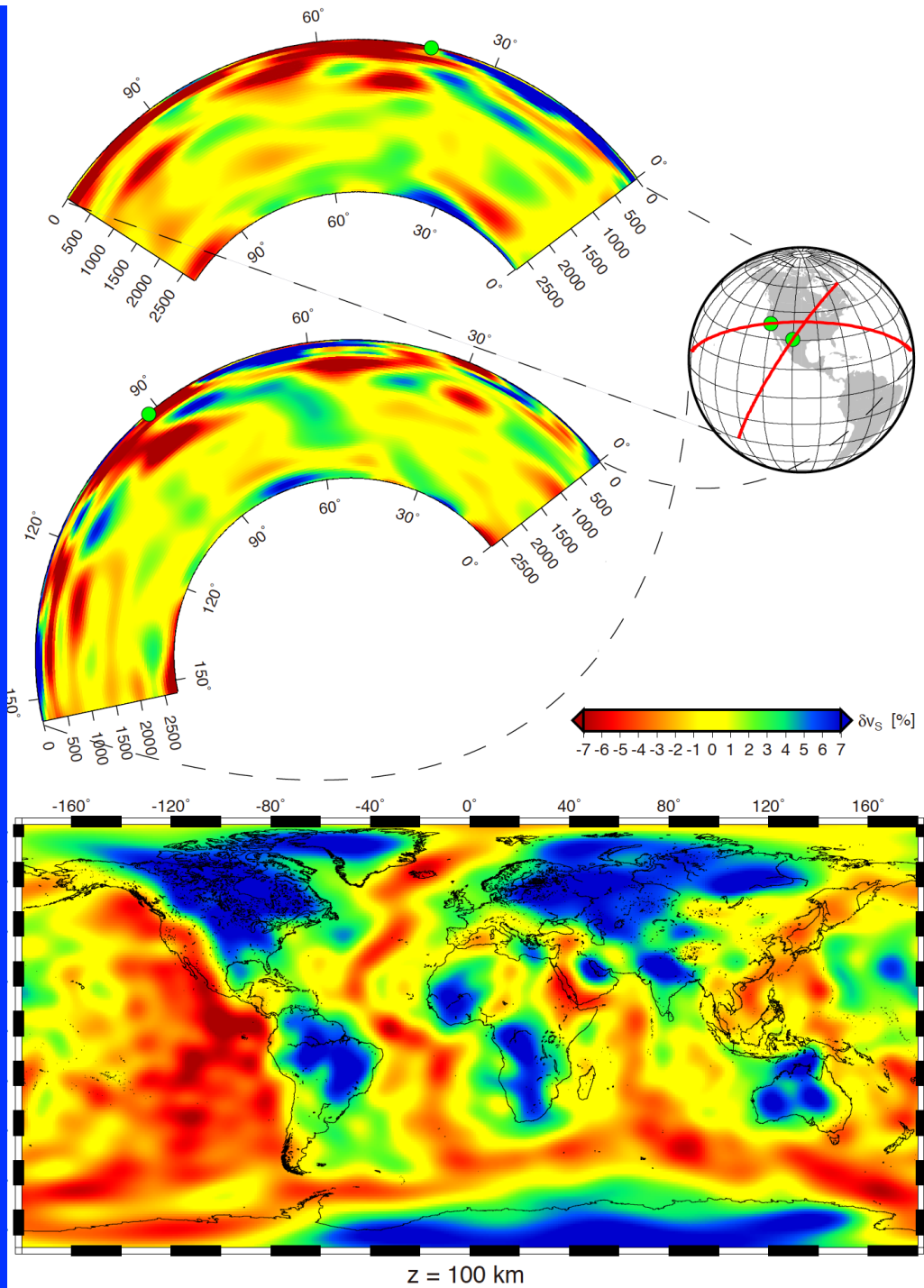
- Mantle tomography and history of subduction models

-750



-810



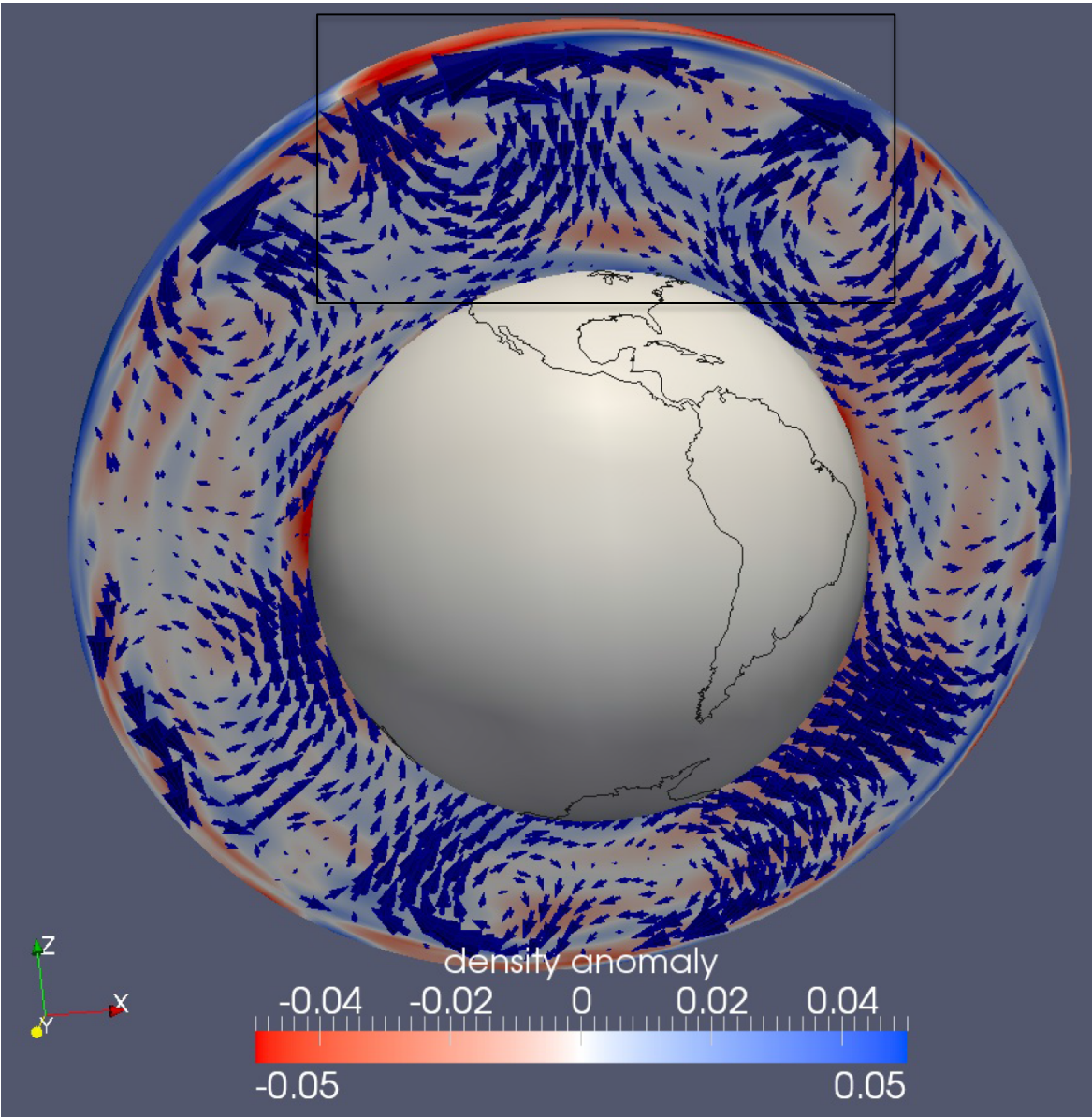


Example of tomography model

*Lekic and Romanowicz [2011]
Geophys. J. Int.*

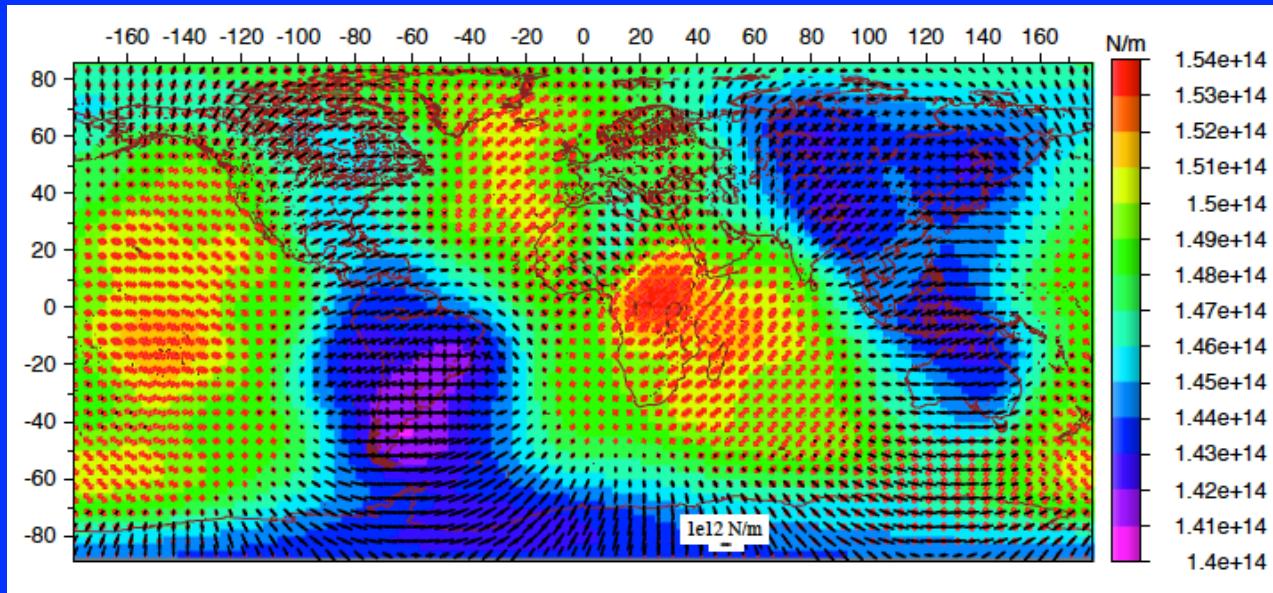
Farallon plate
subduction history
impacts North
America dynamics

Another Example



Tomography model from: *Ritsema, Deuss, van Heijst, & Woodhouse [2011] Geophys. J. Int.*
Computed using HC Code [*Milner et al., 2009] Eos*

Benchmarking with 3-D spherical convection



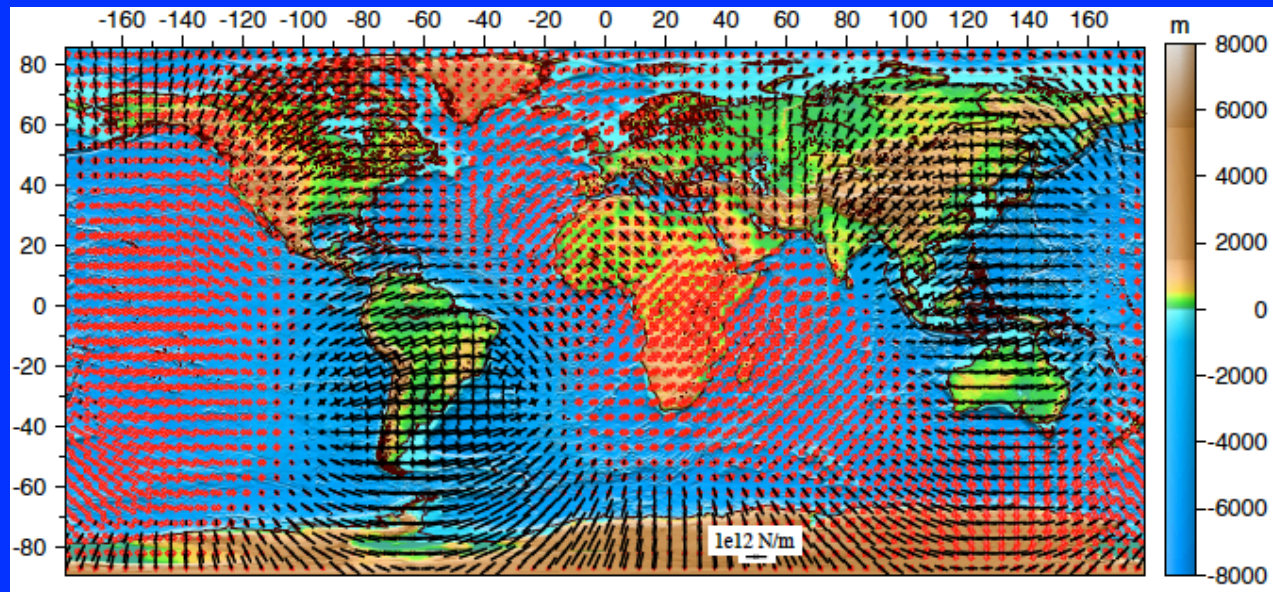
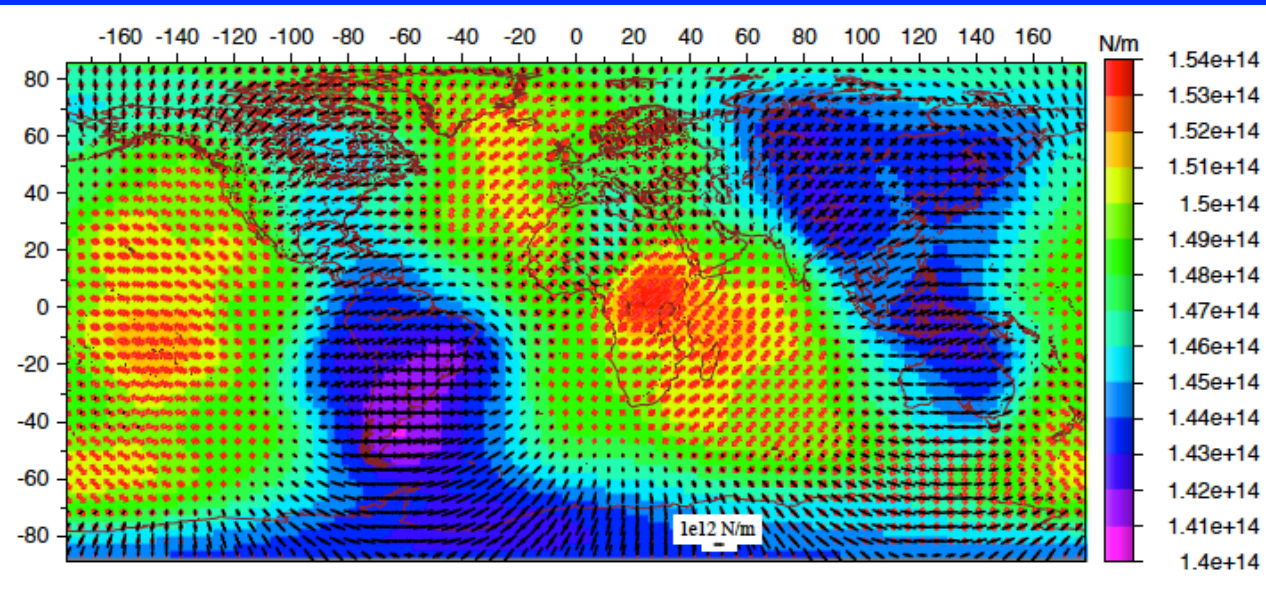
Ghosh et al. [2008], GRL

Thin Sheet
deviatoric stress
response to GPE
differences, created
by dynamic
Topography, created
in 3-D global
convection model

Benchmarking with 3-D spherical convection

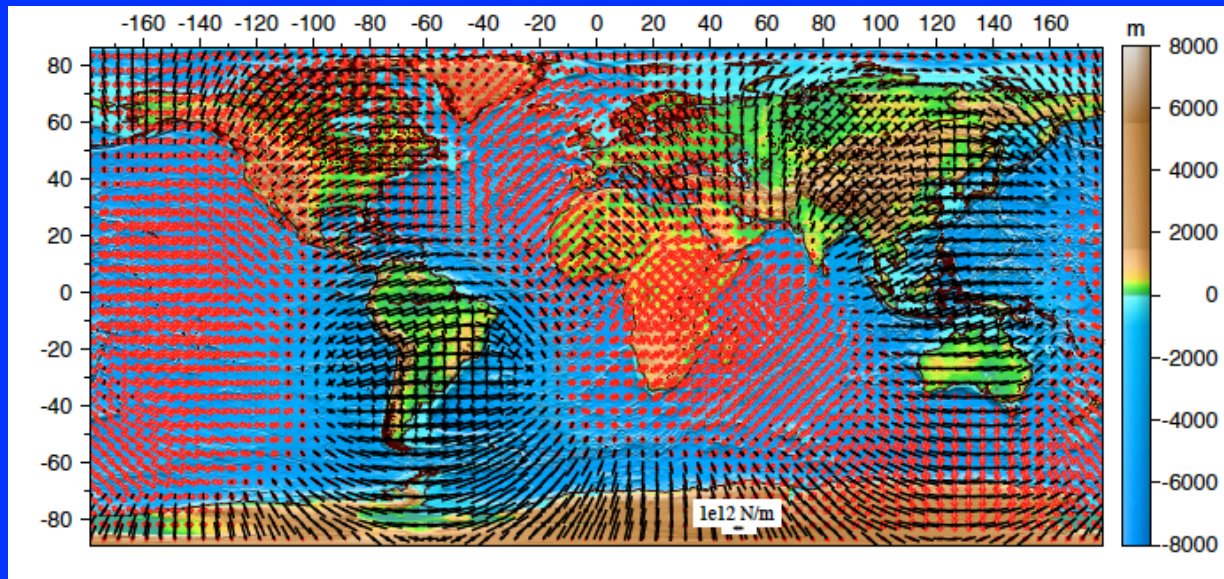
Ghosh et al. [2008], GRL

Thin Sheet
deviatoric stress
response to GPE
differences, created
by dynamic
Topography



Thin sheet deviatoric
stress response to
tractions applied at
base

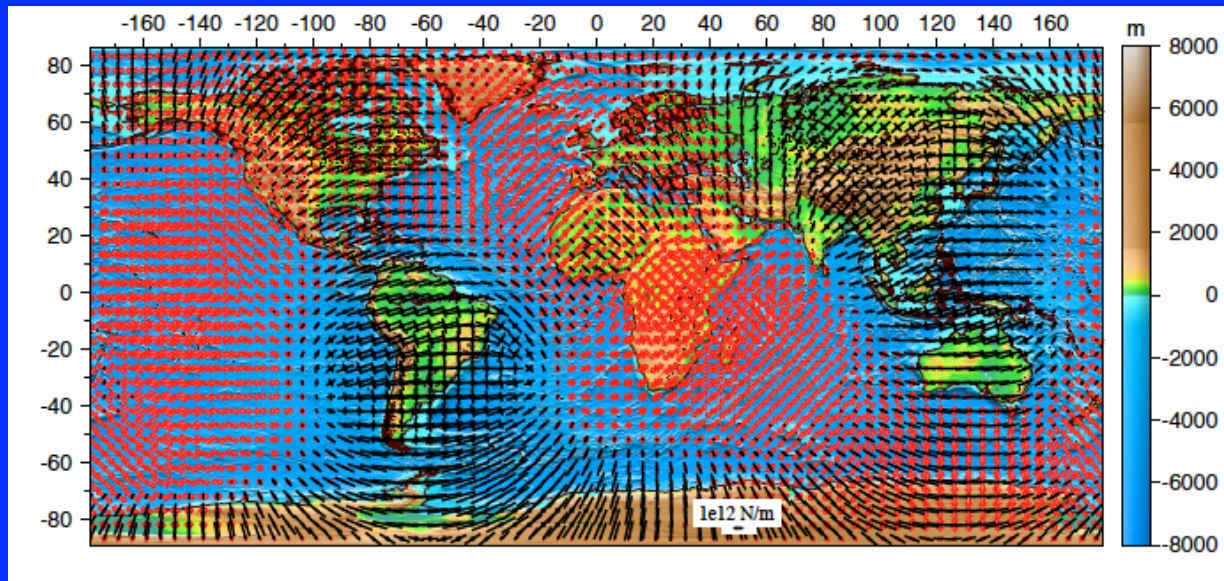
Comparison of thin sheet stresses with output from full 3-D model



Total thin sheet response
= traction solution + GPE
solution (lithosphere
finite element solution)

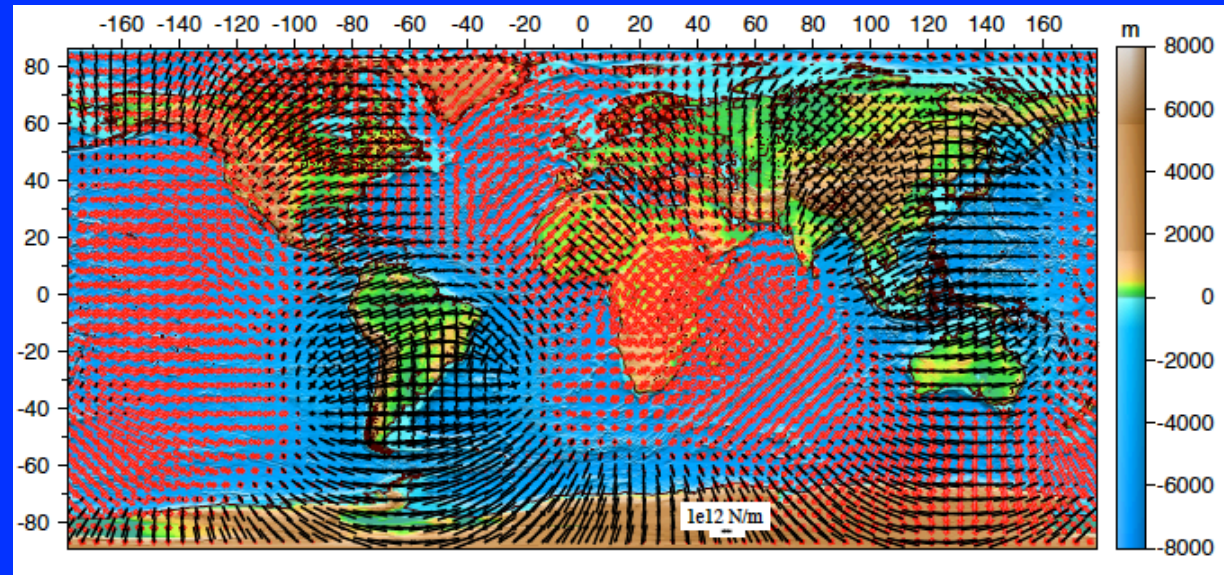
Ghosh et al. [2008], GRL

Comparison of thin sheet stresses with output from full 3-D model



Total thin sheet response
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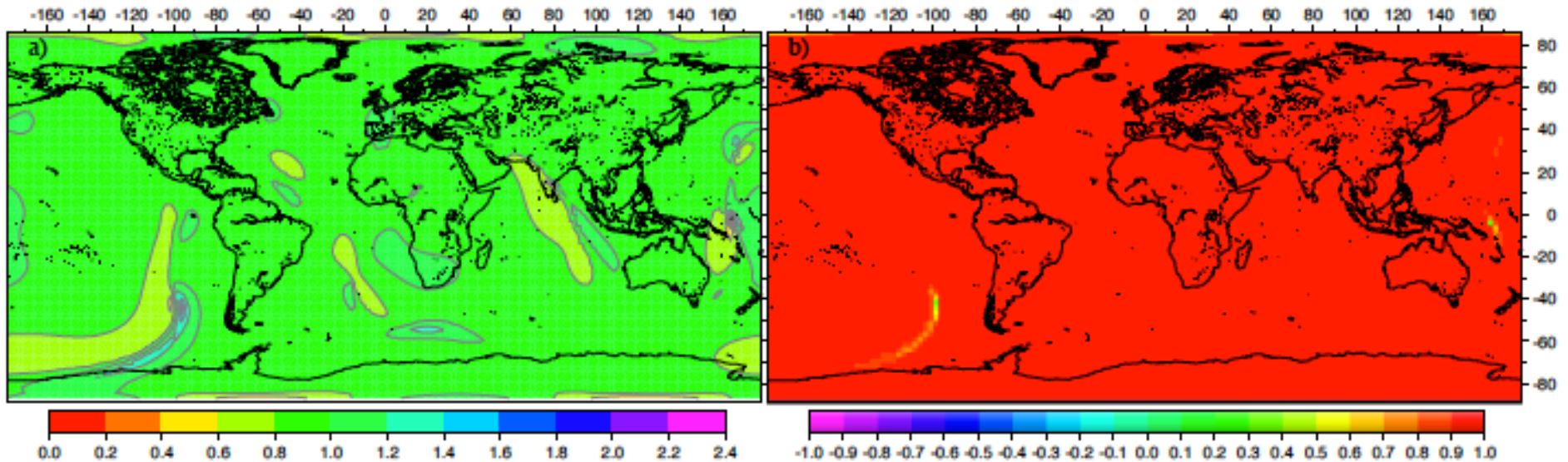
Ghosh et al. [2008], GRL



Deviatoric Stress output
from the full 3-D
convection model

Agreement in magnitude

Agreement in orientation and style



$$(T_{\text{thin sheet}})/(T_{3-D})$$

Ghosh et al. [2008], **GRL** (see suppl.)

*Variable viscosity case benchmarked by
Klein et al. [2009], JGR

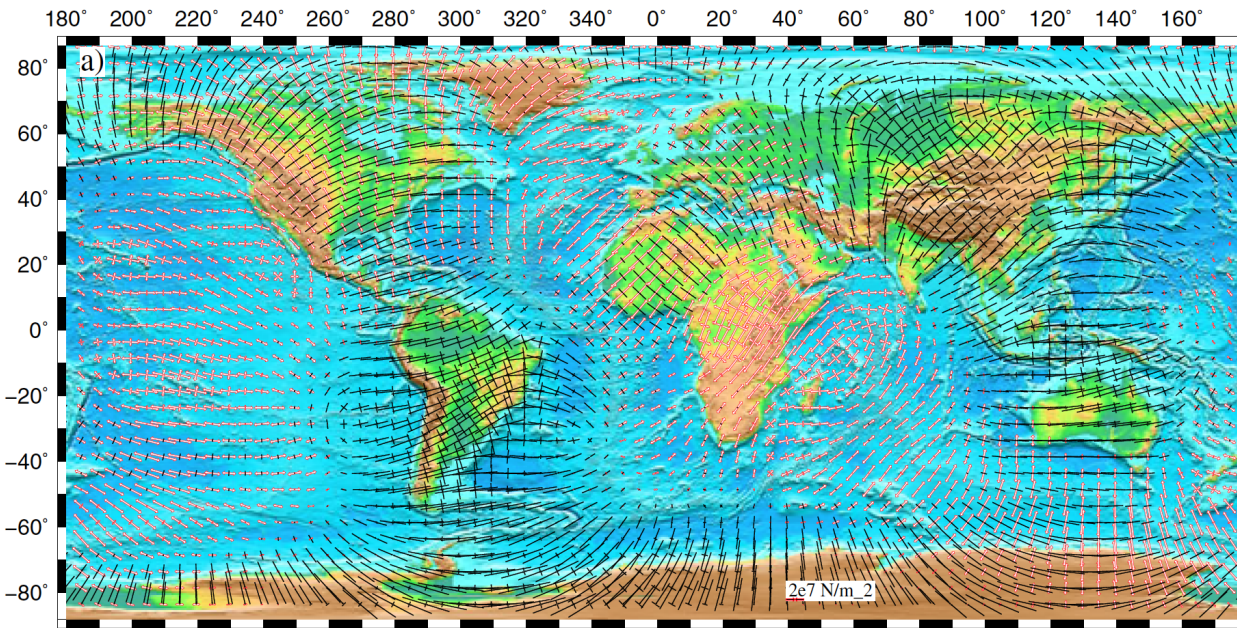
Correlation between tensor field
from thin sheet with tensor field from
global 3-D model = $\tau_1 \bullet \tau_2 / T_1 T_2$

Summary from benchmarking

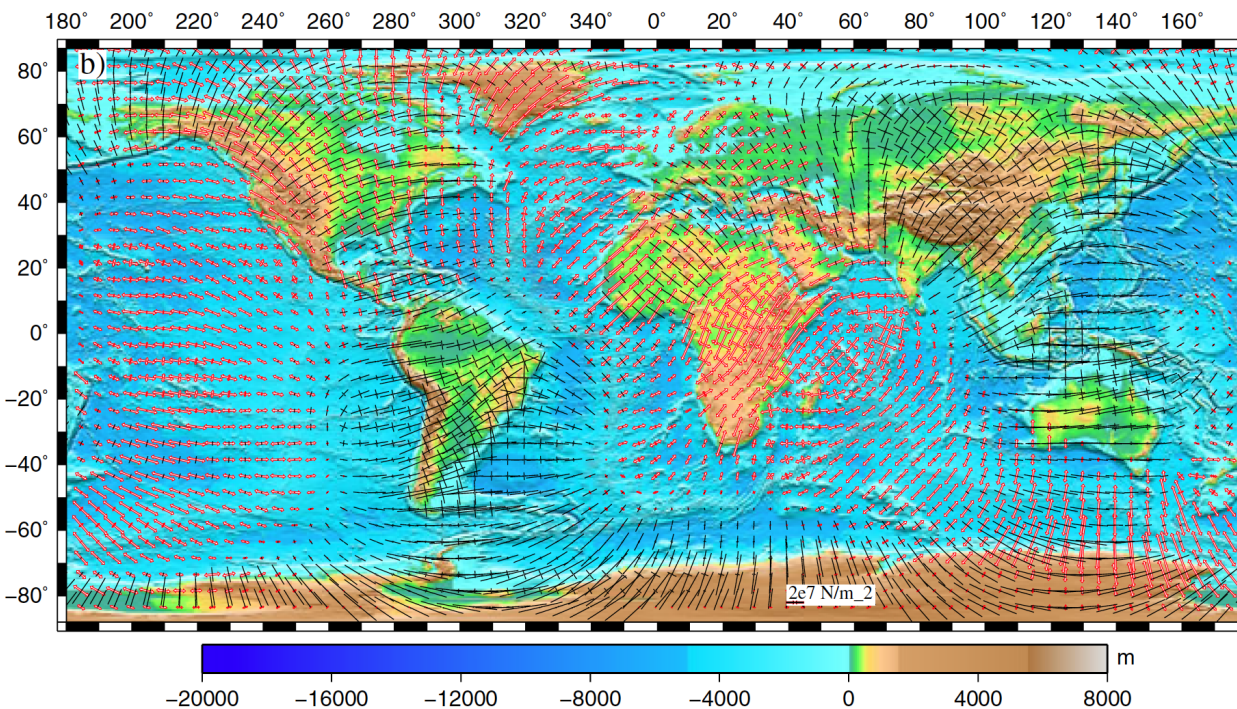
- Can recover the deviatoric stress field given accurate estimates of (1) topography, crustal and upper mantle structure, and (2) knowledge of applied horizontal tractions from mantle flow (reliable convection models).
- If you know surface motions, then you can also recover the absolute values of effective viscosity

Benchmarking with lateral viscosity variations

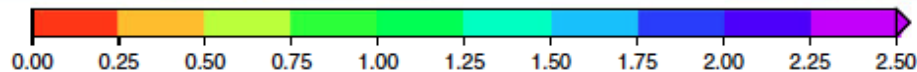
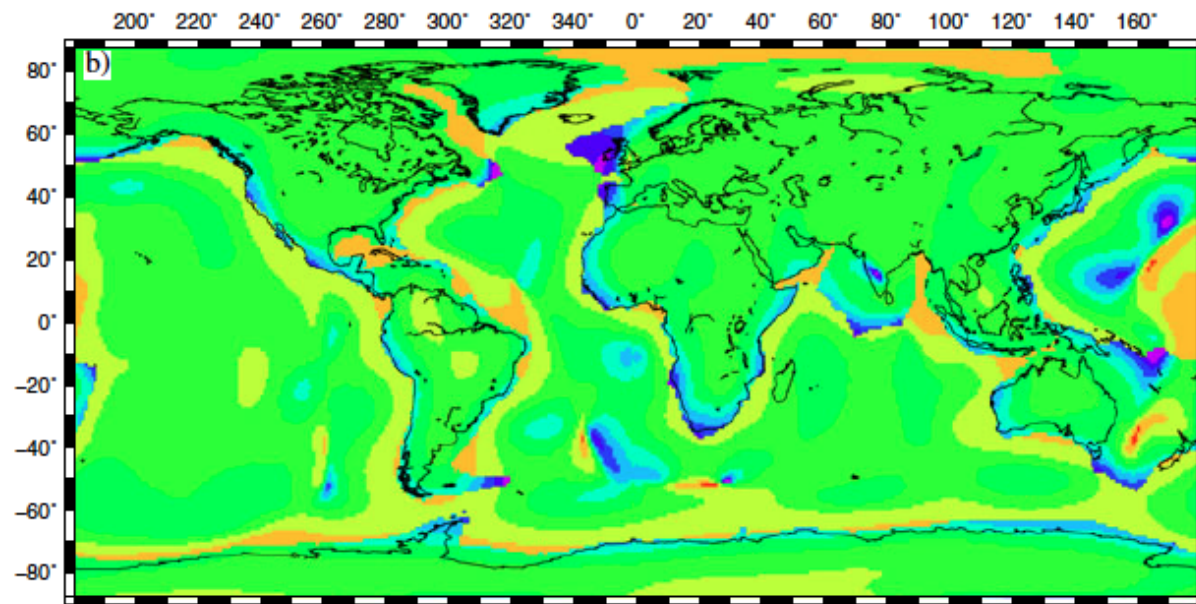
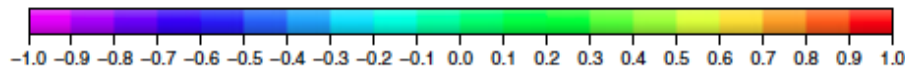
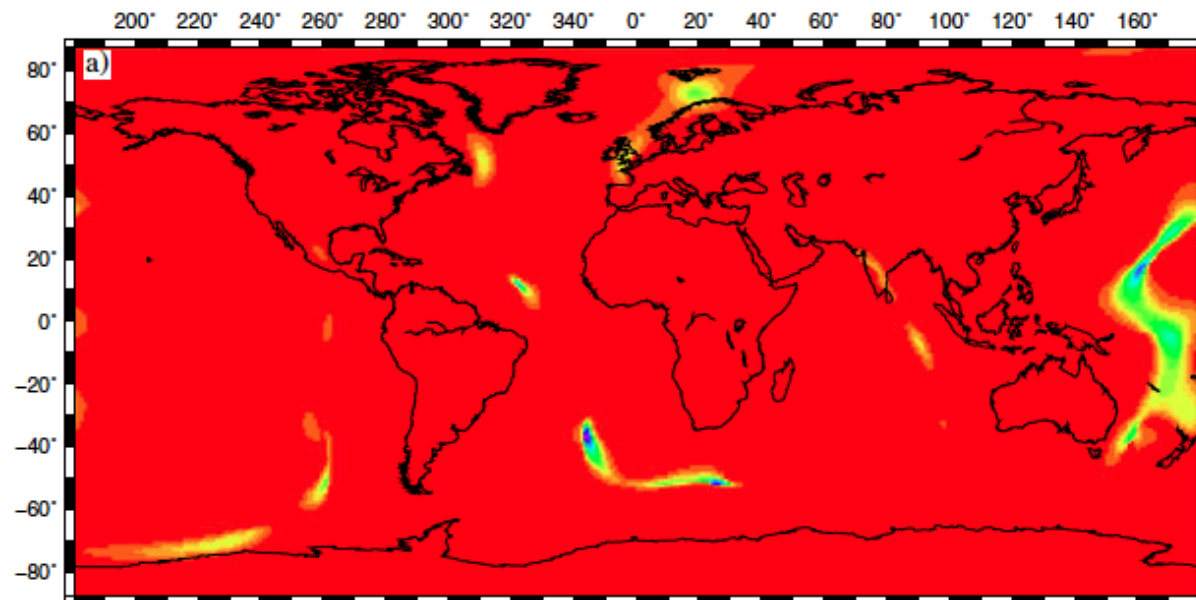
- lateral viscosity variations of 2 order magnitude in full 3-D convection model
- An approximation of the relative viscosity variations (but not exact) was used in the thin sheet model
- Stresses were recovered in thin sheet model with the worst misfits in magnitudes off by factor of 2 in areas with significant lateral variation in viscosity



Thin sheet output
= dynamic topo +
traction
contributions +
using relative
viscosity variations



Output from
full 3-D global
model with
lateral
viscosity
variations



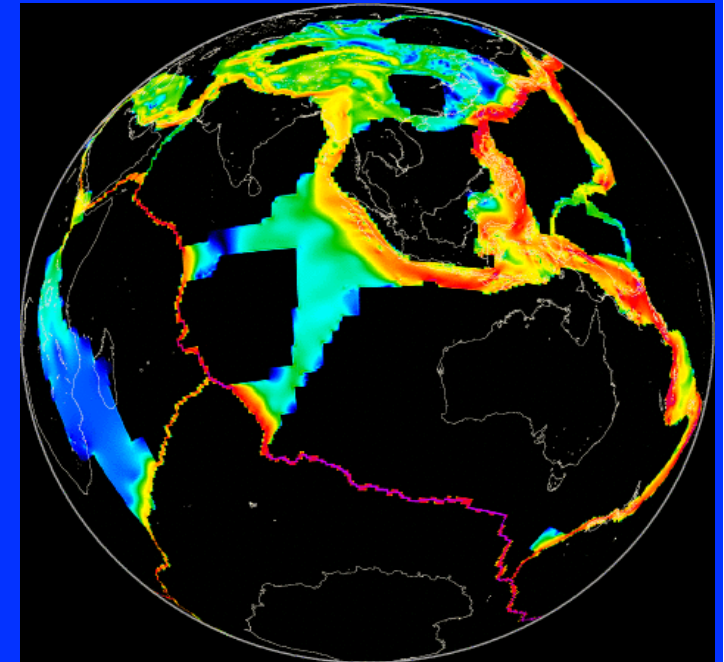
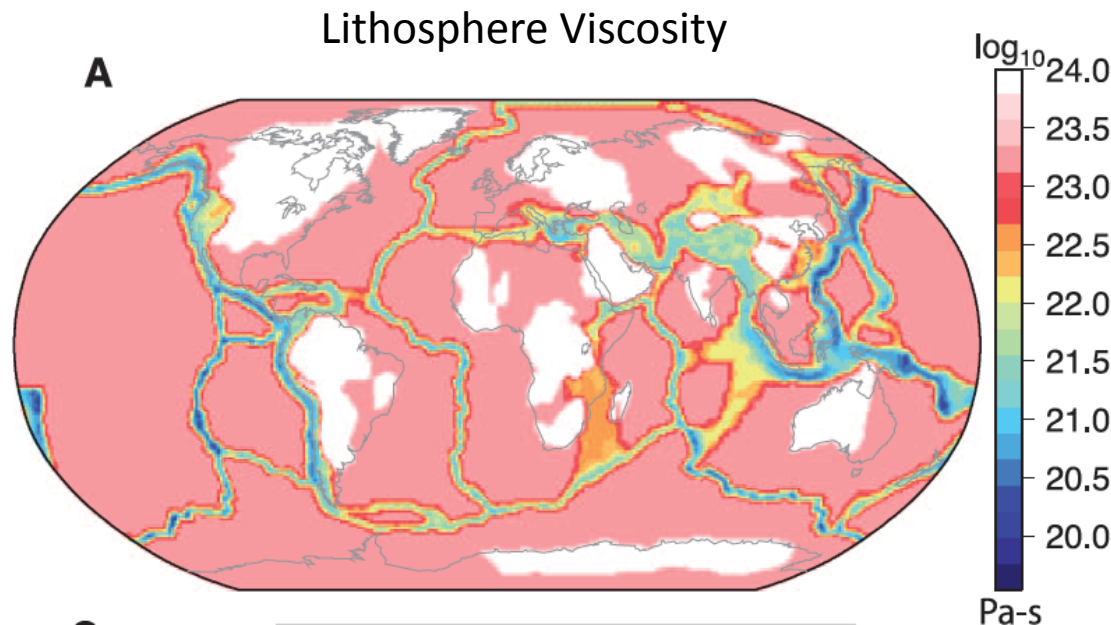
Correlation
between tensor
field from thin
sheet with
tensor field from
global 3-D model
 $= \tau_1 \cdot \tau_2 / T_1 T_2$

$$(T_{\text{thin sheet}}) / (T_{3-D})$$

Forward Dynamic Modeling: Adjustable Parameters

- Lateral viscosity structure of lithosphere
 - Location of keels, cratons, and plates
 - Old vs. Young Ocean lithosphere
 - Location of plate boundary zones and their viscosity distribution
- Mantle Radial Viscosity Profile

Global Modeling to Compute Stresses, Strain Rates, and Surface Motions: (1°x1° grid with over 63,000 elements)



Ghosh and Holt, 2012 Science

Relative viscosity variation:

$$\frac{1}{\mu} = 1 + \left(\frac{1}{\mu_{ref}} - 1 \right) \sqrt{\frac{E^2}{E_{ref}^2}}$$

Plates = 1

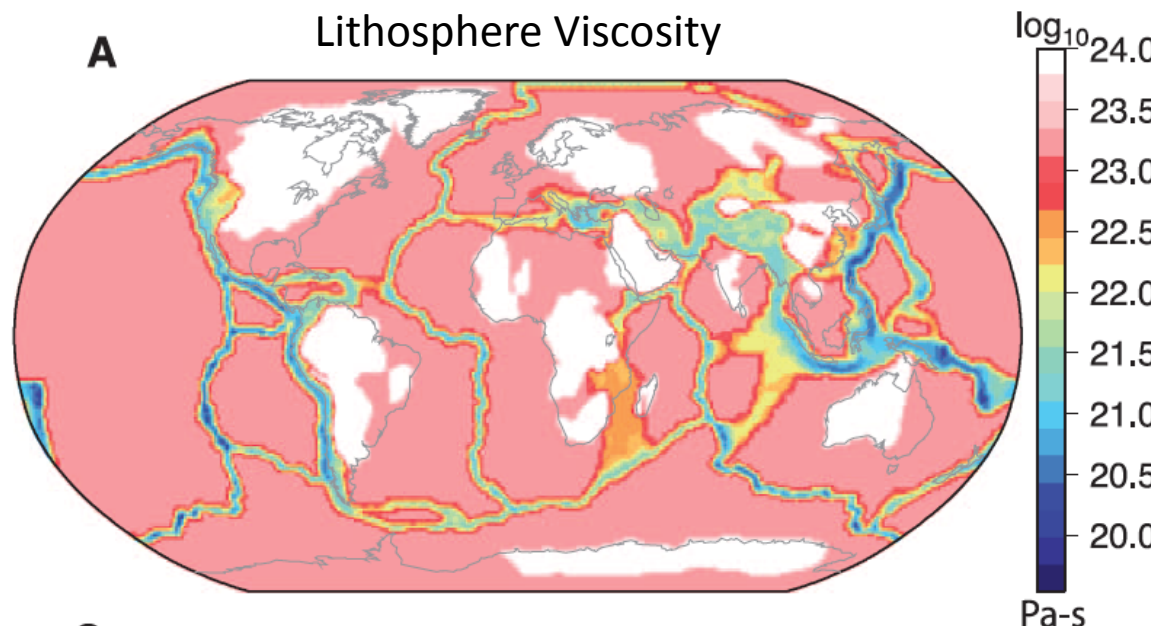
Cratons = 10

E = scalar second invariant of strain rate from GSRM [Kreemer et al., 2003]

E_{ref} = E value corresponding to area with μ_{ref}

μ_{ref} = viscosity for area with E_{ref}

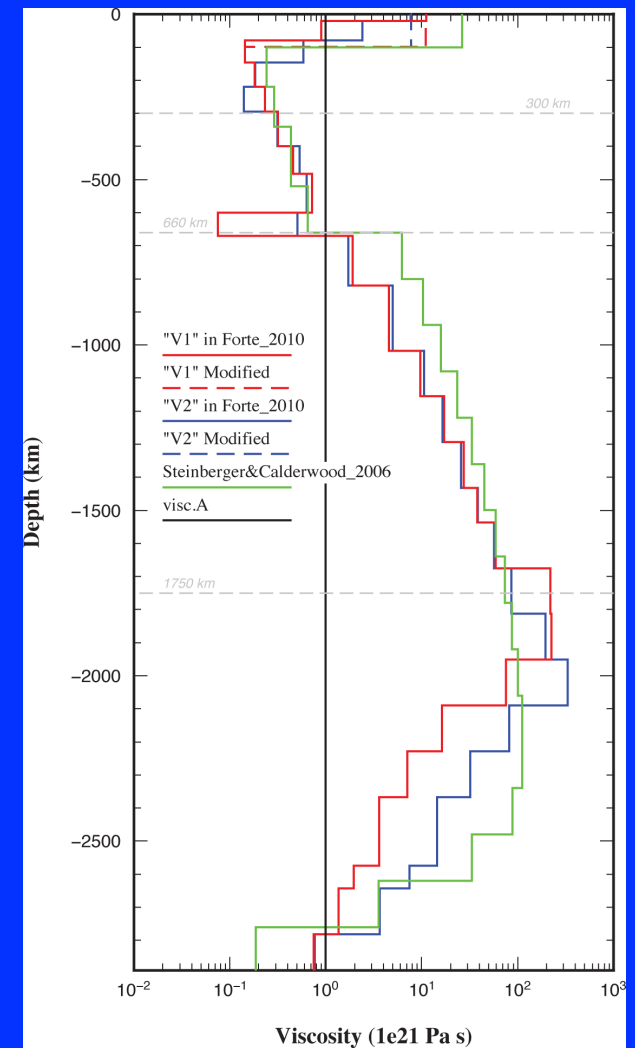
Global Modeling to Compute Stresses, Strain Rates, and Surface Motions



Ghosh and Holt, 2012 Science

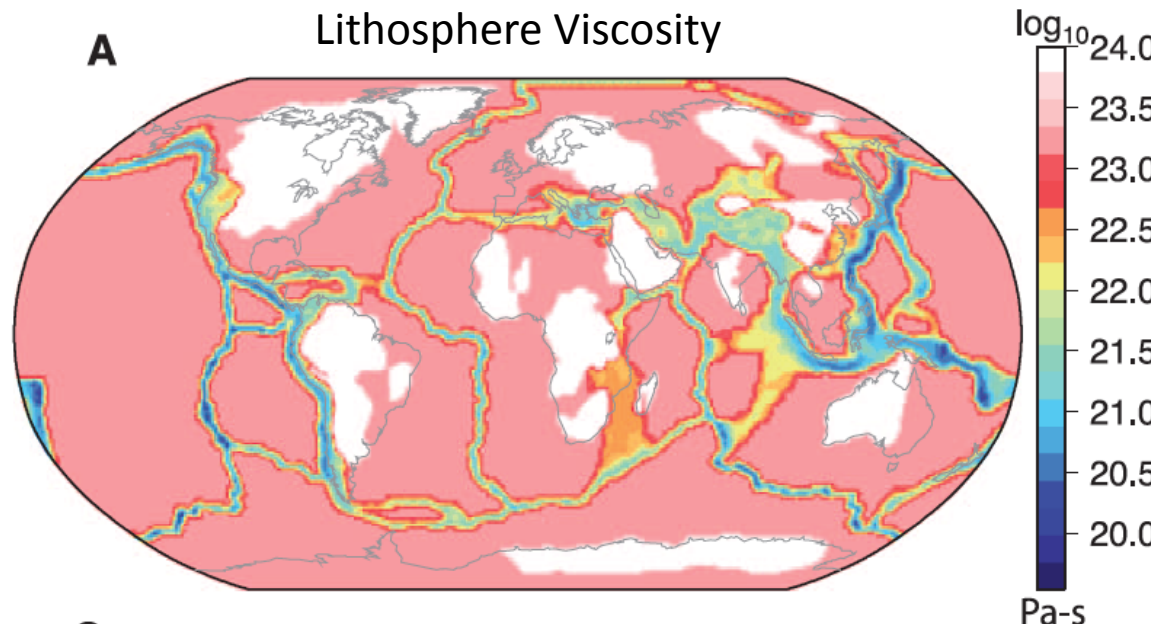
$$\frac{1}{\mu} = 1 + \left(\frac{1}{\mu_{ref}} - 1 \right) \sqrt{\frac{E^2}{E_{ref}^2}}$$

For $E_{ref} = 3e-7/\text{yr}$ we tried $\mu_{ref} = 1/10; 1/30; 1/100; 1/1000$



Radial Viscosity Profiles

Results from 300 forward models



Ghosh and Holt, 2012 Science

Plates = $1e23$ Pa-s

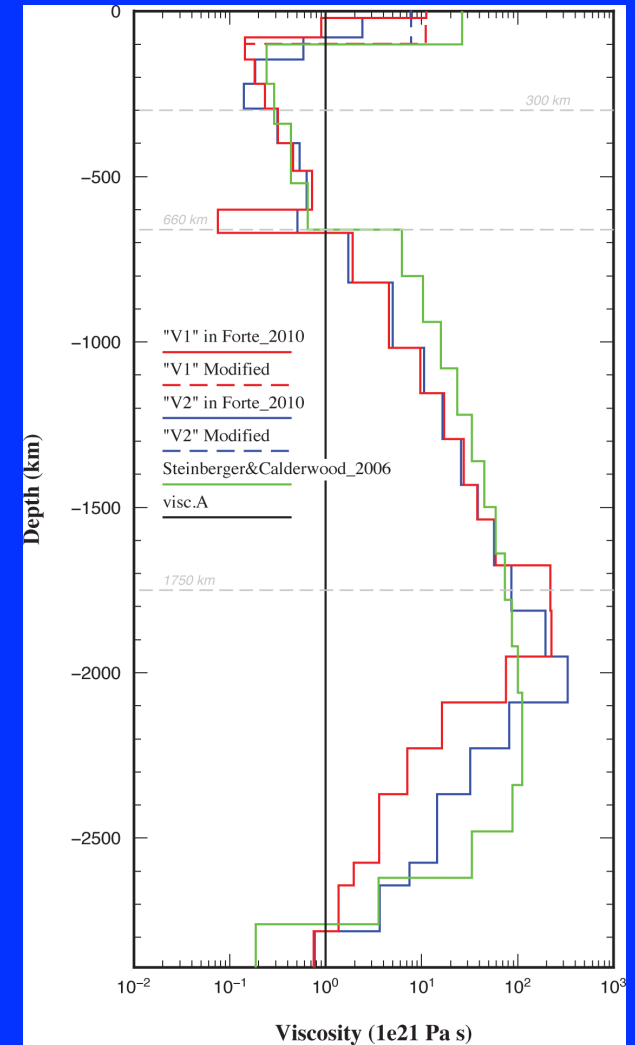
Cratons = $1e24$ Pa-s

Deeper Continental Keels = $1e21 - 1e22$ Pa-s

Asthenosphere = $1e20$ Pa-s

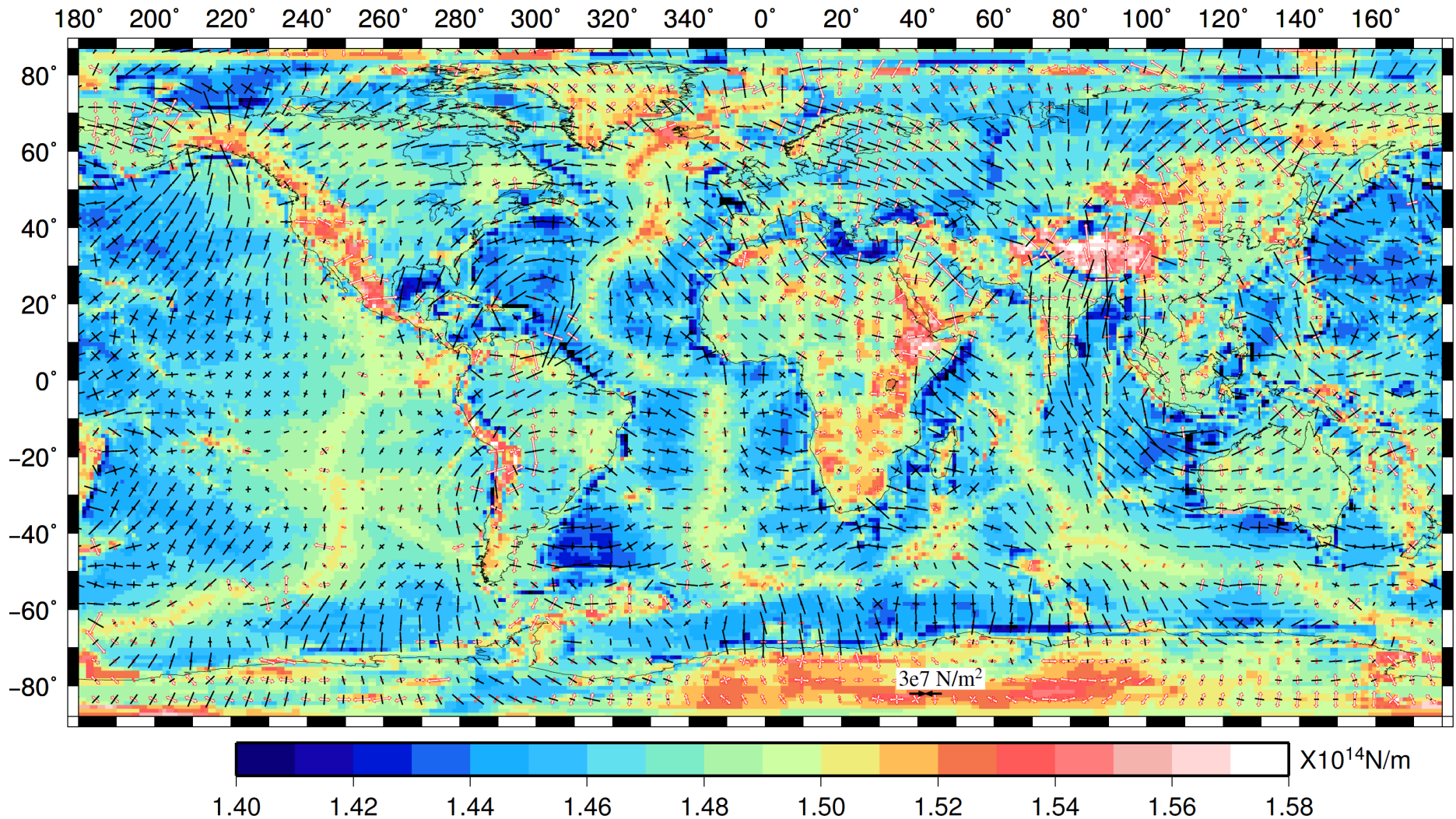
Plate Boundary Zones = Variable Viscosity

Variety of published tomography models have been tried

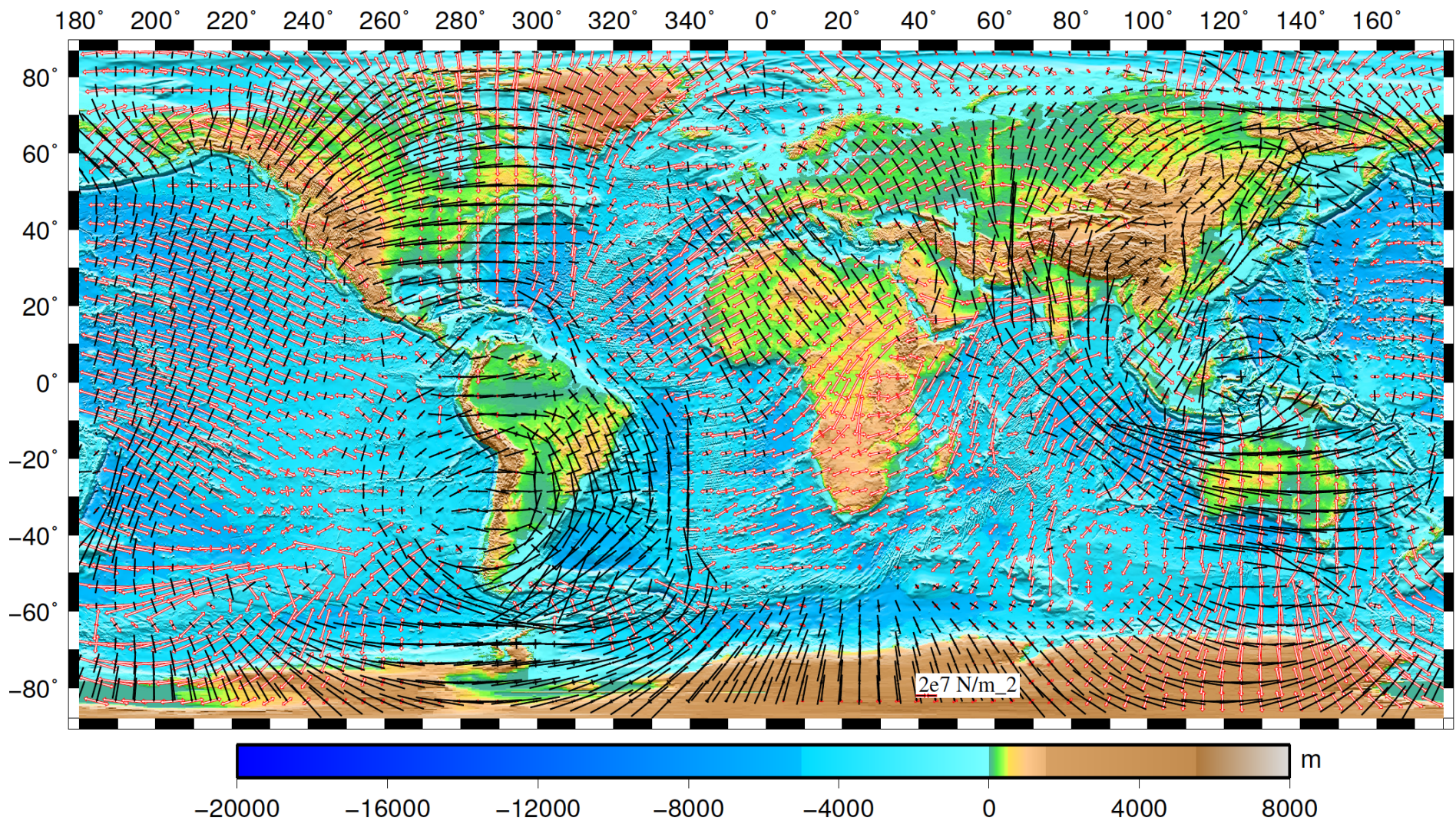


Radial Viscosity Profiles

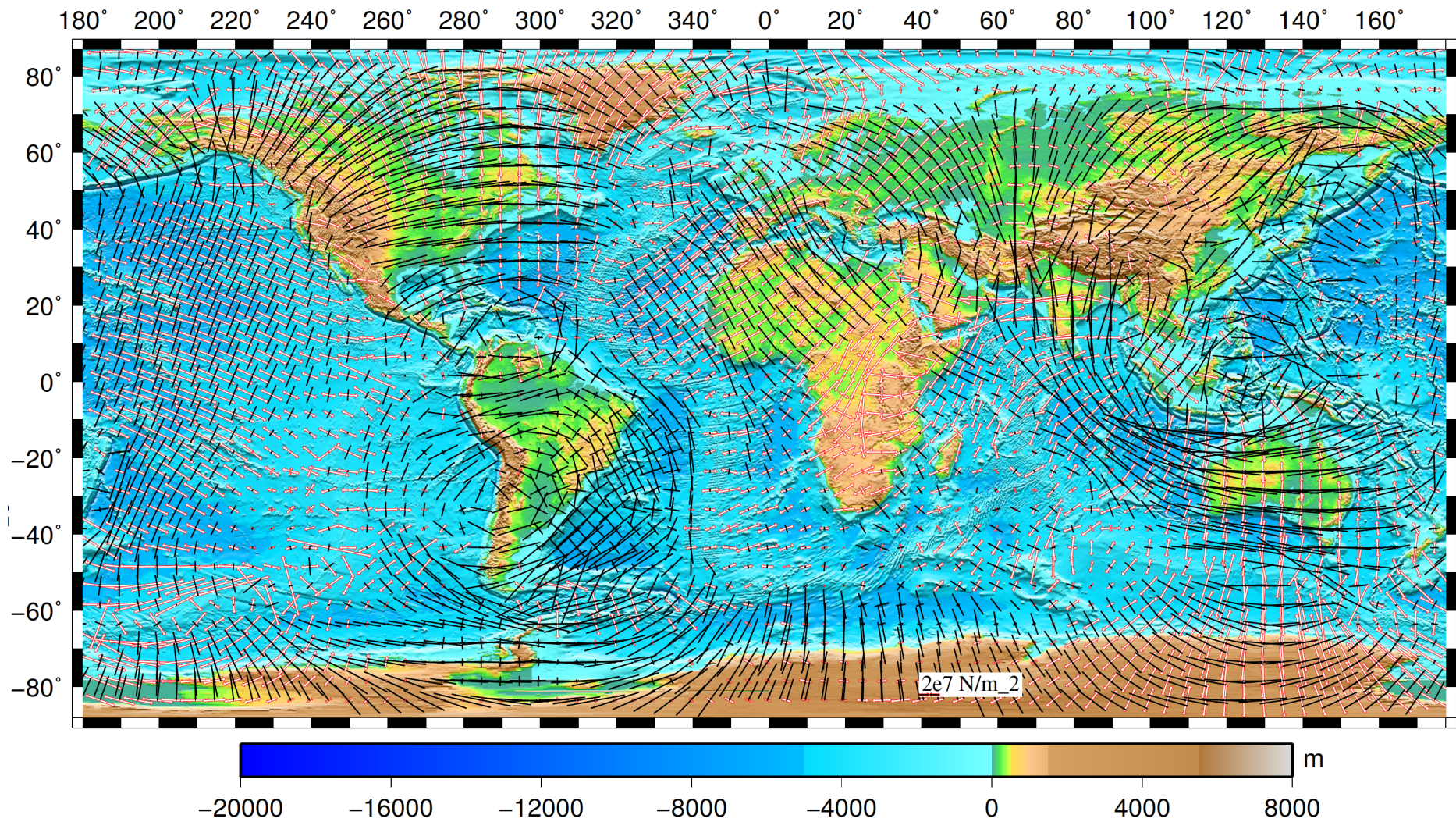
Stresses from Topography and Lithosphere Structure



Ghosh, Holt, Wen, 2013, JGR



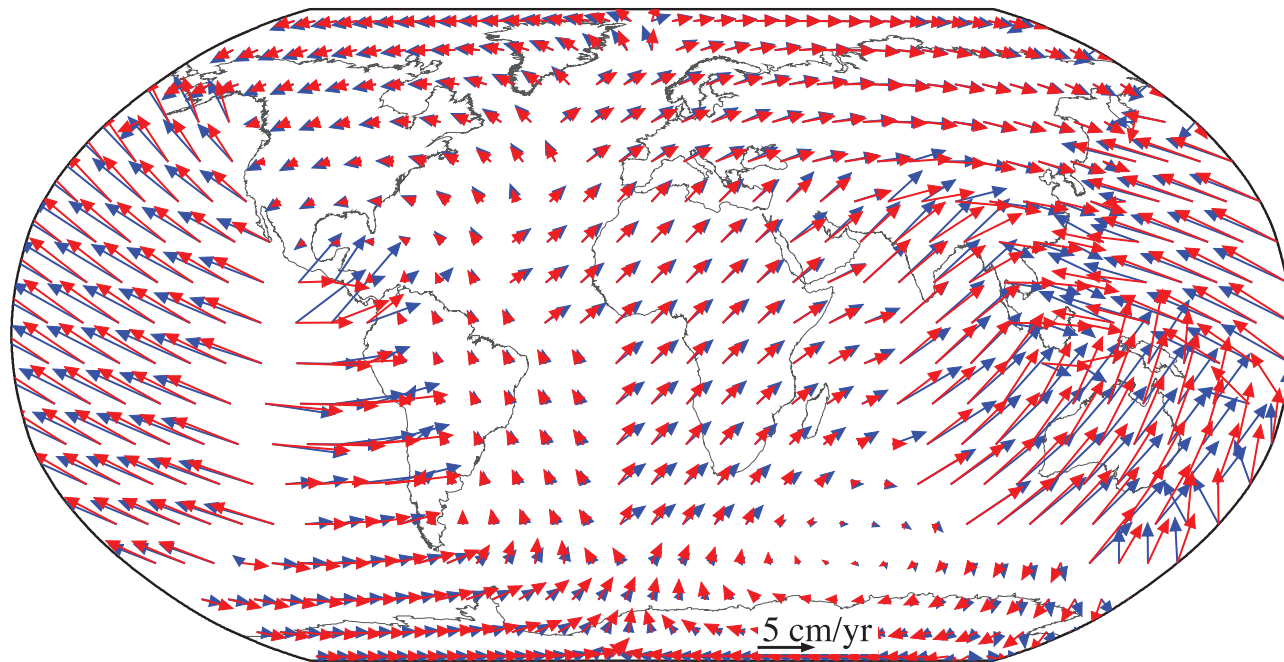
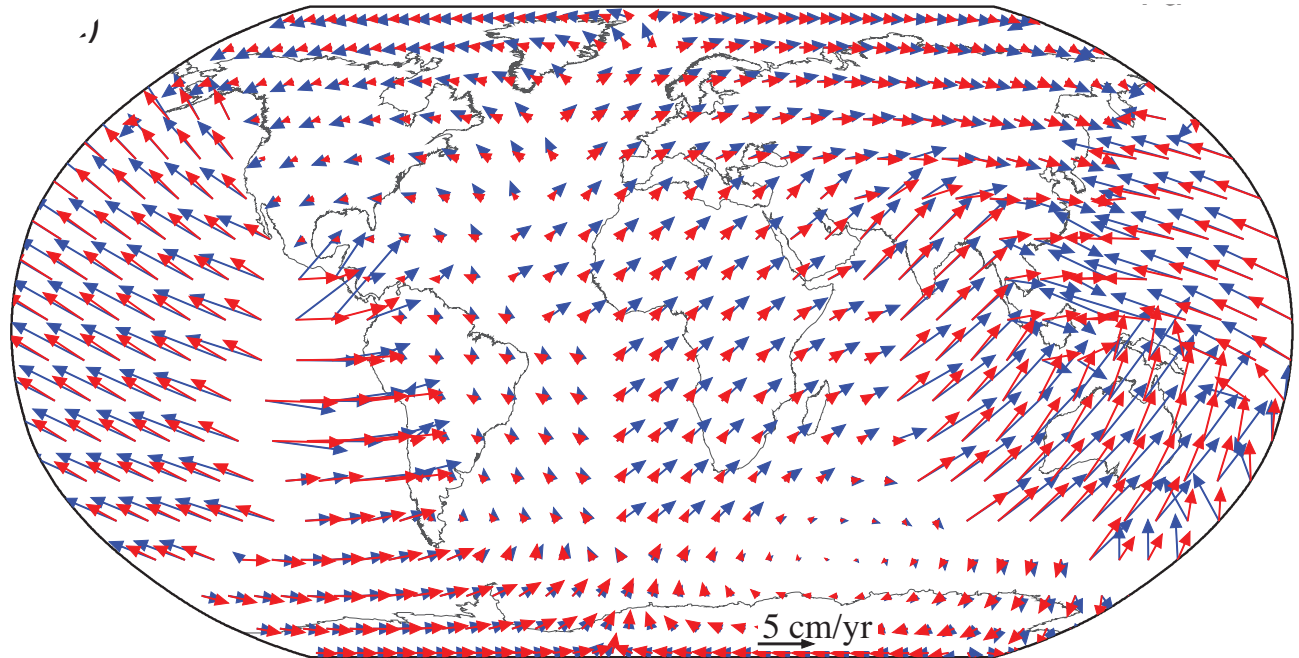
Dev. Stress from tractions associated with mantle flow
Ghosh et al. [2013] J.G.R



Total Dev. Stress from GPE + tractions *Ghosh et al. [2013] J.G.R*
 Compare with WSM in plates and GSRM in plate boundary zones

Results: Plate Motions

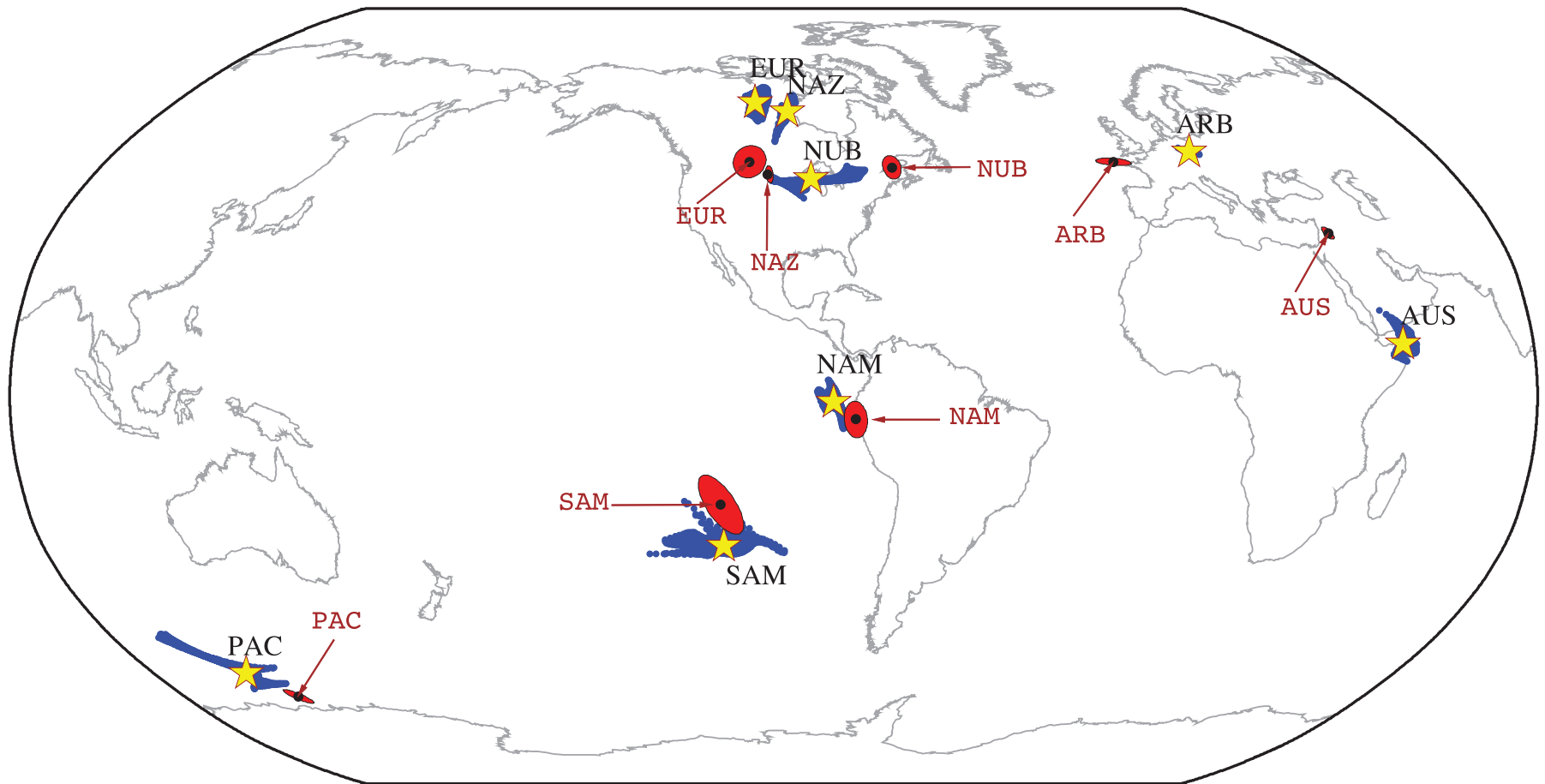
Mantle
tractions



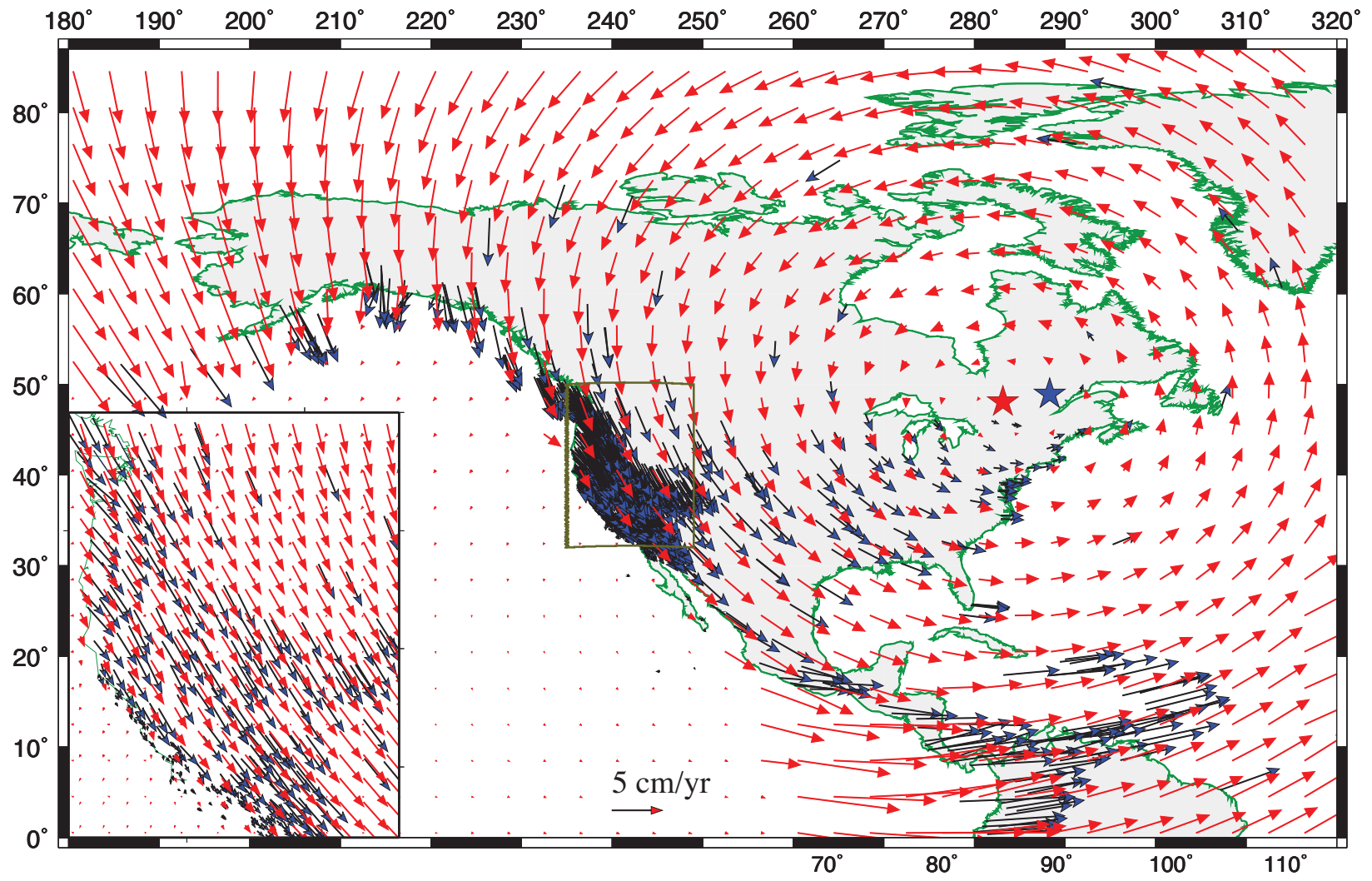
Mantle
tractions
+
GPE

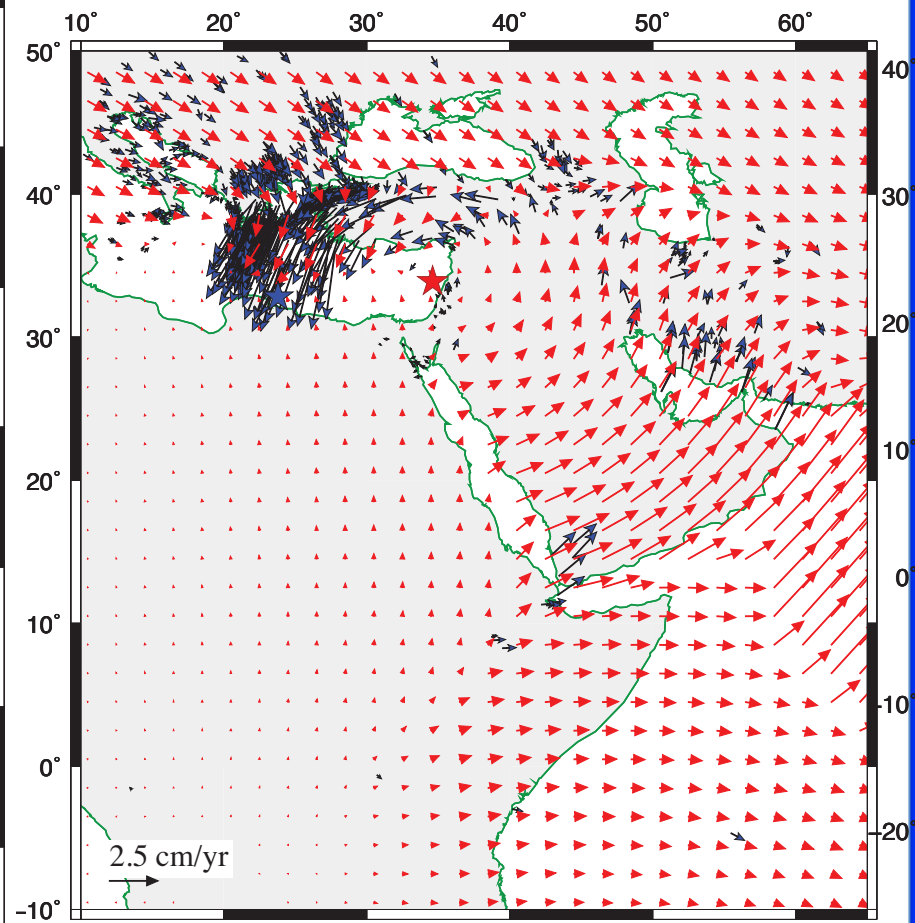
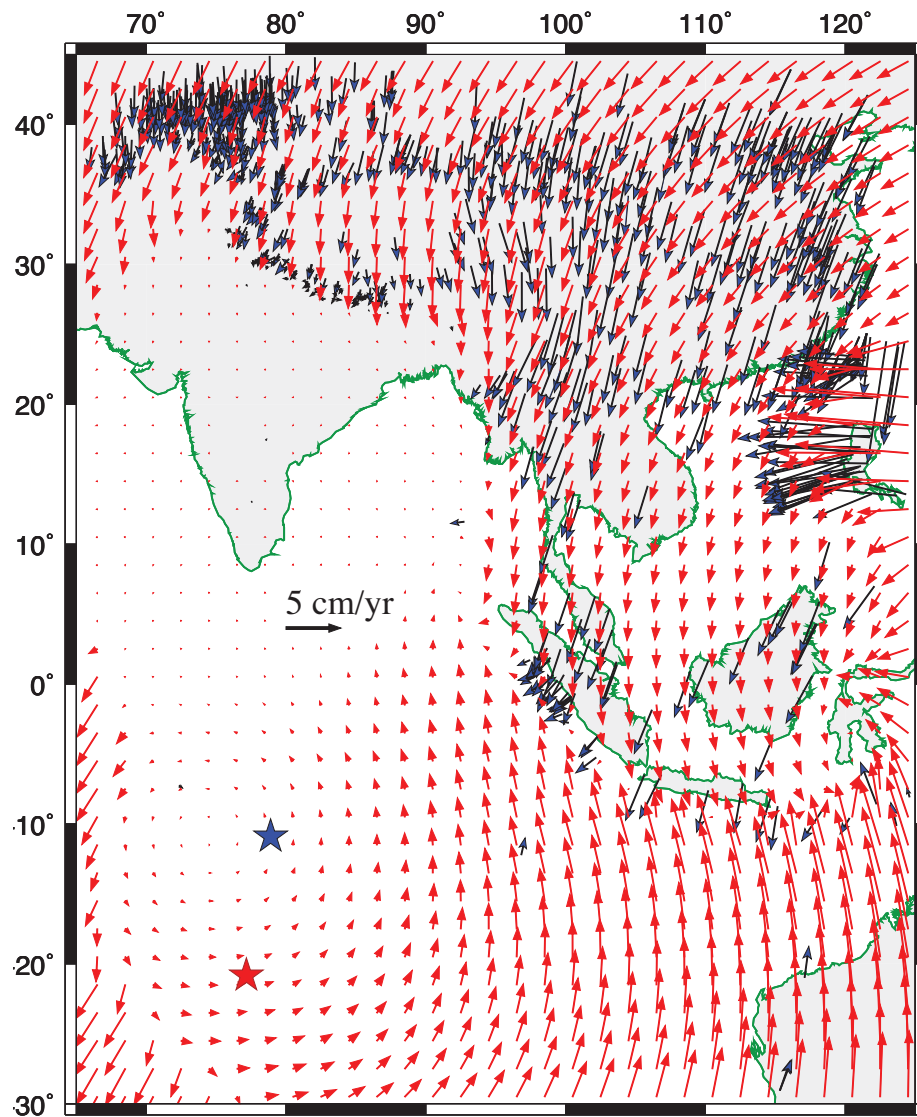
*Ghosh and Holt,
Science (2012)*

RMS misfit < 1 cm/yr



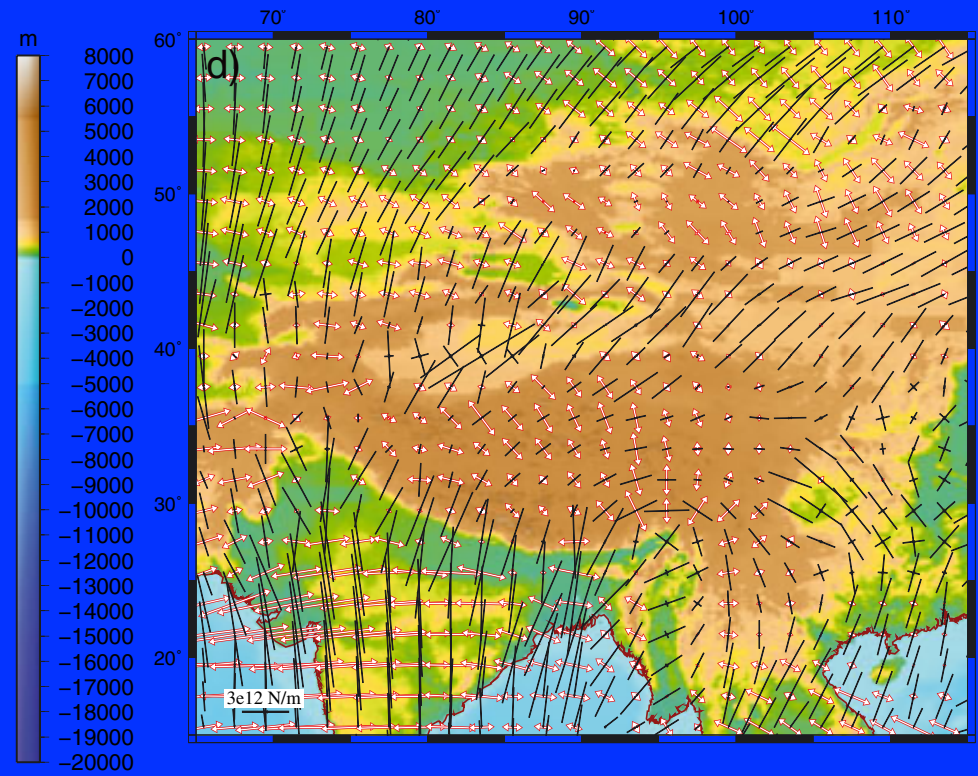
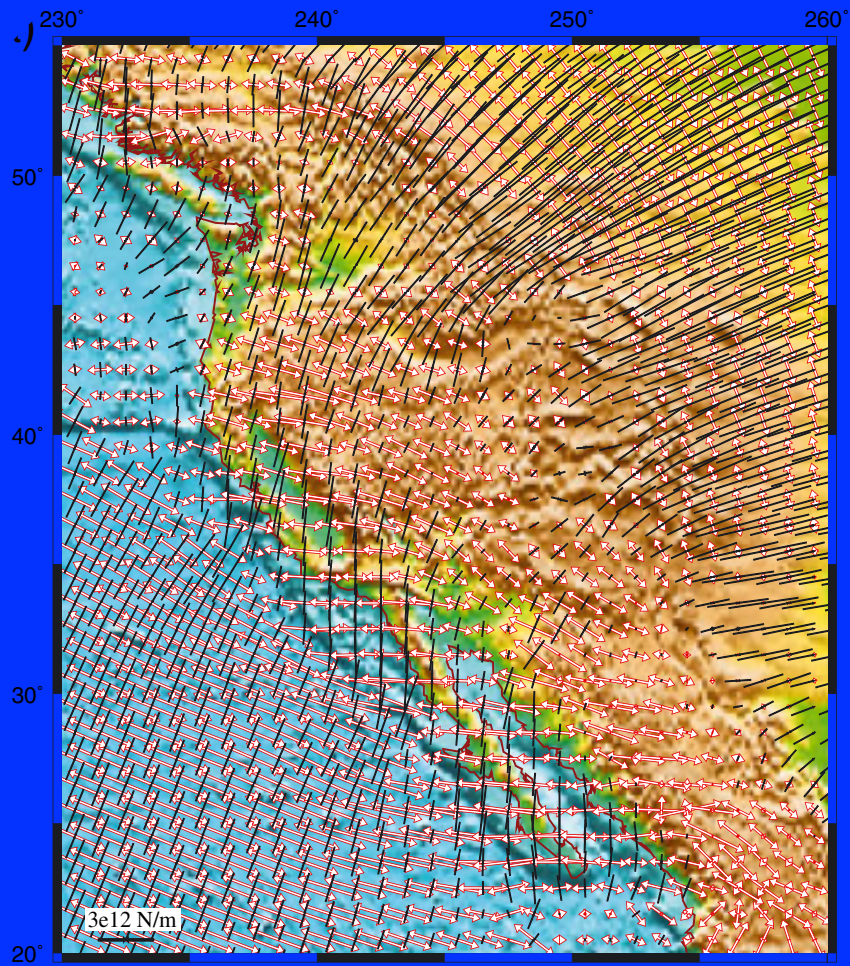
Poles of rotation from dynamic model compared with DeMets et al. [2011]

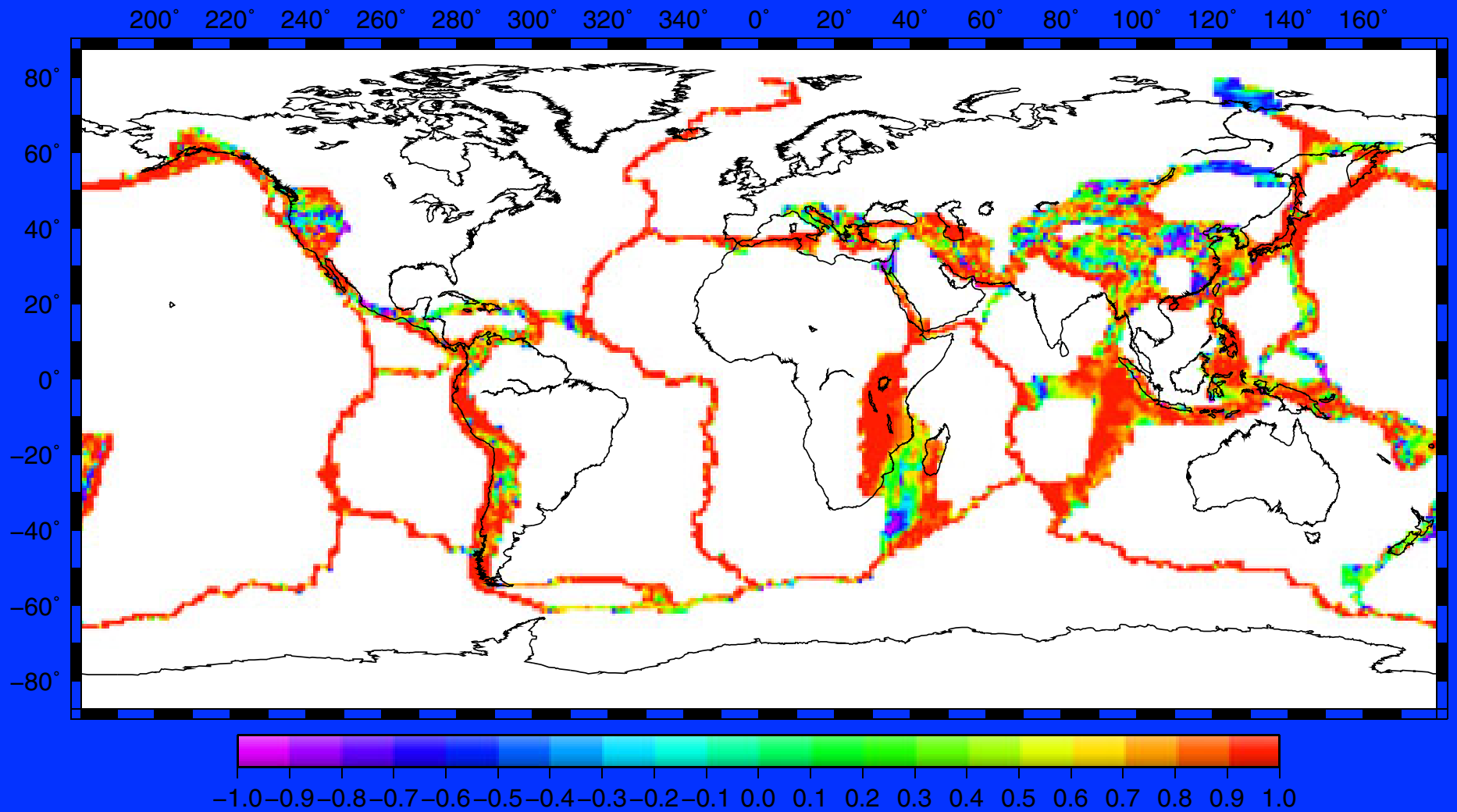




Ghosh and Holt, (2012)

Results: Deviatoric Stresses



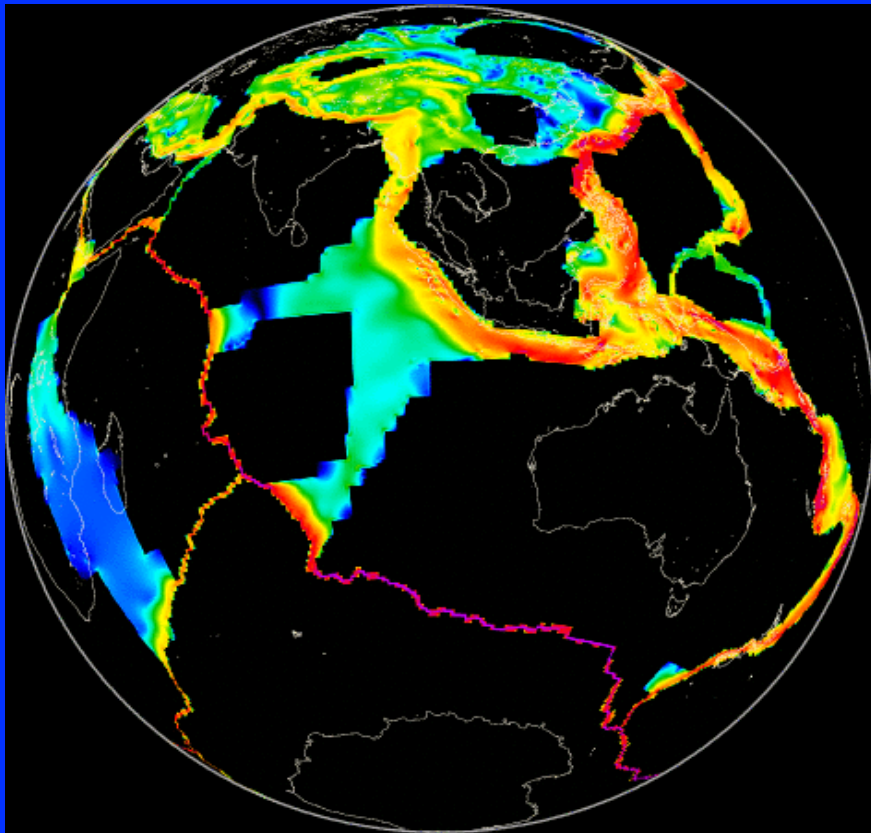


Correlation between predicted deviatoric stresses and strain rates from GSRM

Ghosh et al., JGR (2013)

Global Strain Rate Model

(*Kreemer et al., 2003*)



- Direction of principal axes
- Fault style

Strain

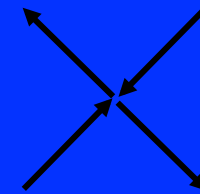
Stress



1



-1

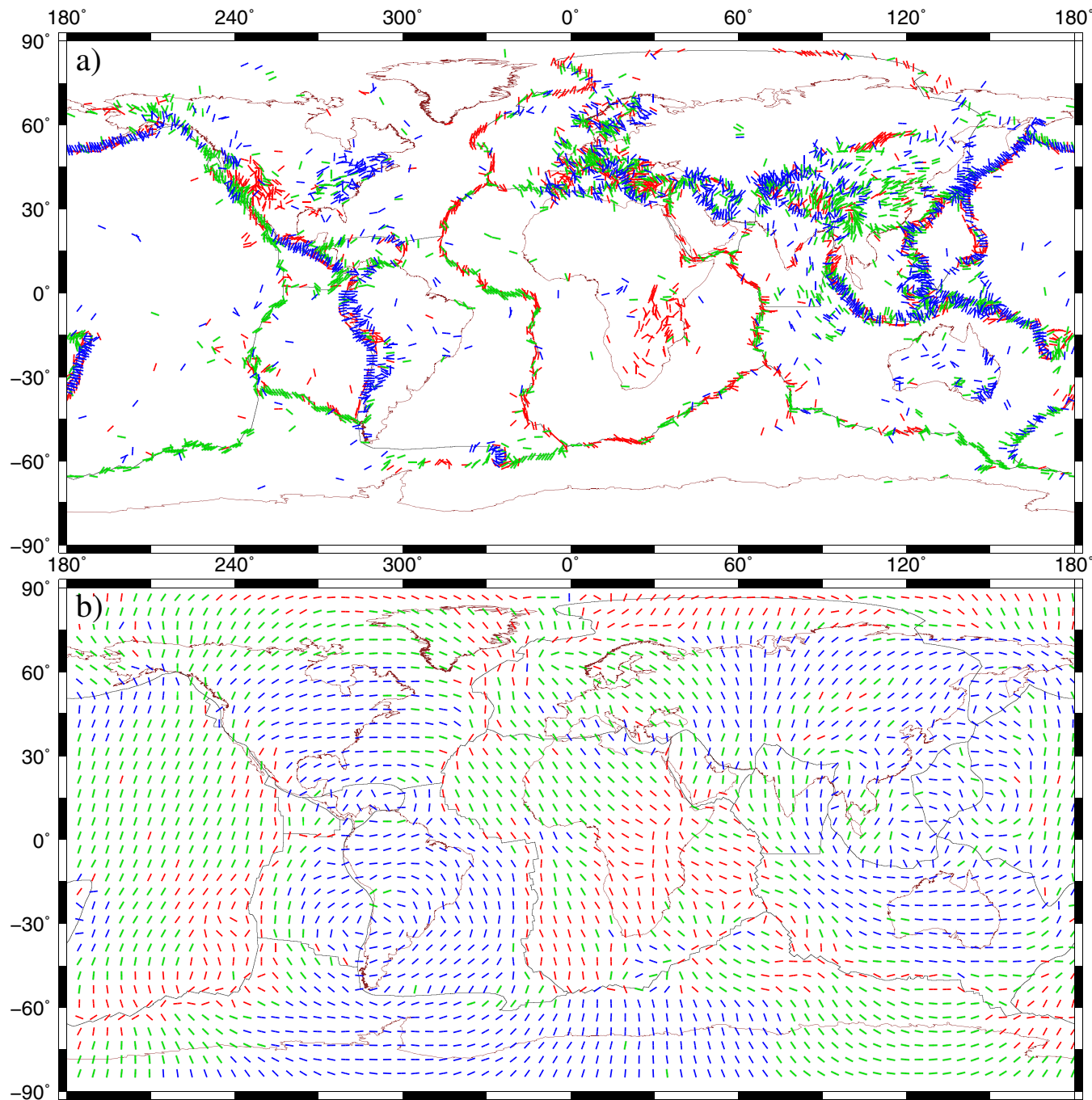


0

Correlation coefficient

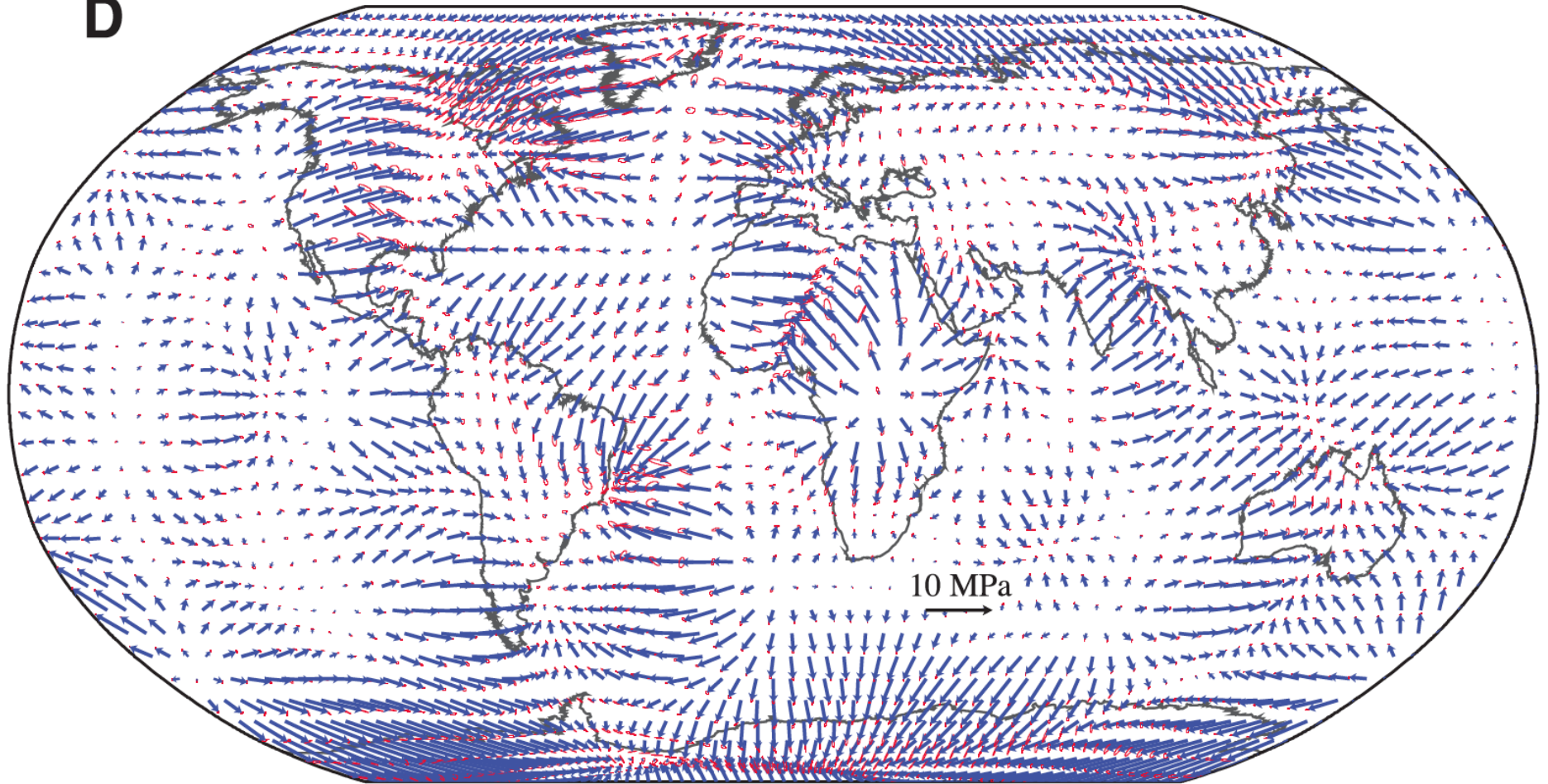
$$-1 \leq \sum_{areas} (\epsilon \cdot \tau) \Delta S / \left(\sqrt{\sum_{areas} (E^2) \Delta S} * \sqrt{\sum_{areas} (T^2) \Delta S} \right) \leq 1$$

Region of Interest	Number of Areas	GPE	Tractions	Differences Plus Basal Tractions
Western North America	618	0.46	0.81	0.78
Andes	440	-0.16	0.98	0.93
Eastern Africa	865	0.32	0.91	0.87
Mediterranean	352	0.68	0.59	0.75
Central Asia	995	0.25	0.62	0.61
Indo-Australian plate boundary zone	836	0.84	0.84	0.90
Mid-oceanic ridges	916	0.94	0.96	0.97
Western Pacific	538	0.42	0.87	0.84
Southeast Asia	800	0.59	0.77	0.82
Total	8588	0.60	0.84	0.85



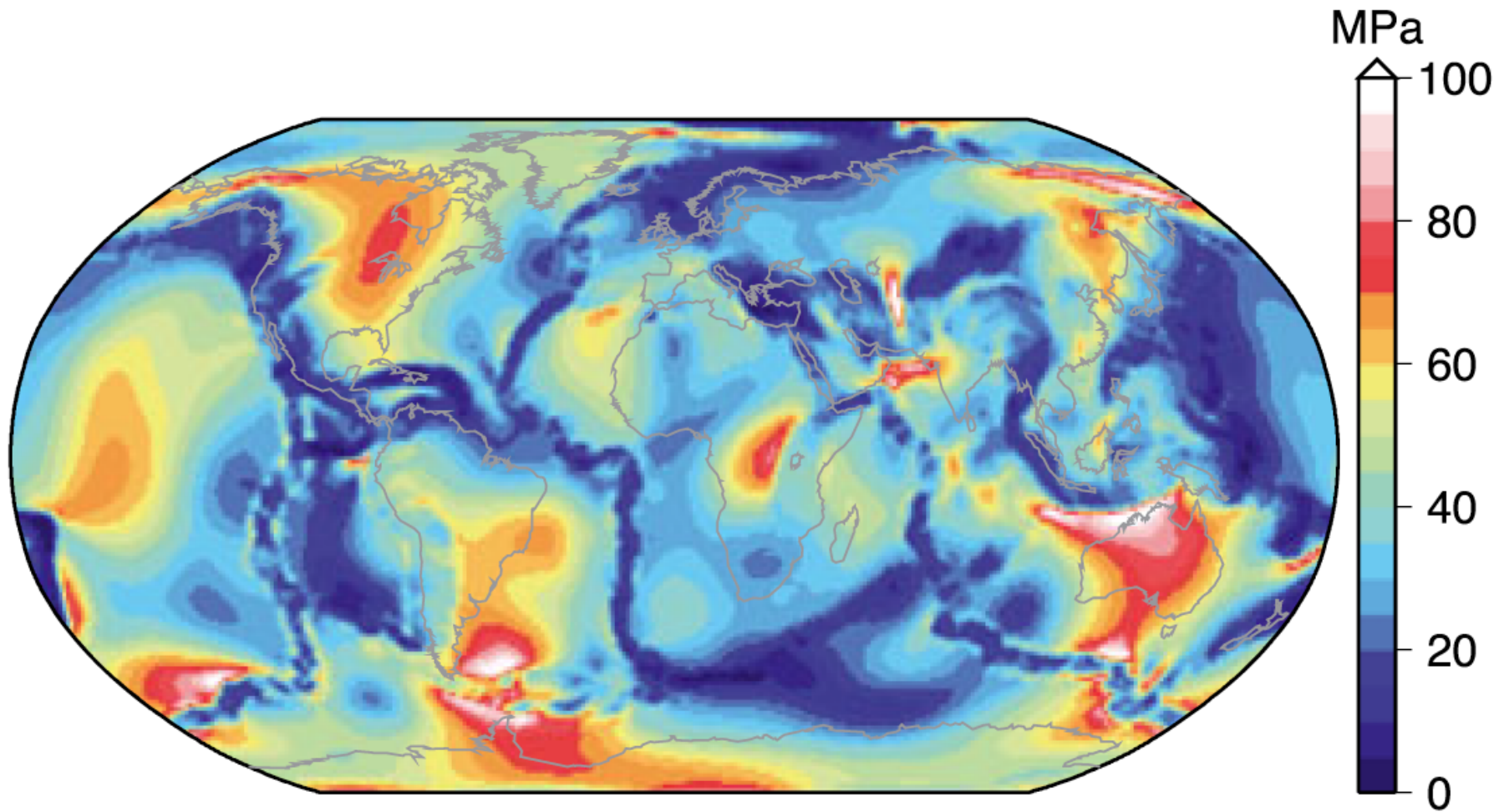
Comparison with
World Stress Map

D

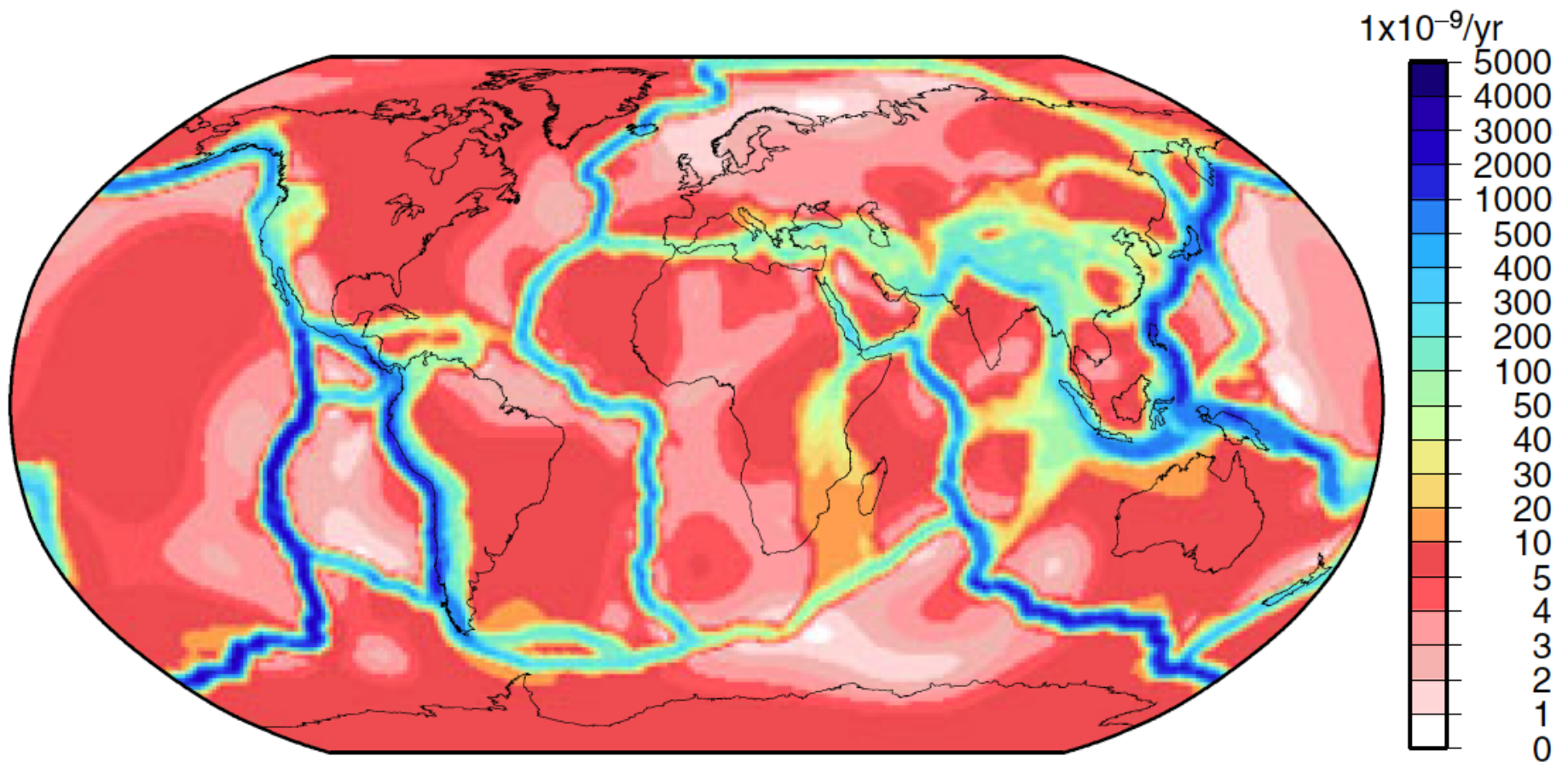


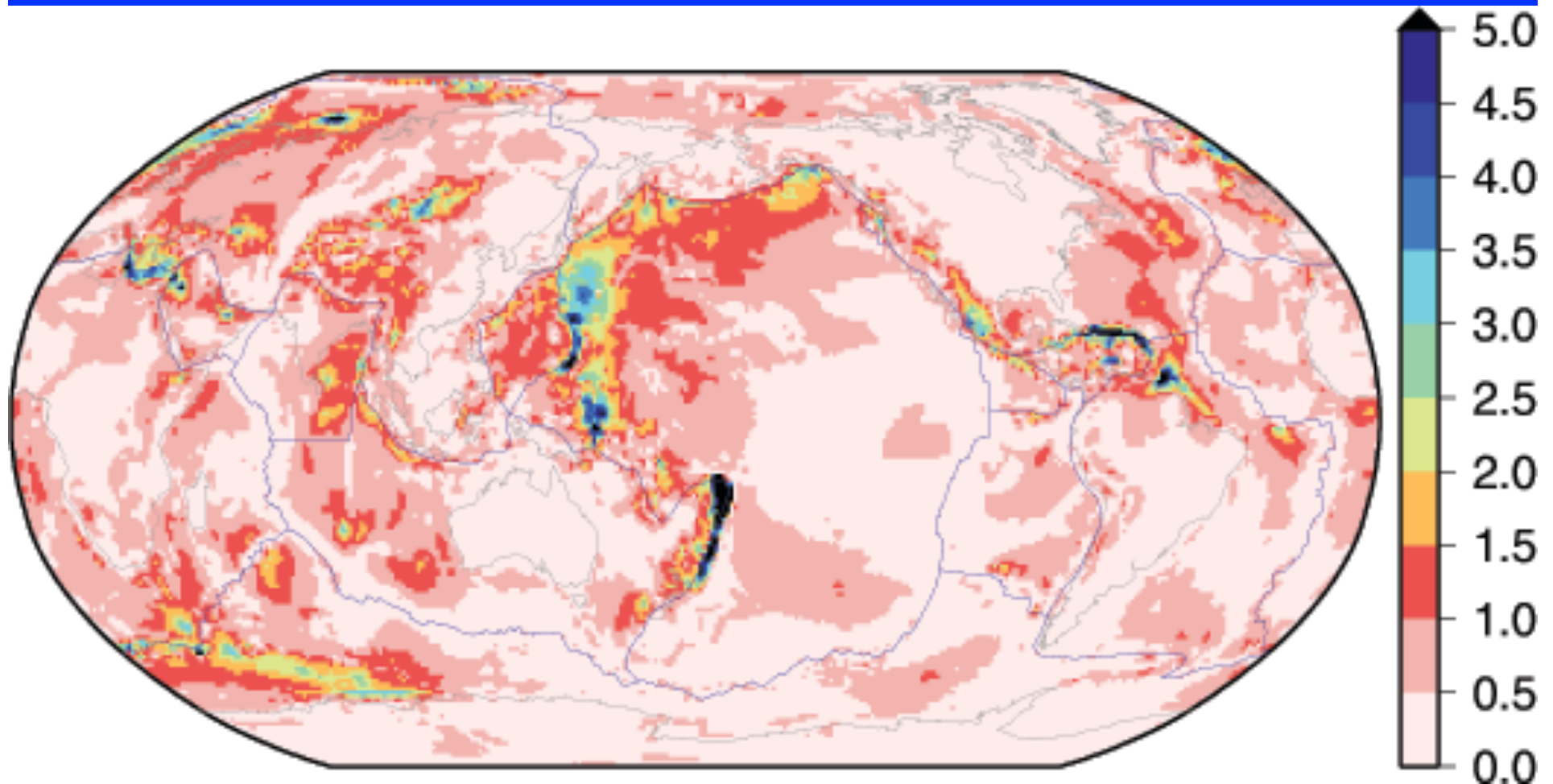
Tractions at base of lithosphere imposed by mantle flow
Ghosh and Holt [2012] Science

Second Invariant of Deviatoric Stresses



Strain Rates

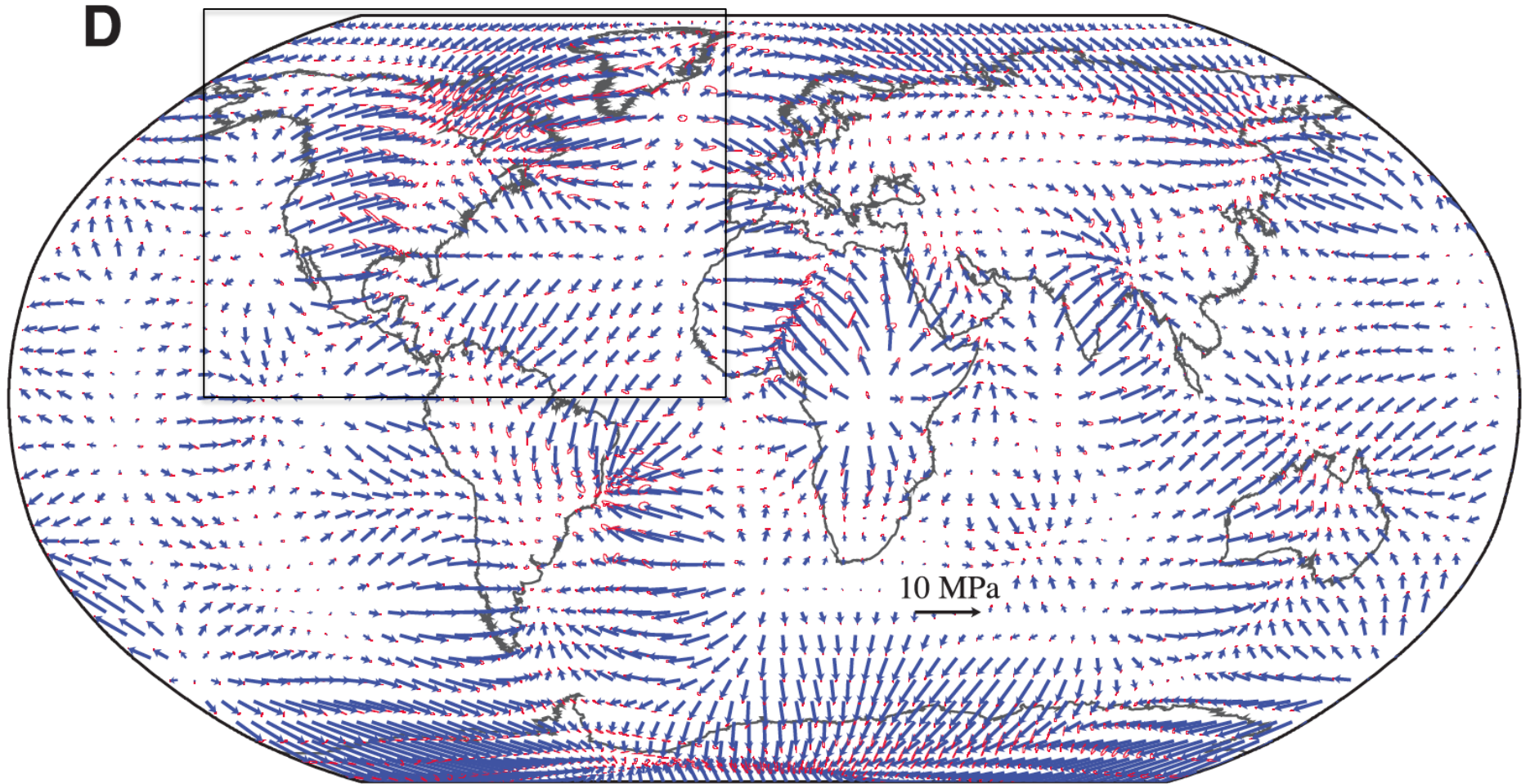




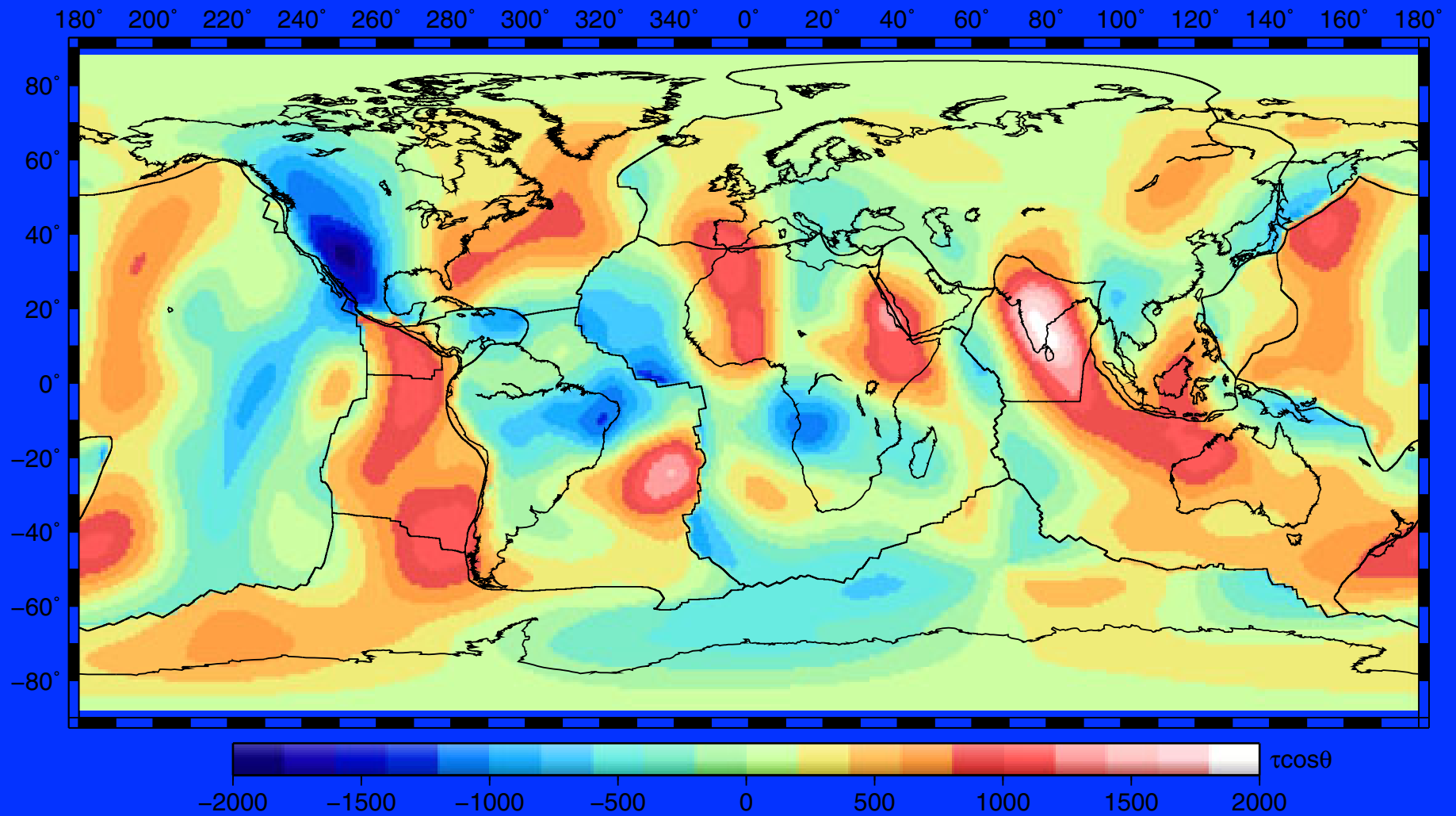
$T(\text{GPE})/T(\text{Tractions})$

Tractions from mantle flow $\sim 60\%$

Lithosphere topography and structure $\sim 40\%$



Tractions at base of lithosphere imposed by mantle flow
Ghosh and Holt [2012] Science



Tractions are both resistive and driving

Ghosh et al., JGR (2013)

Bottom Line

- Mantle leads the lithosphere (driving tractions) beneath major orogenic zones (Andes/Nazca, India, Eastern U.S.)
- Traction integrate and provide important component to global force-balance of stress
- Observations require tractions 1-5 MPa, which provides traction-associated stresses that are of similar magnitude as GPE-associated stresses (1-4 TN/m).
- History of subduction is key in the mantle flow picture and therefore in global force balance
- Slabs, however, provide no stress guide effect that impact stresses within the plates

Bottom Line, Continued

- Depth integrated deviatoric stress magnitudes of 1-4 TN/m for plate boundary zones implies that weakening mechanisms (weak faults, presence of water in upper mantle, etc.) are required for strain accommodation within plate boundary zones.
- Rapidly deforming plate boundary zones are weaker than the more slowly deforming plate boundary zones