

**Introduction to
DynEarthSol2D/3D
and
How to make
Coulomb angle-oriented
shear bands**

Eunseo Choi

Center for Earthquake Research and Information
University of Memphis

Outline

- DynEarthSol2D/3D
 - Key algorithmic components of DynEarthSol2D.
 - Validation and verification by benchmarks.
 - Challenges with 3D extension:
 - parallelization
 - meshing/remeshing.
- Strain localization: How to get shear bands oriented at the Coulomb angle.

Collaborators

Eh Tan

Academica Sinica, Taiwan

Luc Lavier

University of Texas, Austin

Victor M. Calo

KAUST, Saudi Arabia

Byunghyun Jang

University of Mississippi

Md. Sabber Ahamed

CERI, University of Memphis

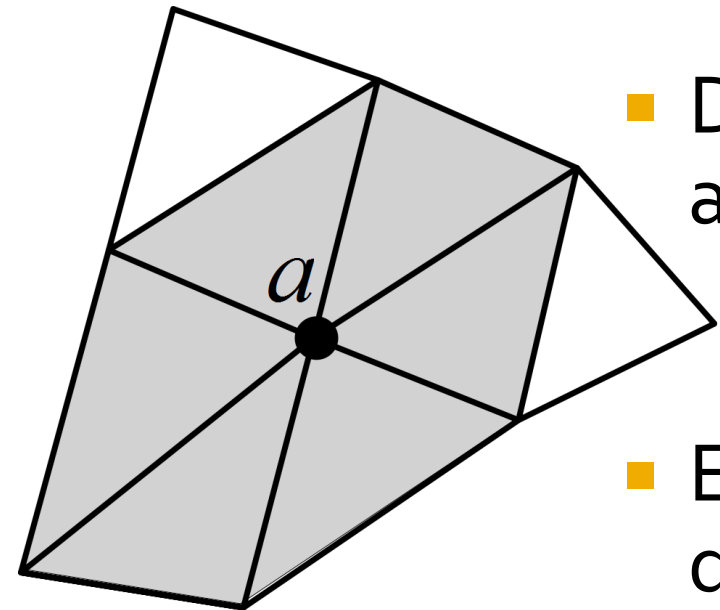
Motivations: Desirable Features

- Fast Lagrangian Analysis of Continua (FLAC)
 - Based on algorithms proposed by Cundall (1989).
 - A long list of successful applications.
 - Many variants out there.
 - FYI, one version being maintained as an open source: <https://bitbucket.org/tanz2/flac>
 - OpenMP-parallel. Shows a good scaling.
- Unstructured meshes are often desirable for a wider range of applications and computational efficiency.

Key Components of DynEarthSol2D

- **Dynamic Earth Solver** for 2D.
- Principle of virtual power

$$0 = \int_{\Omega} \delta \mathbf{v} \left(\rho \frac{\partial \mathbf{v}}{\partial t} \right) d\Omega - \int_{\Omega} \nabla(\delta \mathbf{v}) : \boldsymbol{\sigma} d\Omega - \int_{\Omega} \delta \mathbf{v} \rho \mathbf{g} d\Omega$$



- Discretized momentum equation after the standard FE procedure

$$m_a \mathbf{a}_a = \mathbf{F}_a^{int} + \mathbf{F}_a^{ext}$$

- Energy balance equation is discretized similarly.

Key Components of DynEarthSol2D

- Unstructured mesh created by
 - `triangle` (<http://www.cs.cmu.edu/~quake/triangle.html>) in 2D
 - `tetgen` (<http://wias-berlin.de/software/tetgen/>) in 3D.
- **Lagrangian** description of motion with *explicit* time integration.

$$\mathbf{v}_a^{(t+\Delta t/2)} = \mathbf{v}_a^{(t-\Delta t/2)} + \mathbf{F}_a^{(t)} \frac{\Delta t}{m_a}$$

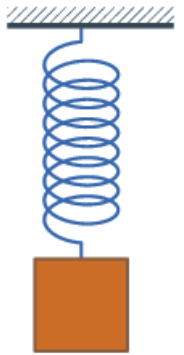
$$\mathbf{x}_a^{(t+\Delta t)} = \mathbf{x}_a^{(t)} + \mathbf{v}_a^{(t+\Delta t/2)} \Delta t$$

Key Components of DynEarthSol2D

- **Dynamic relaxation** for (quasi-)static solutions
 - Local damping

$$v_a^{i,(t+\Delta t/2)} = v_a^{i,(t-\Delta t/2)} + (F_a^{i,(t)} + F_d^i) \frac{\Delta t}{m_a},$$

where $F_d^i = -\alpha |F_a^{i,(t)}| \text{sgn}(v_a^i)$, where $0 \leq \alpha < 1$.

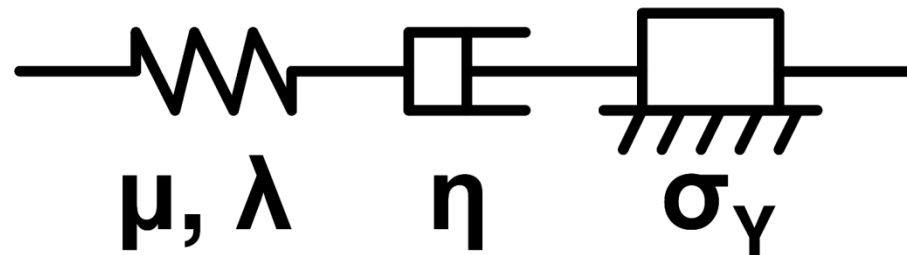


- **Mass scaling** for a large and stable Δt

$$\Delta t < \frac{\Delta x}{v_p} \quad v_p = \sqrt{\frac{K}{m_s}} \quad m_s \gg m_g = \int \rho dV$$

Key Components of DynEarthSol2D

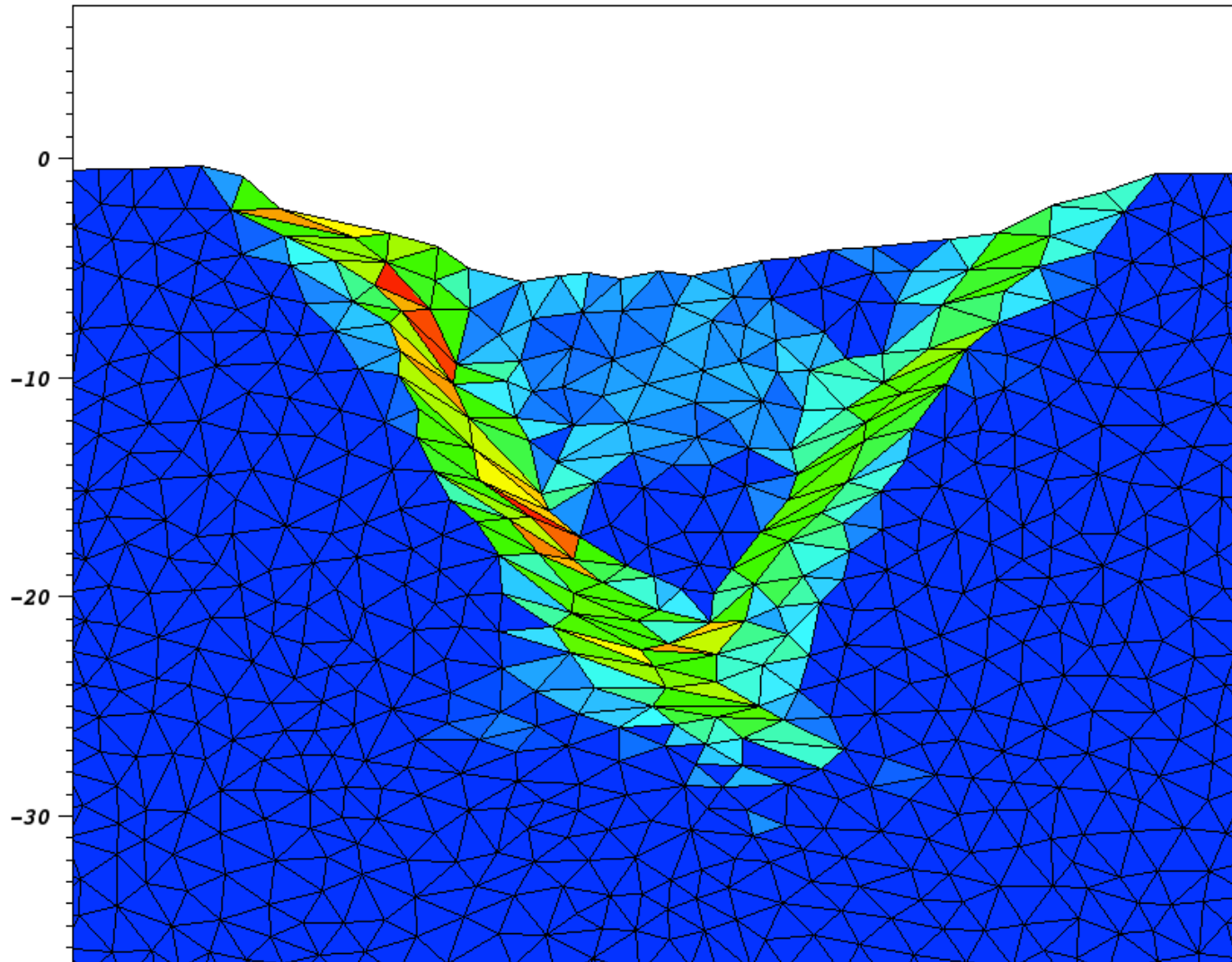
- Constitutive model: **elasto-visco-plastic**



- $\eta \rightarrow \infty$: Mohr-Coulomb plasticity.
- $\sigma_Y \rightarrow \infty$: Maxwell viscoelasticity.
- $\eta = \eta(T, \sigma)$: temperature-determined brittle-ductile transition
- $\sigma_Y = \sigma_Y(\epsilon^*)$: strain hardening/softening

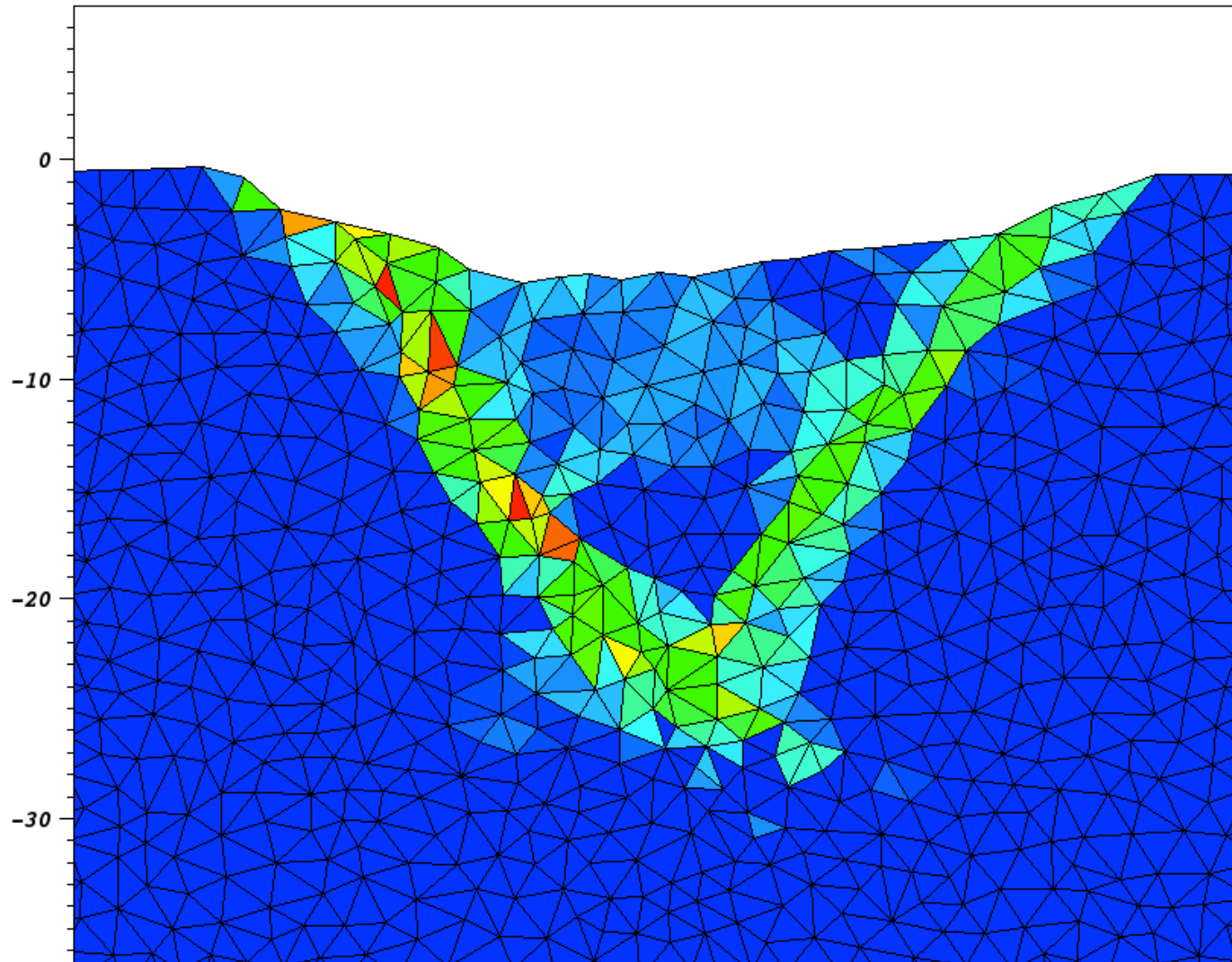
Key Components of DynEarthSol2D

- Remeshing



Key Components of DynEarthSol2D

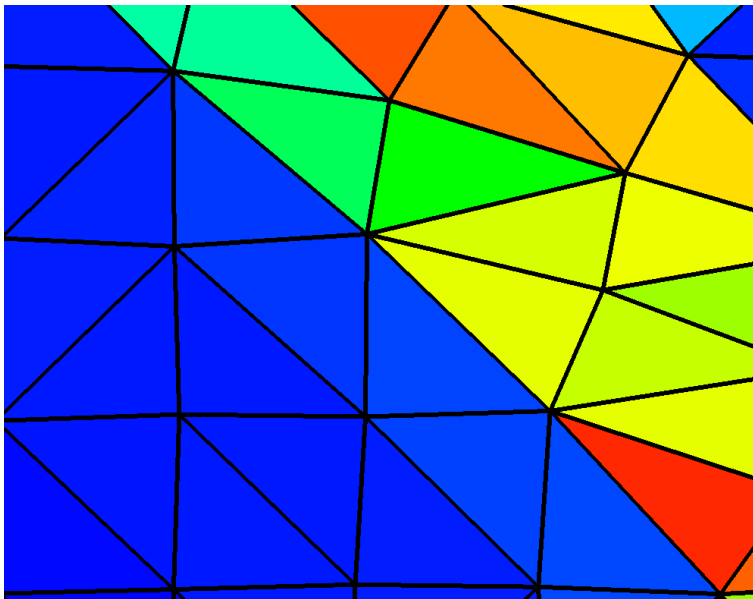
- Remeshing



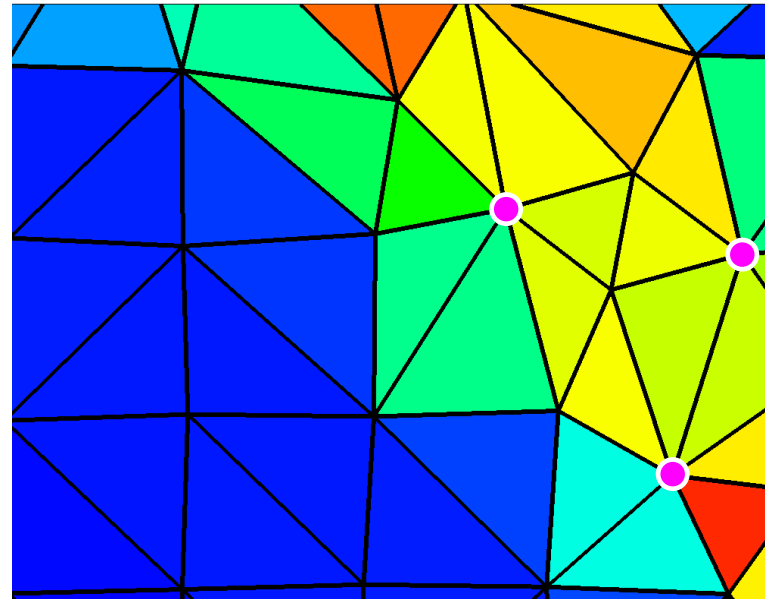
Key Components of DynEarthSol2D

- Remeshing by **edge-flipping** and **node addition/subtraction** (via *triangle* library by Shewchuk)

Before



After

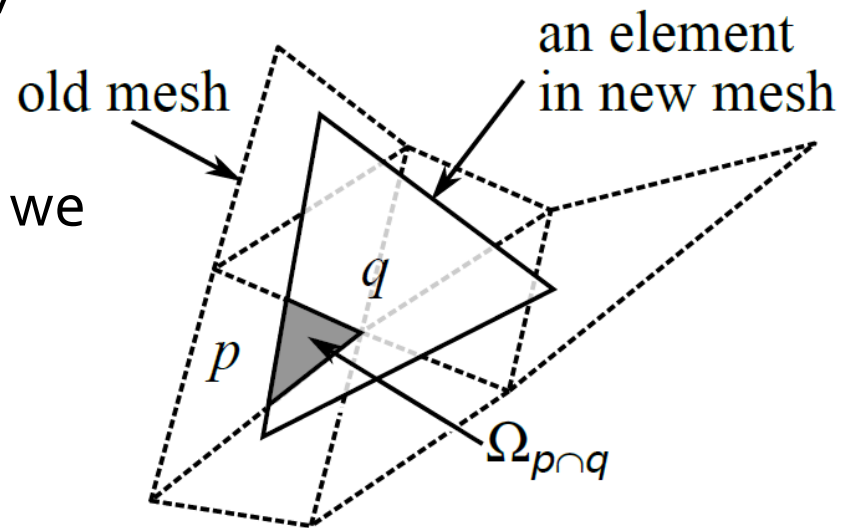


Low  High

Key Components of DynEarthSol2D

- Remeshing (cont'd)

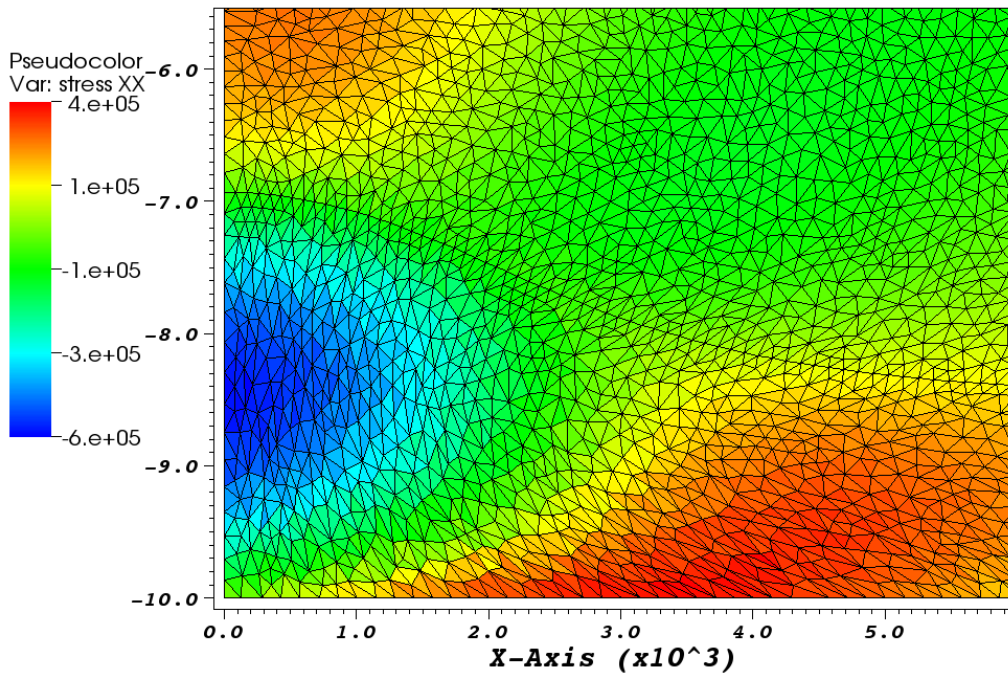
- Fields defined on nodes are easily interpolated.
- For quadrature-registered fields, we tried one of the conservative mappings: **Local supermesh construction** (Farrel & Maddison, CMAME, 2011) implemented in `Fluidity` library (Davies et al., G3, 2011).



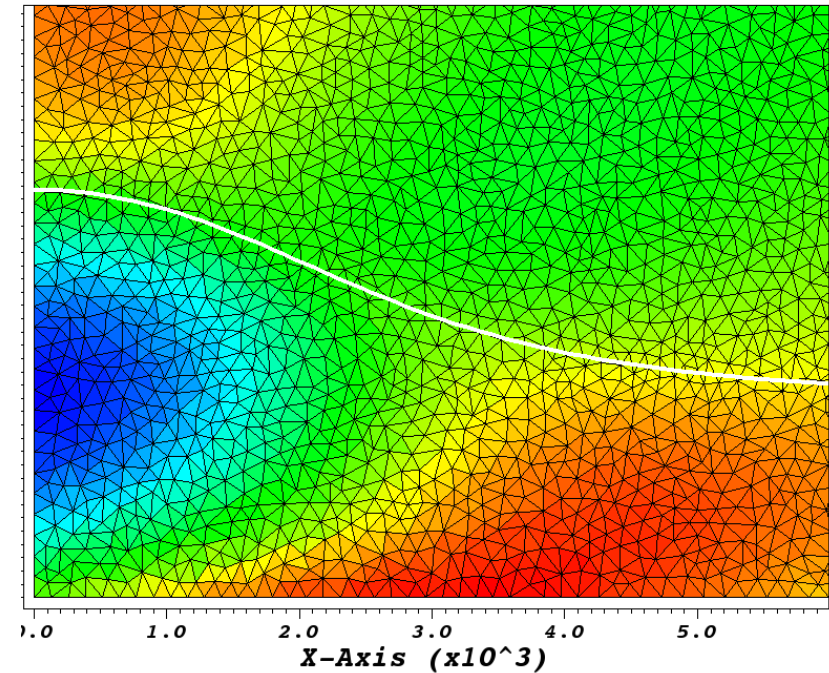
Key Components of DynEarthSol2D

- Remeshing (cont'd)
 - Mapping of smooth fields

Before



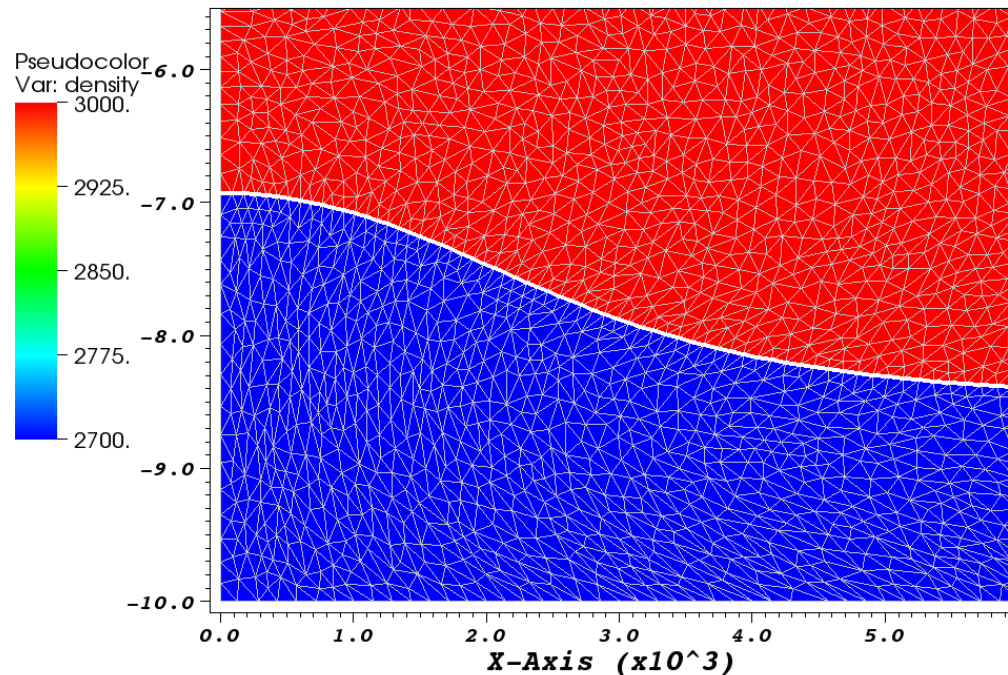
After



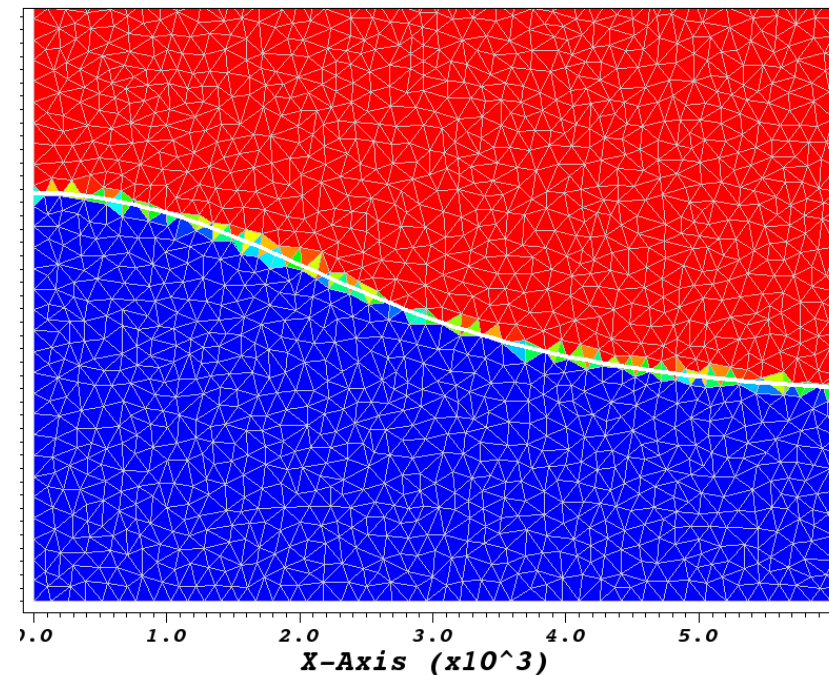
Key Components of DynEarthSol2D

- Remeshing (cont'd)
 - Mapping of sharp boundaries: **Markers** further needed.

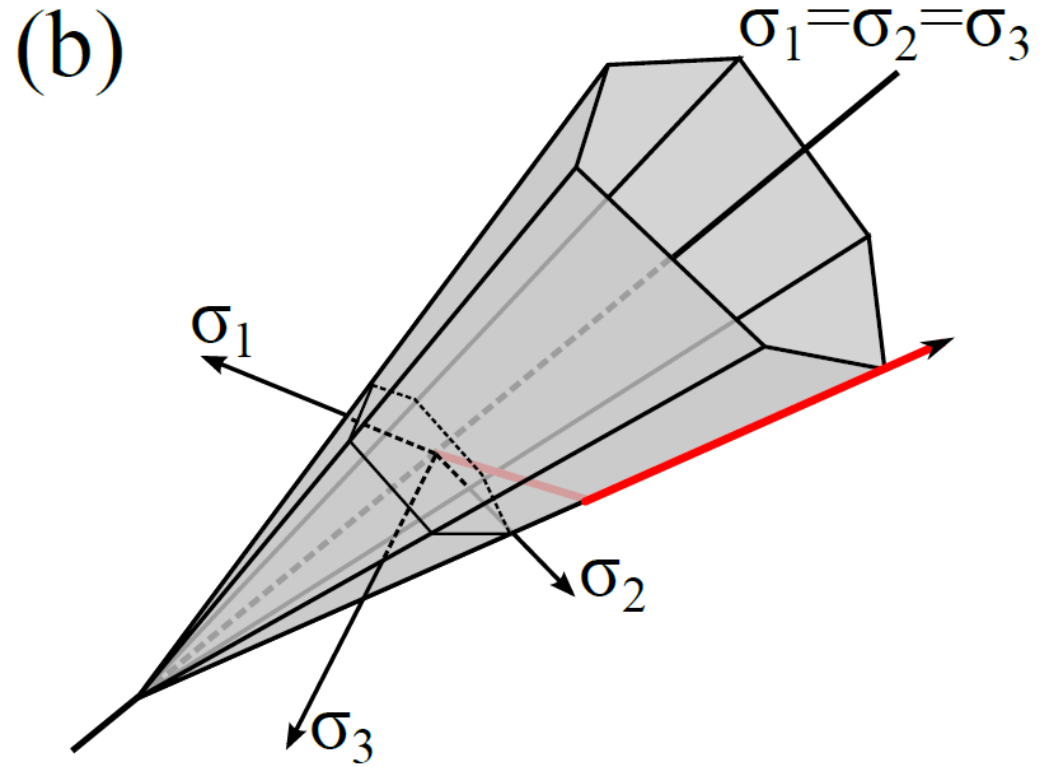
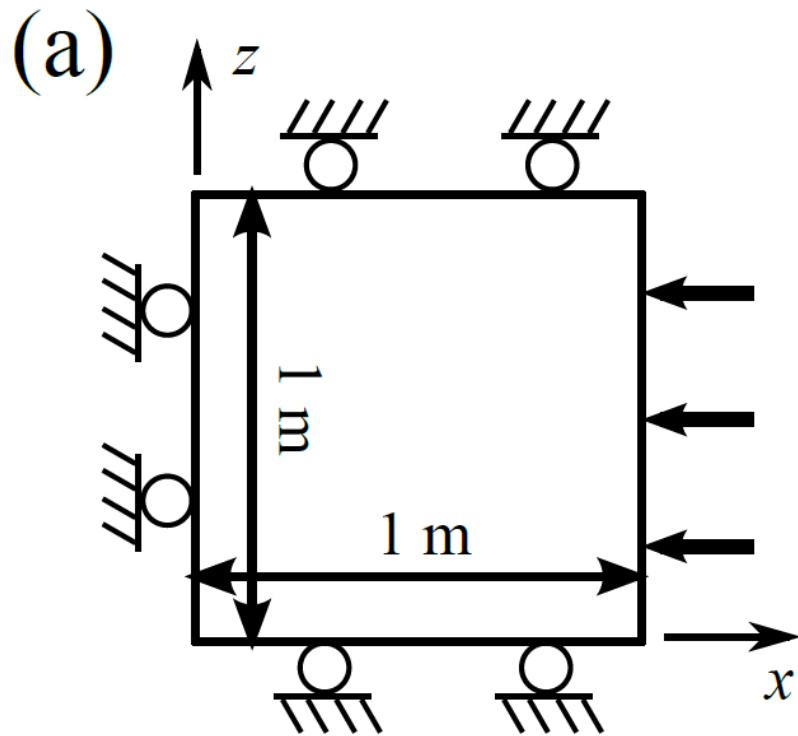
Before



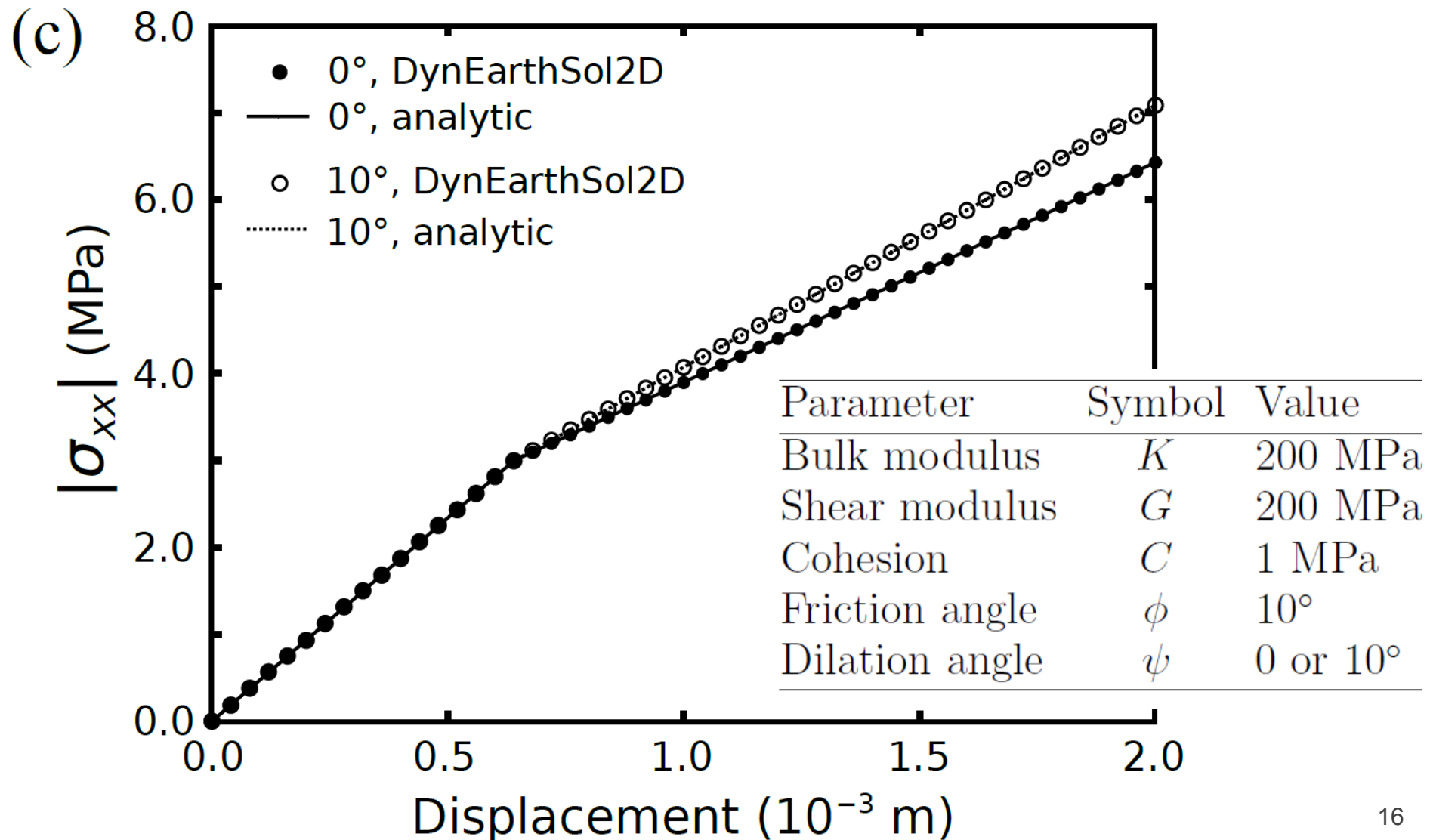
After



Benchmarks: Plastic Oedometer

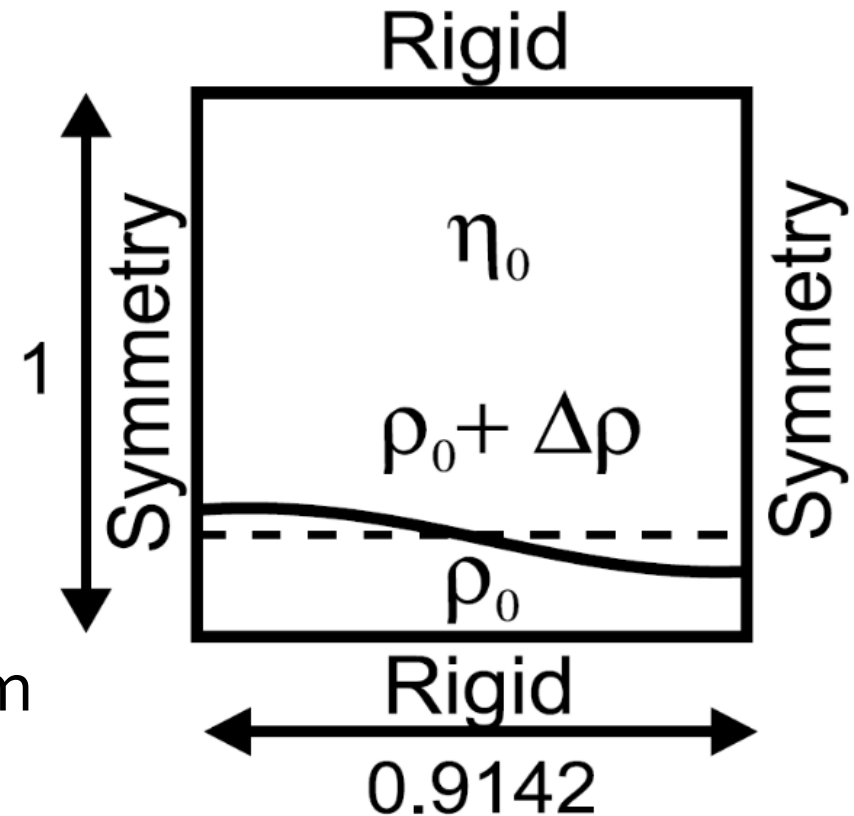


Benchmarks: Plastic Oedometer




Benchmarks: Rayleigh-Taylor Instability

- $G = 30 \text{ GPa}$, $\nu = 0.25$
- $g = 10 \text{ m/s}^2$
- $\eta = 10^{17} \text{ Pa}\cdot\text{s}$
- $\rho_o = 2700$,
 $\Delta\rho = 300 \text{ kg/m}^3$
- Length scale factor: 10 km
- Resolution: $\sim 100 \text{ m}$



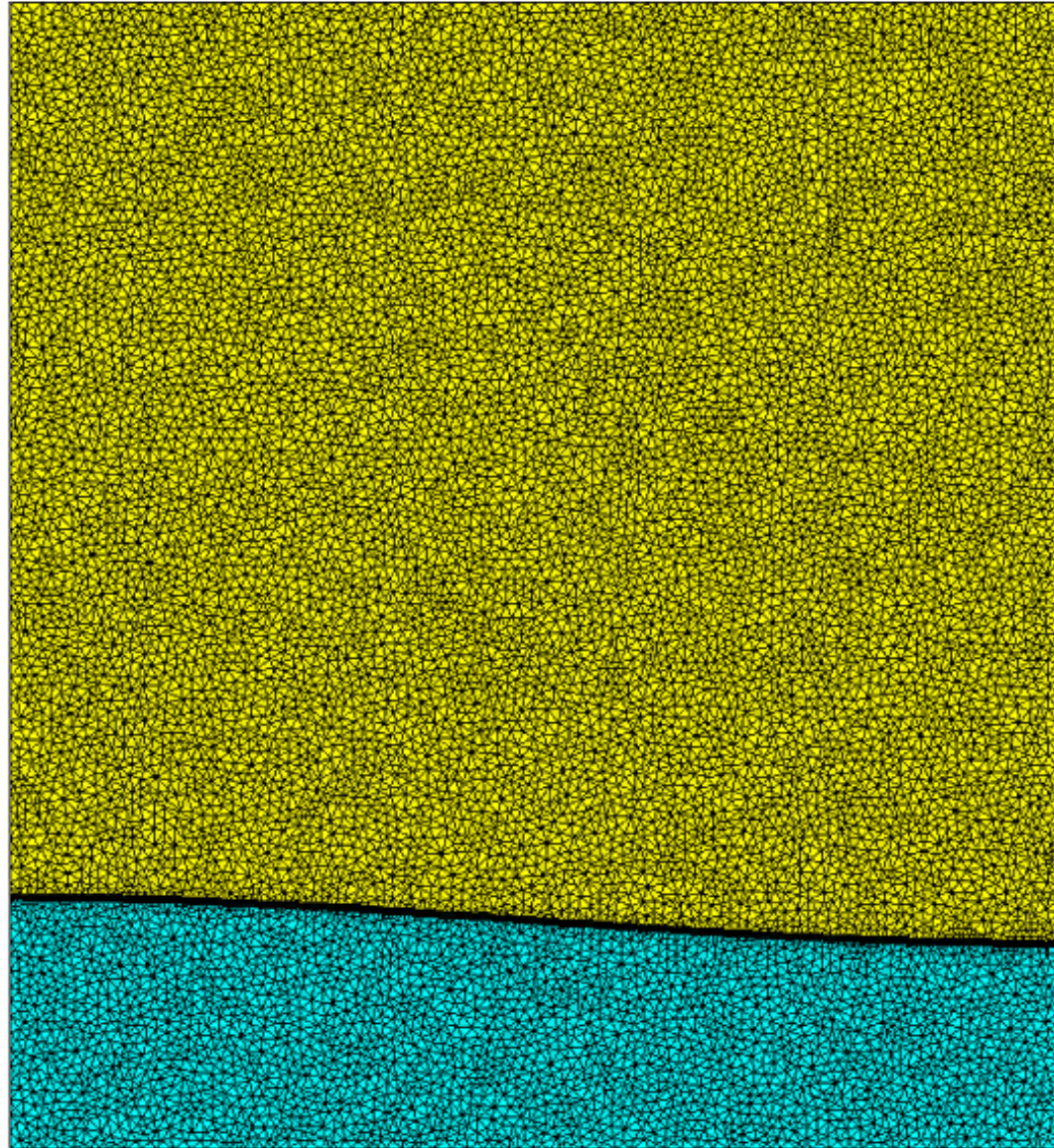
Benchmarks: Rayleigh-Taylor Instability

Pseudocolor
Var: density



3000.
2850.
2700.

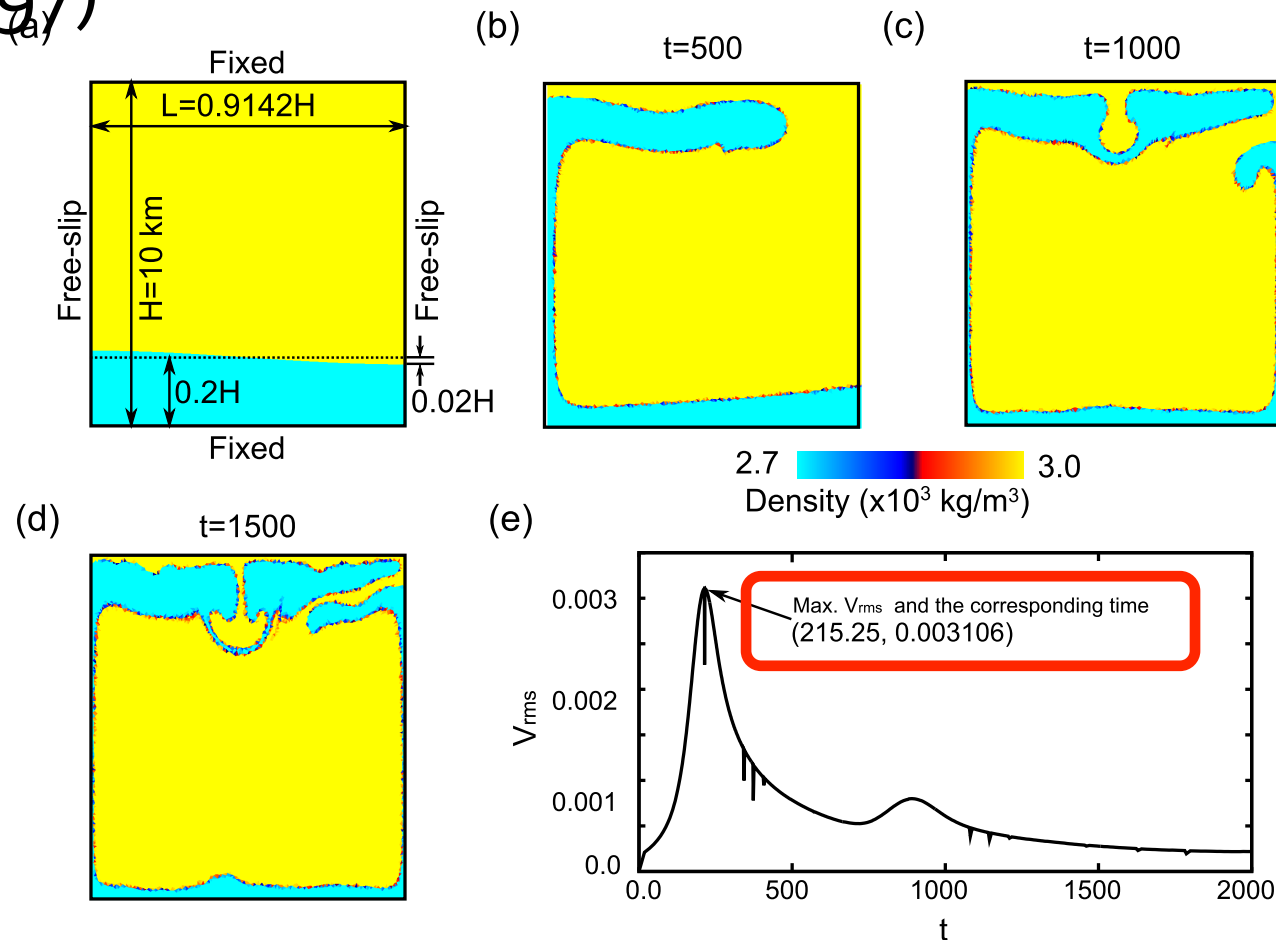
A vertical color bar legend for density. The top is yellow (3000), transitioning through orange and red to a dark blue (2850), and then to a light cyan (2700).



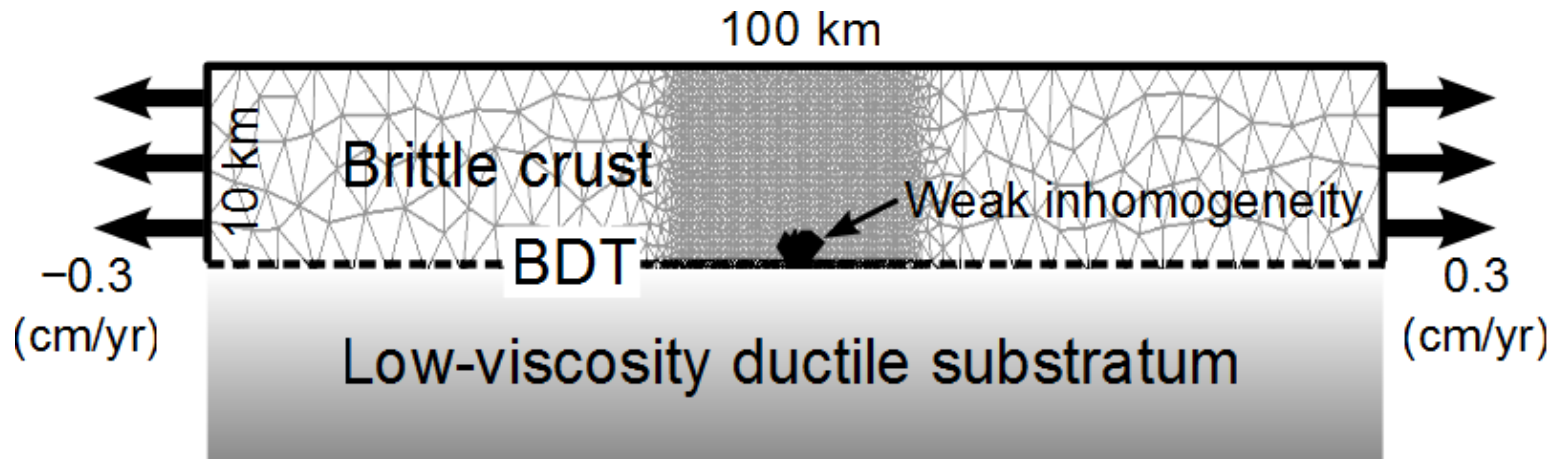
Benchmarks: Rayleigh-Taylor Instability

- 1st peak of v_{rms} is within the range reported in the benchmark study by Van Keken et al.

(1997)

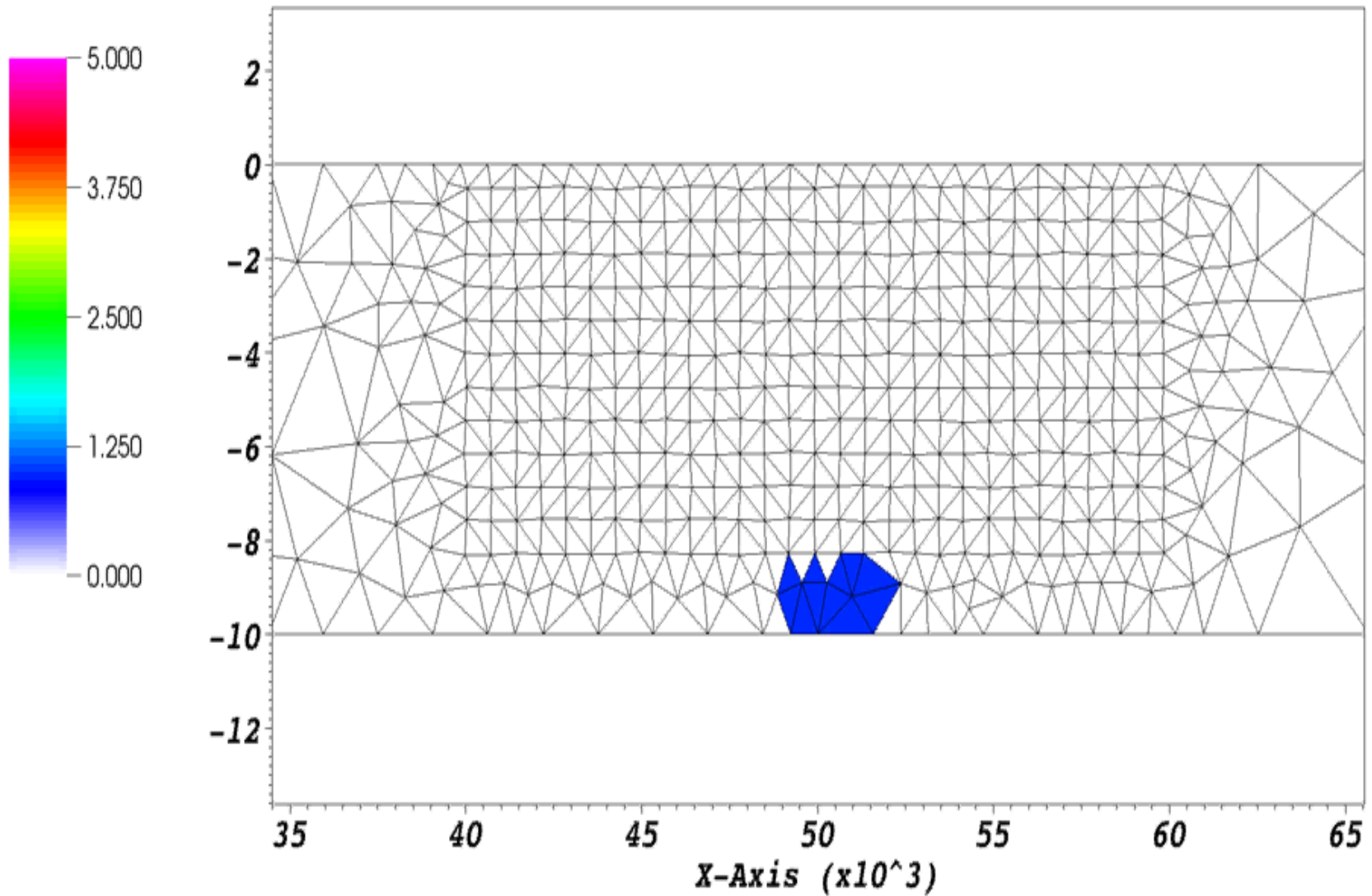


Benchmarks: Fault Evolution

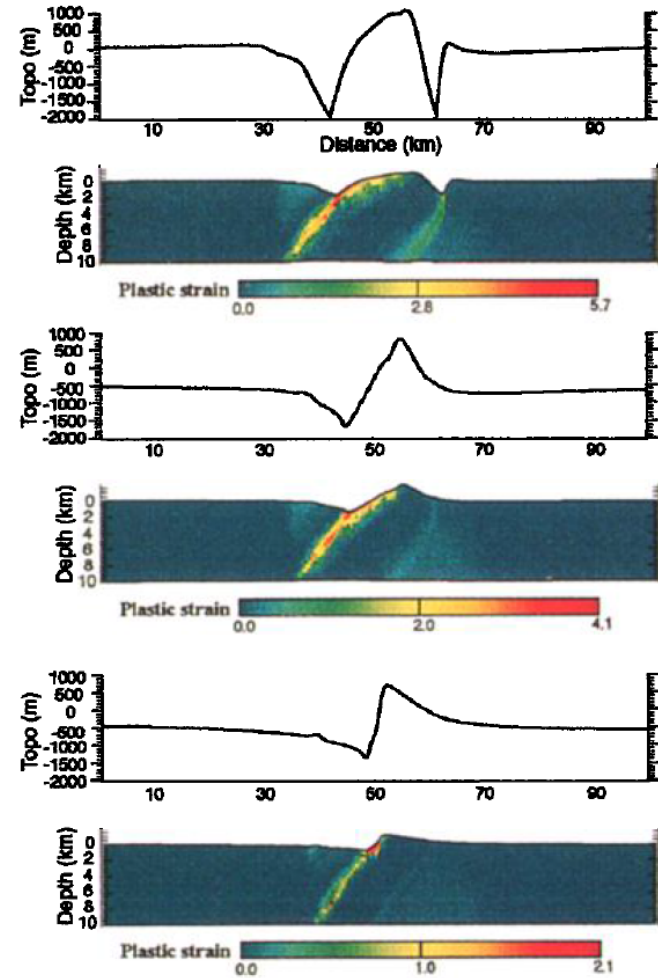
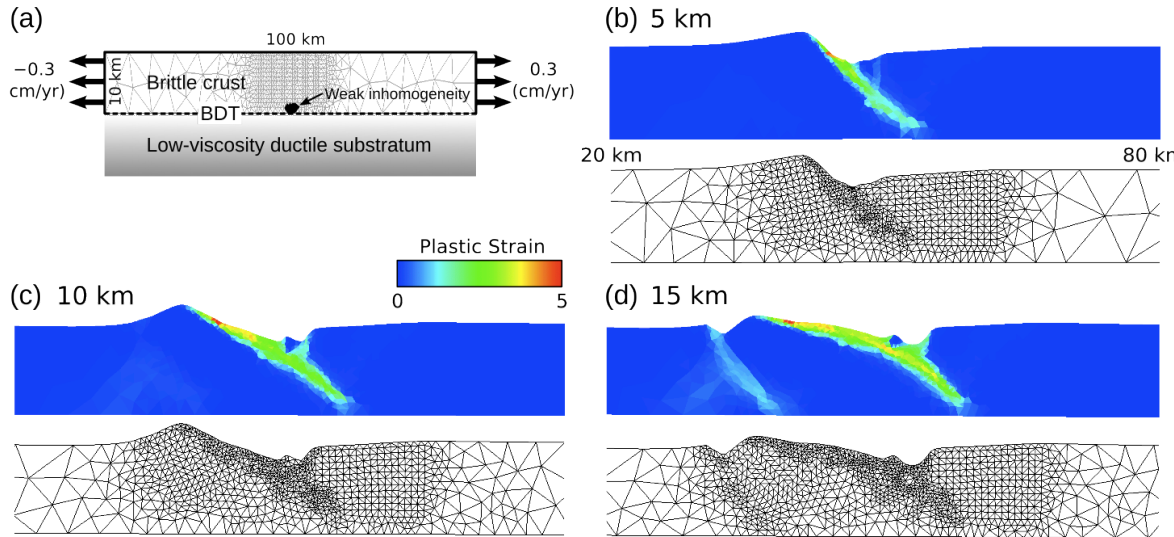


- Lamé's constants: 30 GPa.
- More-Coulomb plasticity:
 - Friction angle = 30°
 - Initial Cohesion = 20 Mpa
 - Strain softening:
 - Cohesion 20 \rightarrow 4 Mpa as pl. strain increases to 5.0.

Benchmarks: Fault Evolution



Benchmarks: Fault Evolution



(Lavie et al., JGR, 2000)

- Reproduced the “footwall snapping” mode.
- Contingent **dynamic mesh refinement** along shear zones.

Challenges with 3D version

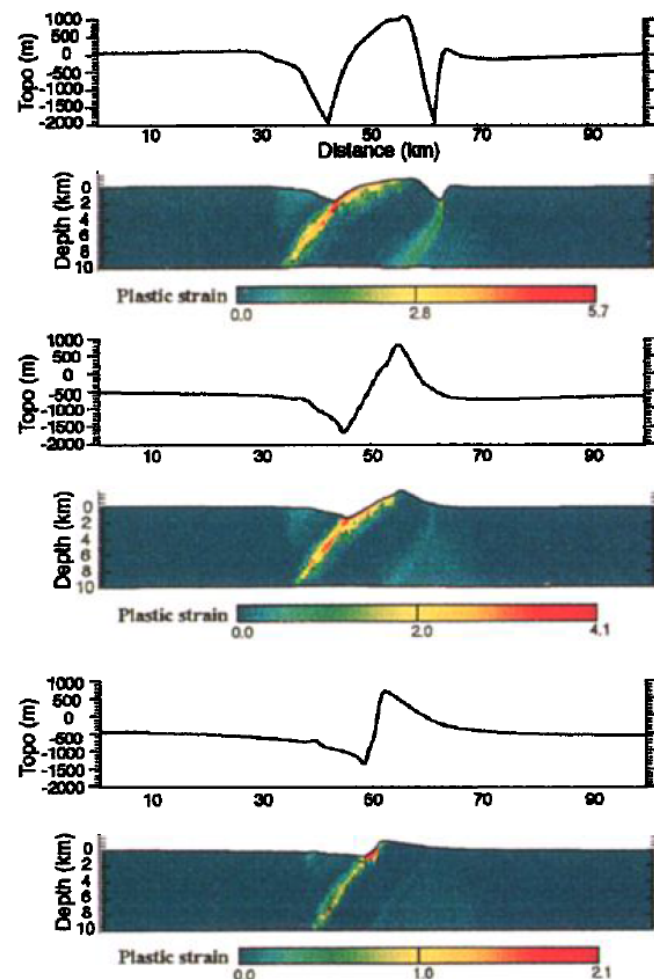
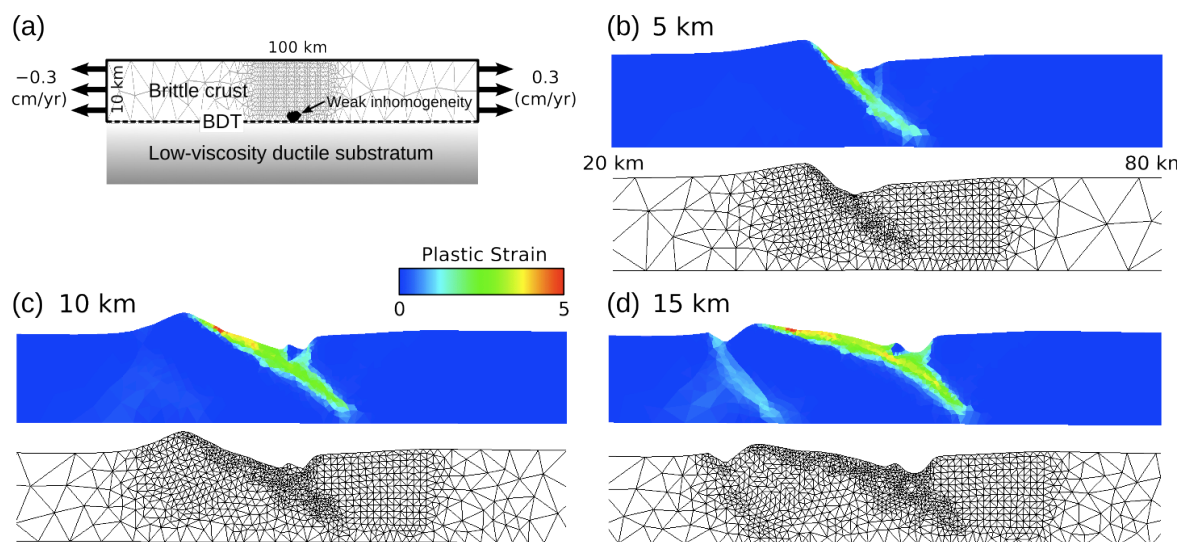
- Important operations become much slower than in 2D:
 - Remeshing with `tetgen` → Local modification.
 - Local supermesh construction → Markers only.
- Parallelization
 - For performance gain with domain decomposition, each time step \gg MPI overhead. However, in DynEarthSol3D, each time step $<$ MPI overhead even for a decent size of model.
 - Thread-level parallelism with OpenMP.
 - For massive thread generation, trying out co-processors (e.g., GPGPU and Intel Xeon Phi).

Summary

- DynEarthSol2D/3D
 - **Explicit, Lagrangian FE** code for **thermo-mechanical** modeling.
 - Open source:
<https://bitbucket.org/tanz2/dyneathsol3d>
<https://bitbucket.org/tanz2/dyneathsol2d>
 - **Dynamic relaxation** and **mass scaling** for (quasi-) static solutions.
 - **Unstructured, non-uniform mesh.**
 - **Elasto-visco-plastic** base rheology.
 - **Remeshing** for indefinite amount of deformation
 - Contingent **dynamic mesh refinement.**
 - **Benchmarked.**

Strain Localization at Coulomb Angle

- Strain localization is extremely useful for representing discontinuities like faults in continuum models.



Strain Localization at Coulomb Angle

- Sometimes, we want to predict the orientation of strain localization just as we want to predict fault orientation w.r.t. σ_1 .

- Coulomb angle

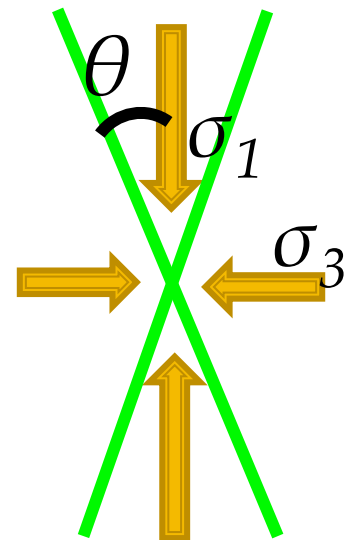
$$\theta = \frac{\pi}{4} - \frac{\phi}{2}$$

- Roscoe angle

$$\theta = \frac{\pi}{4} - \frac{\psi}{2}$$

- Arthur angle

$$\theta = \frac{\pi}{4} - \frac{\phi + \psi}{4}$$



Strain Localization at Coulomb Angle

- Meaning of dilation angle

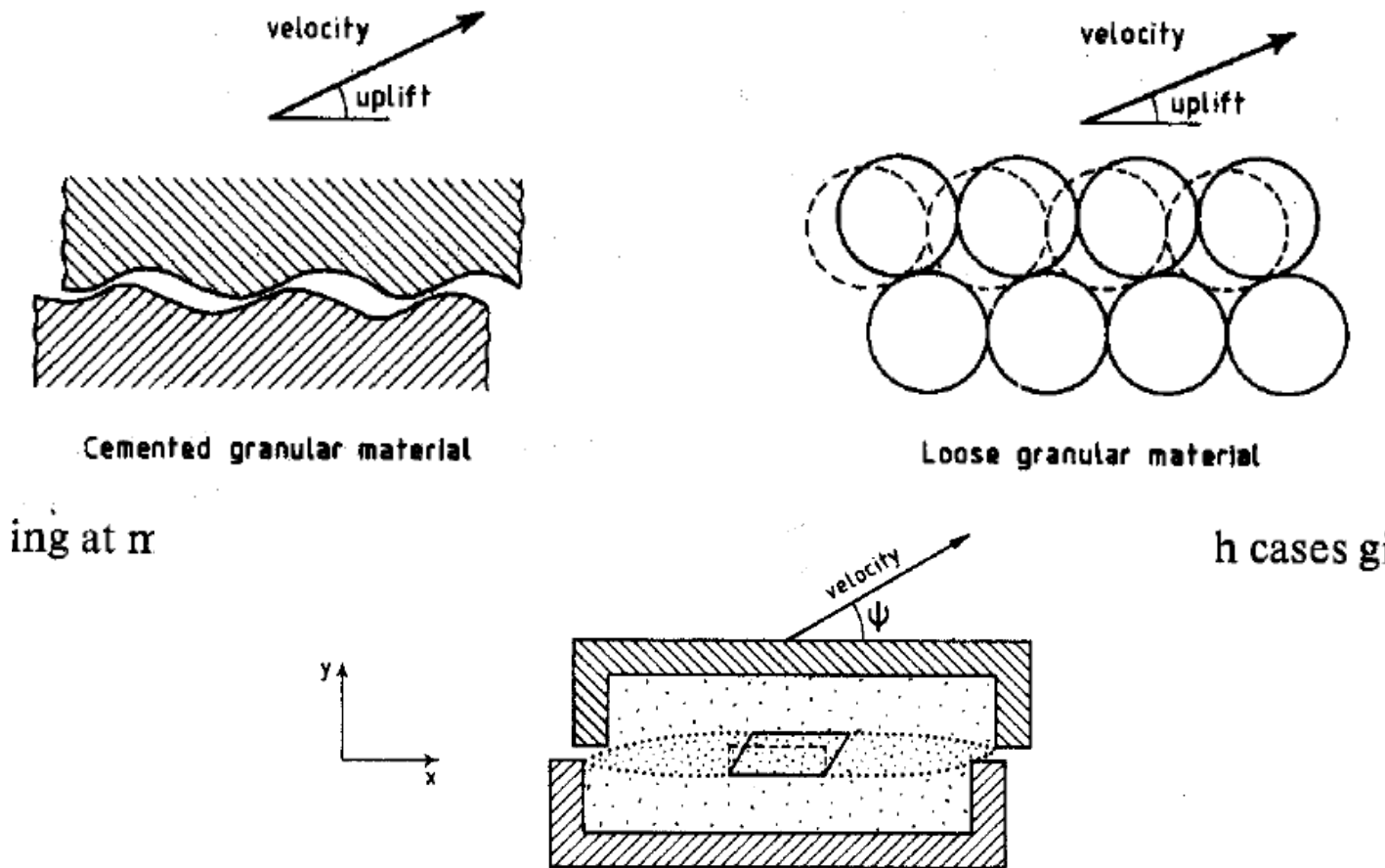
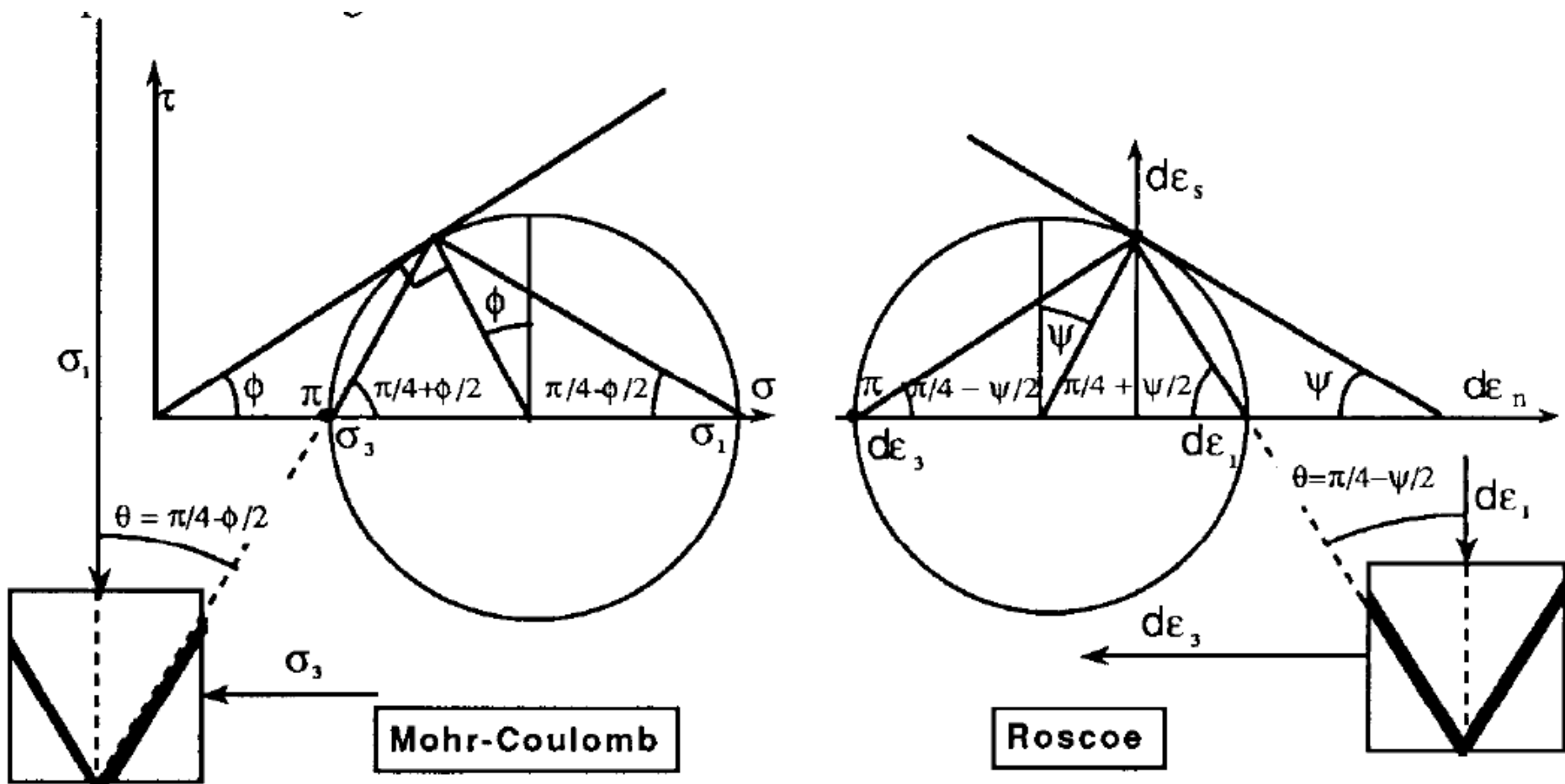


Fig. 4.2 The model predicts an uplift angle ψ for shear bands.

(Vermeer and de Borst, Heron, 1984)

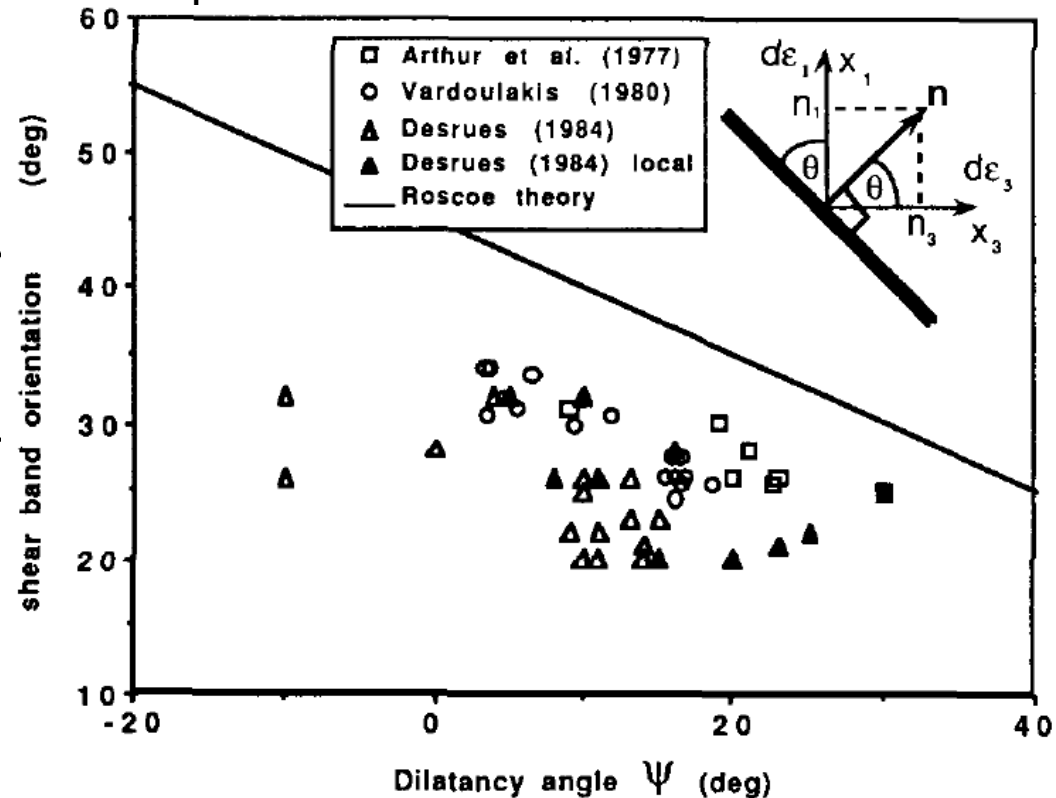
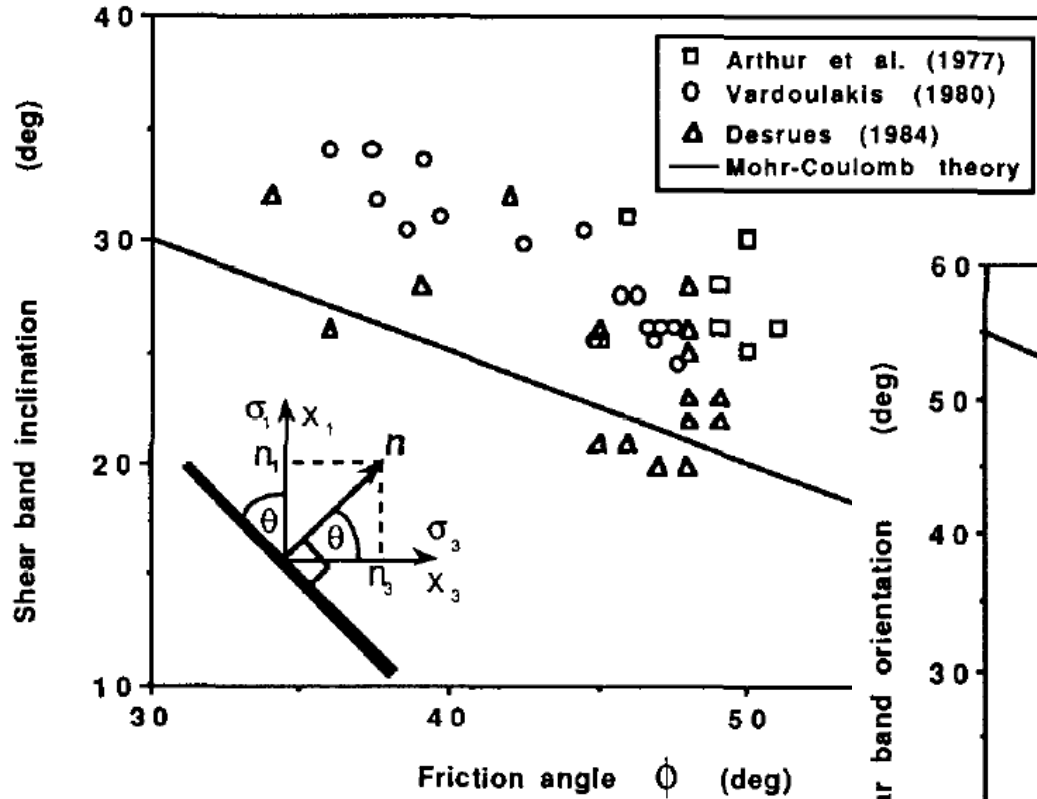
Strain Localization at Coulomb Angle

- Geometric derivation



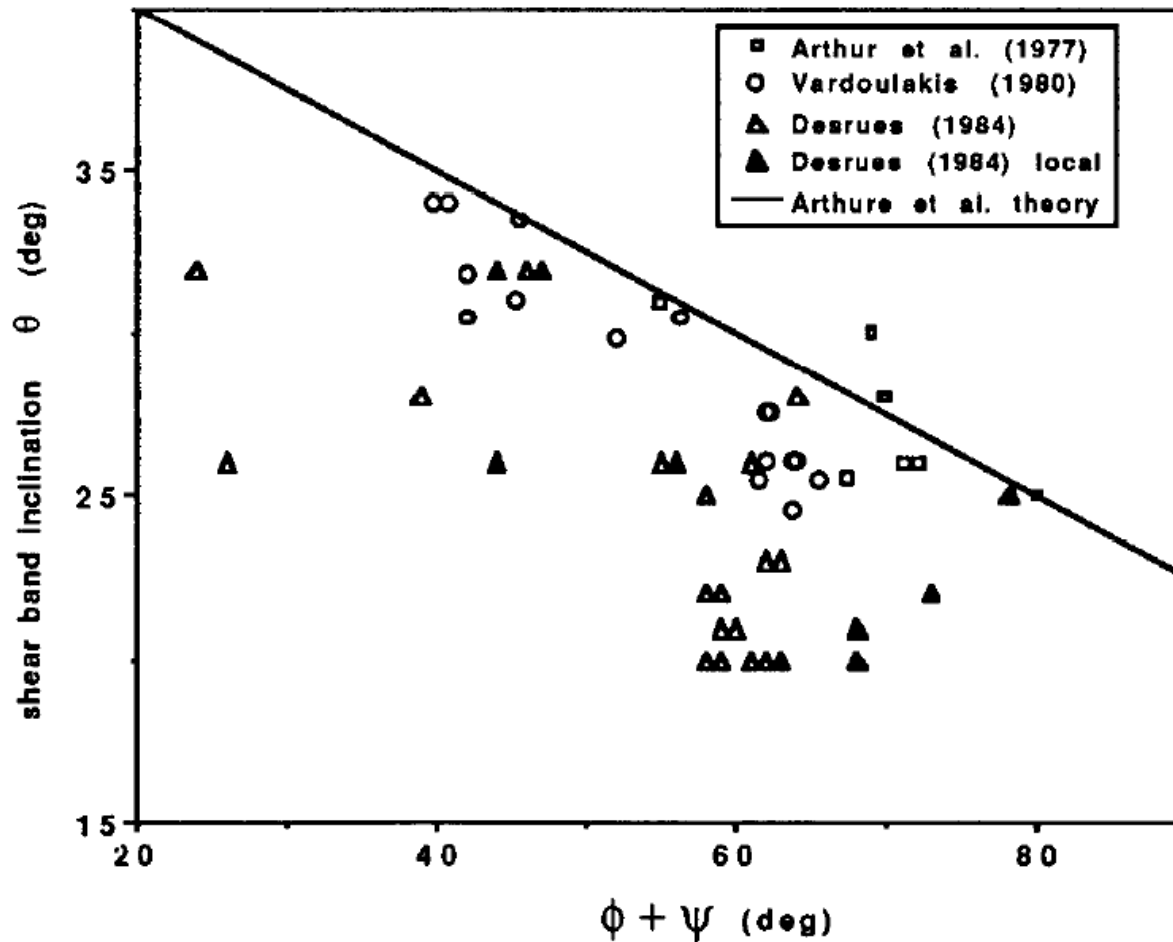
Strain Localization at Coulomb Angle

■ Comparison with experiments



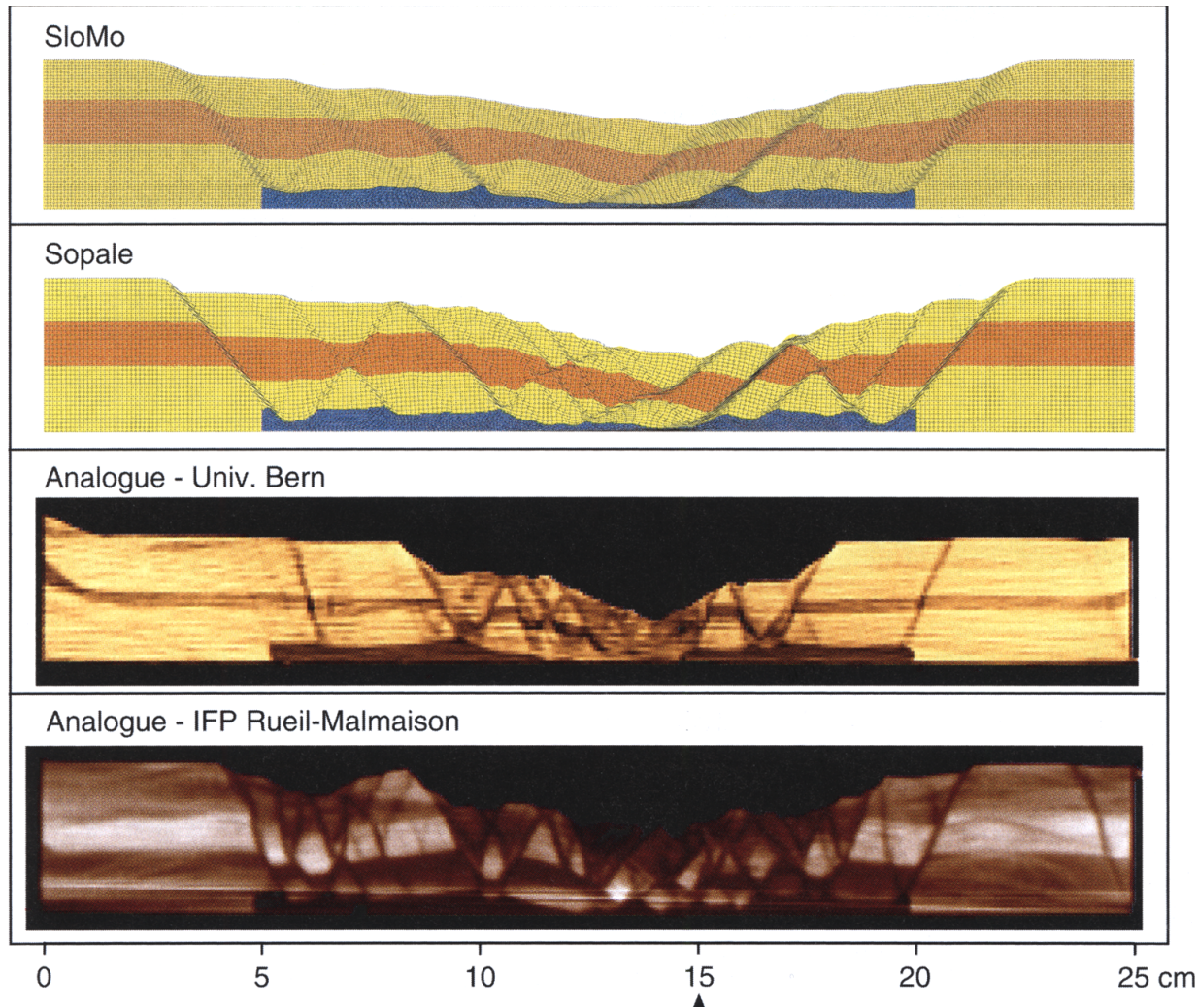
Strain Localization at Coulomb Angle

- Comparison with experiments



Strain Localization at Coulomb Angle

- Numerical and analogue models



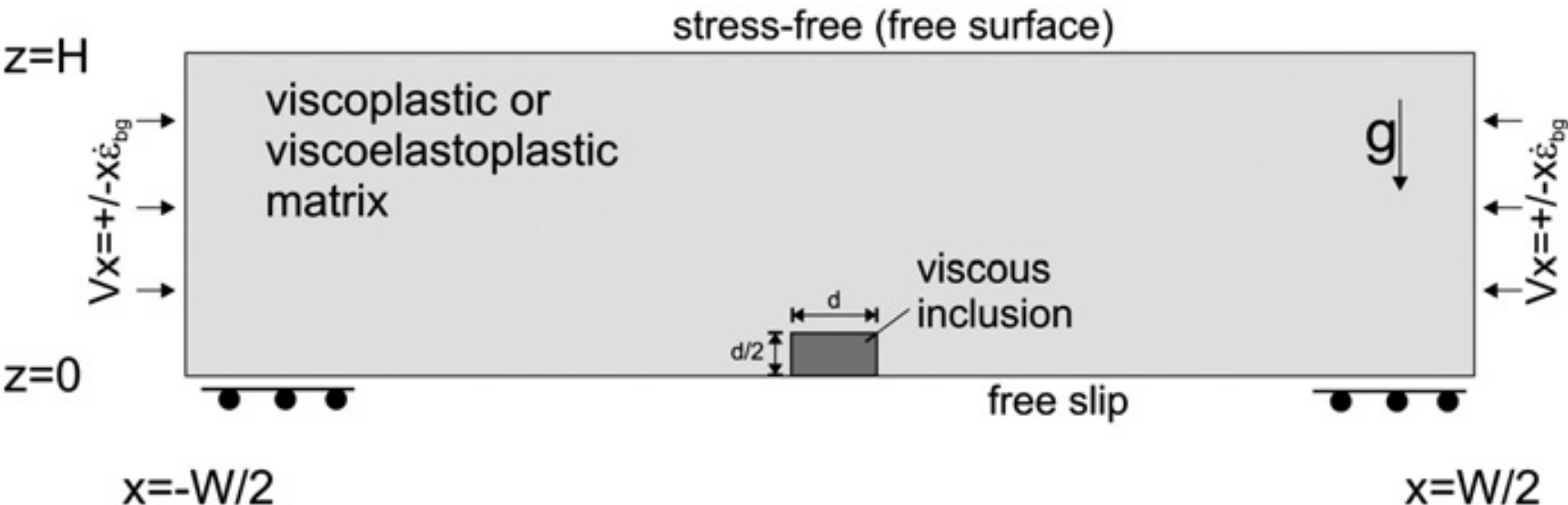
Numerical
Models

Analogue
Models

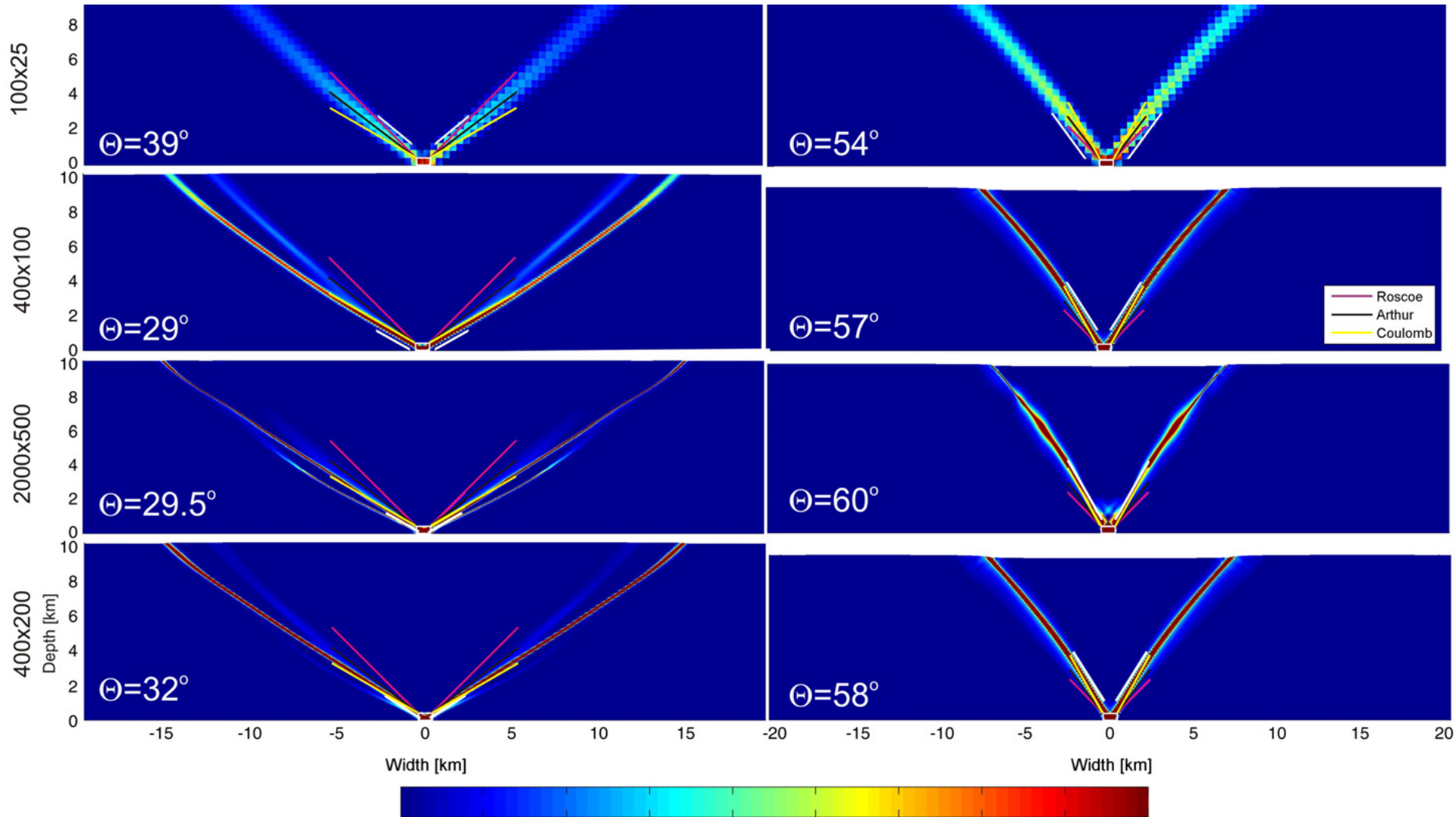
(Buiter et al., 2006)

Strain Localization at Coulomb Angle

- Numerical models compared with simple theories (Kaus, 2010).



Strain Localization at Coulomb Angle



Strain Localization at Coulomb Angle

- We have shear band orientations from theory, experiments and numerical models.
 - theory \neq experiments : maybe ok (blame theory!)
 - numerical models \neq experiments: maybe ok, too.
- What about theory \neq numerical models?
 - e.g.: shear band from the Mohr-Coulomb plasticity \neq the Coulomb angle
 - Problematic considering models are based on the theory.
 - This type of discrepancy is often termed “mesh dependence”.
 - Maybe not a critical issue but certainly inconvenient for some type of analysis.

Strain Localization at Coulomb Angle

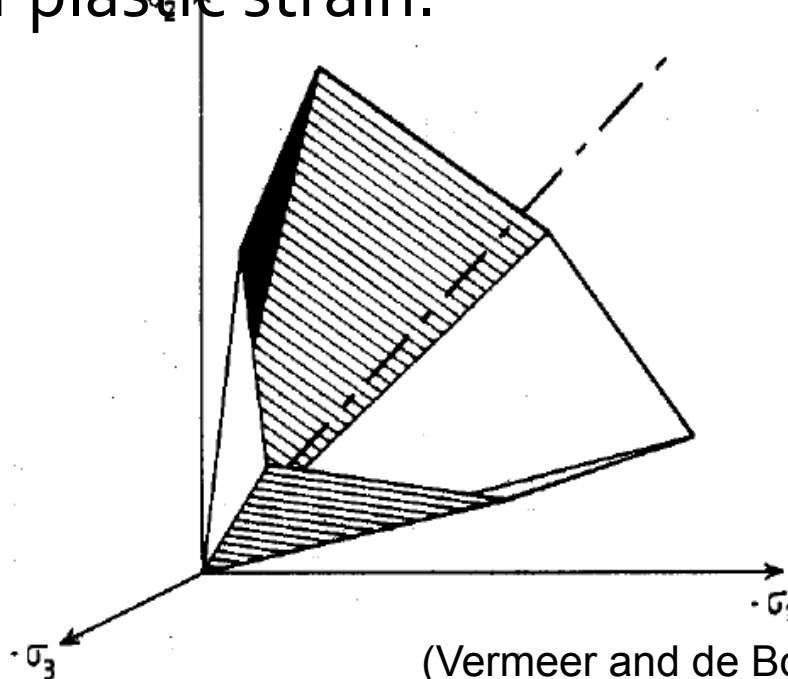
- As a solution, Kaus (2010) suggested that the key to achieving the Coulomb angle is to resolve inhomogeneity (weak “seed”) with sufficiently many elements.
- Often the size of seed and the mesh resolution needs to be independent of each other.
- Still need to understand why models show discrepancy from simple theoretical predictions.

Strain Localization at Coulomb Angle

- Strain localization theory: Mohr-Coulomb yield function

$$f(\sigma_1, \sigma_3, \alpha) = (\sigma_1 - \sigma_3) - \sin \phi(\alpha) \left(\sigma_1 + \sigma_3 + \frac{C(\alpha)}{\tan \phi(\alpha)} \right) = 0.$$

- α : Internal variable, a metric (typically, second invariant) of plastic strain.



Strain Localization at Coulomb Angle

- Strain localization theory: Hardening modulus

$$H = \frac{\partial f}{\partial \alpha} = \frac{\partial f}{\partial \phi} \frac{\partial \phi}{\partial \alpha} + \frac{\partial f}{\partial C} \frac{\partial C}{\partial \alpha}$$

- $H > 0$: strain hardening, $H < 0$: strain weakening/softening.

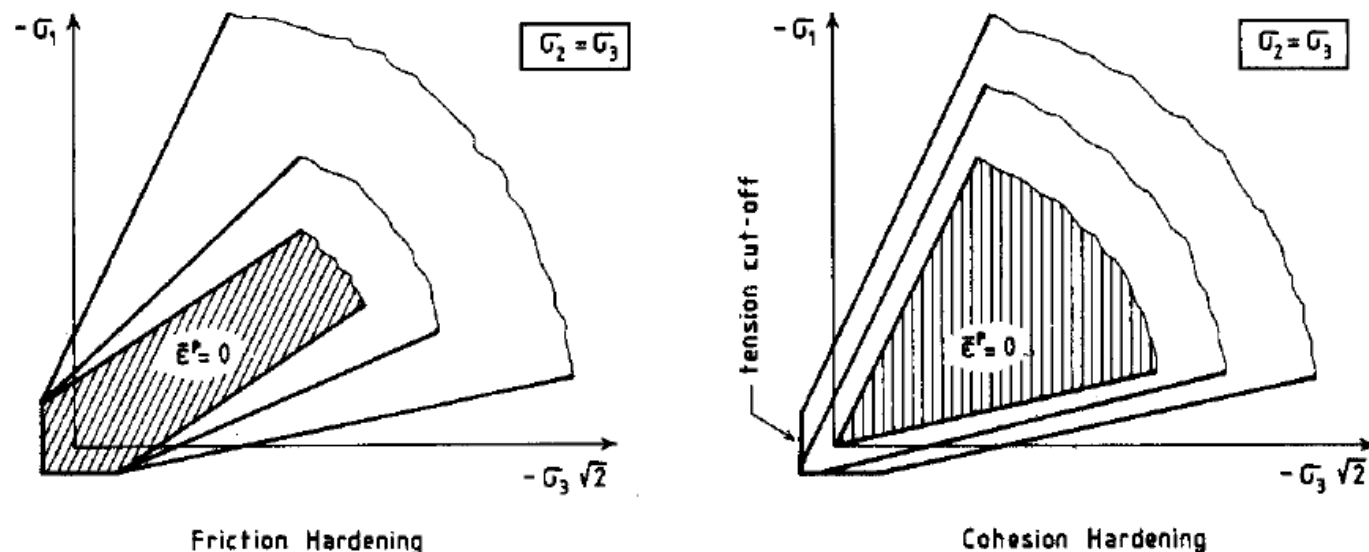


Fig. 6.4 Largely different modes of expansion for the elastic range.
(Vermeer and de Borst, Heron, 1984)

Strain Localization at Coulomb Angle

- Strain localization theory: Conditions on stress/strain
 - normal traction must be continuous across the shear band boundaries.
 - Don't allow band-parallel strain.

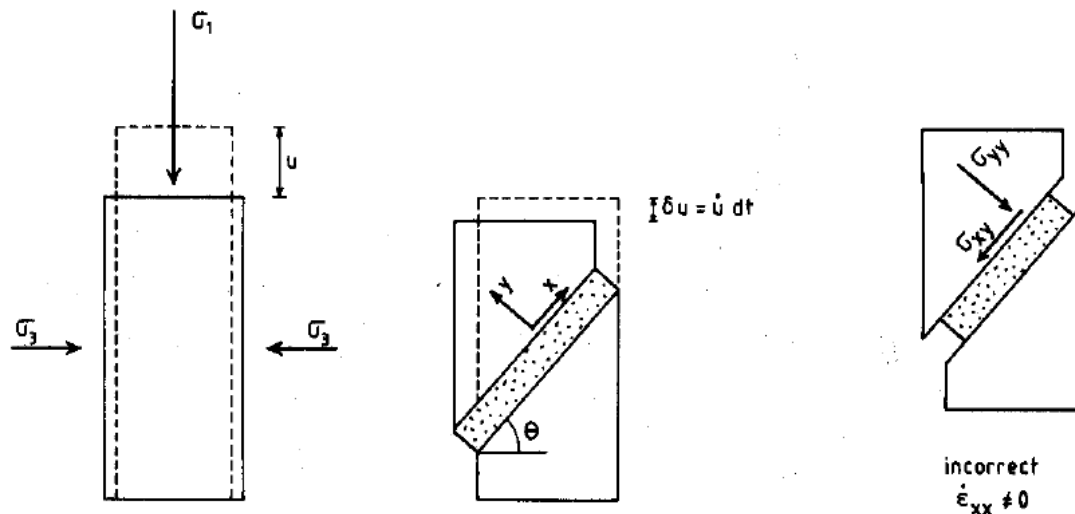
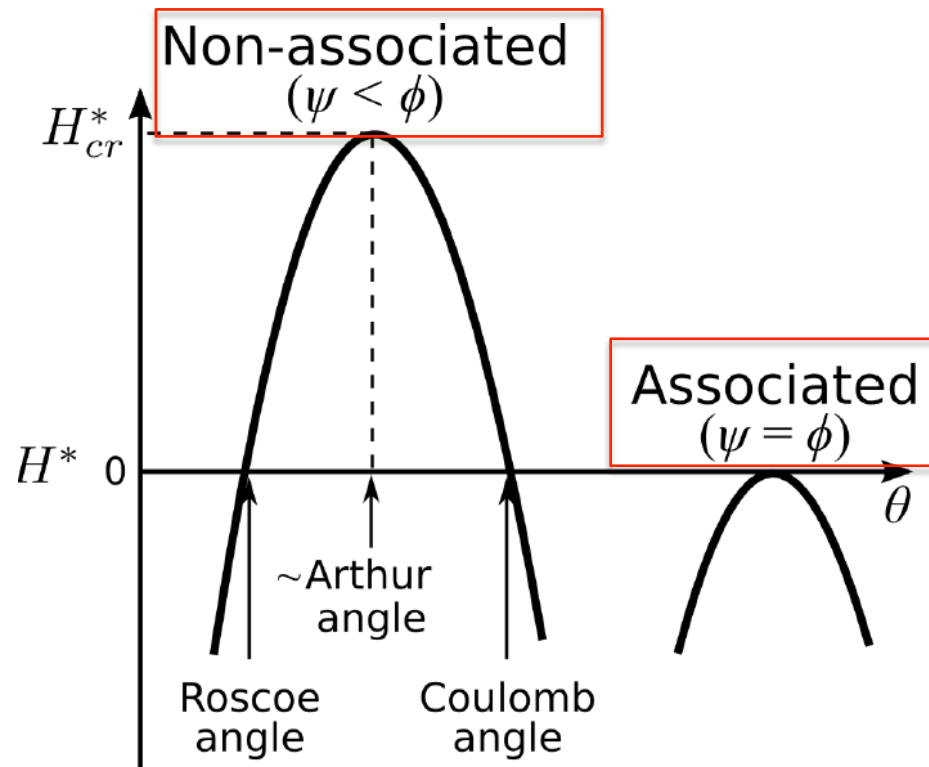


Fig. 8.3 a. Uniform deformation up to current state
b. Further deformation localized in a shear band
c. Incorrect mechanism.

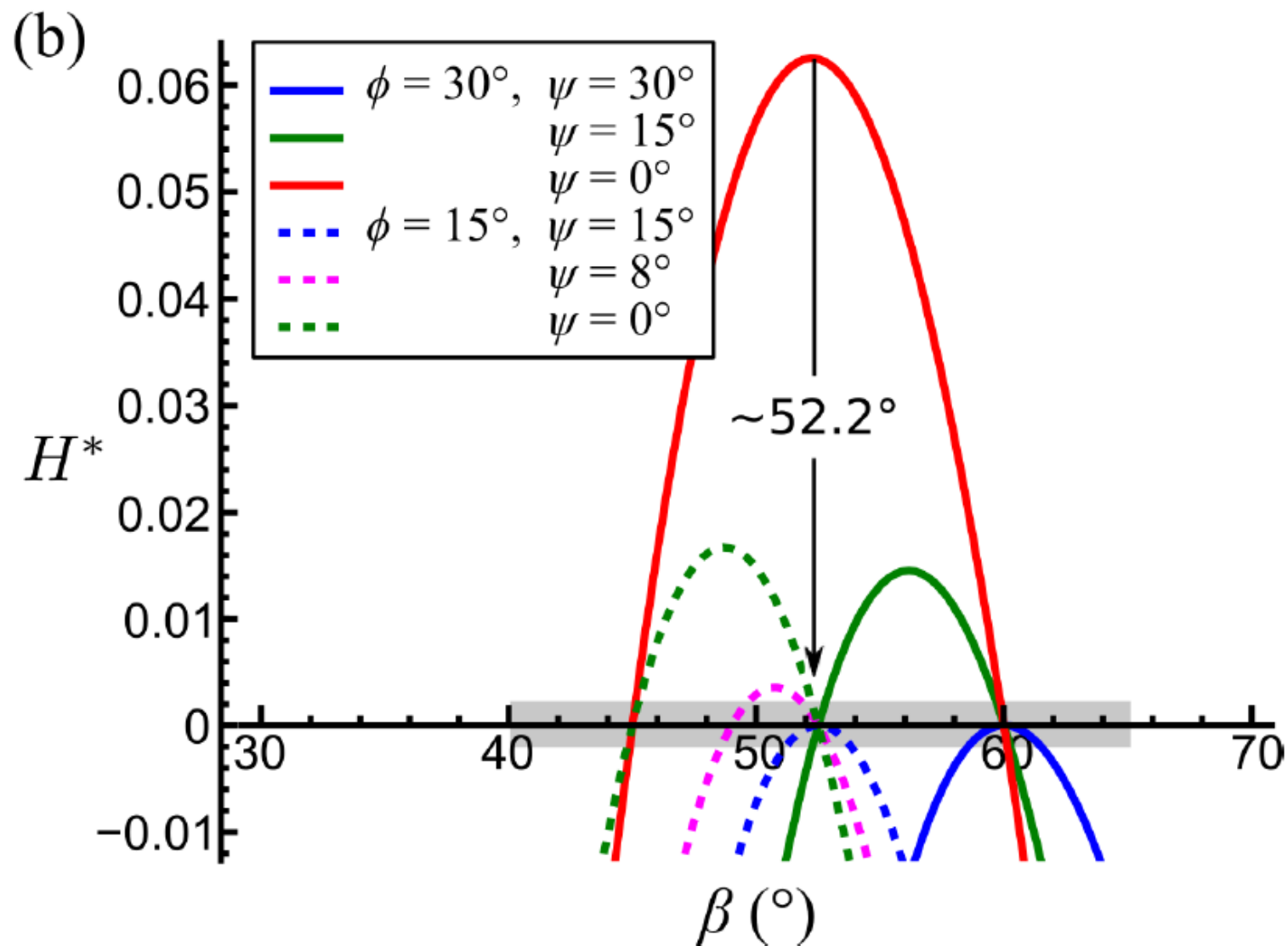
Strain Localization at Coulomb Angle

- From these conditions, we get a relationship between H^* and θ :

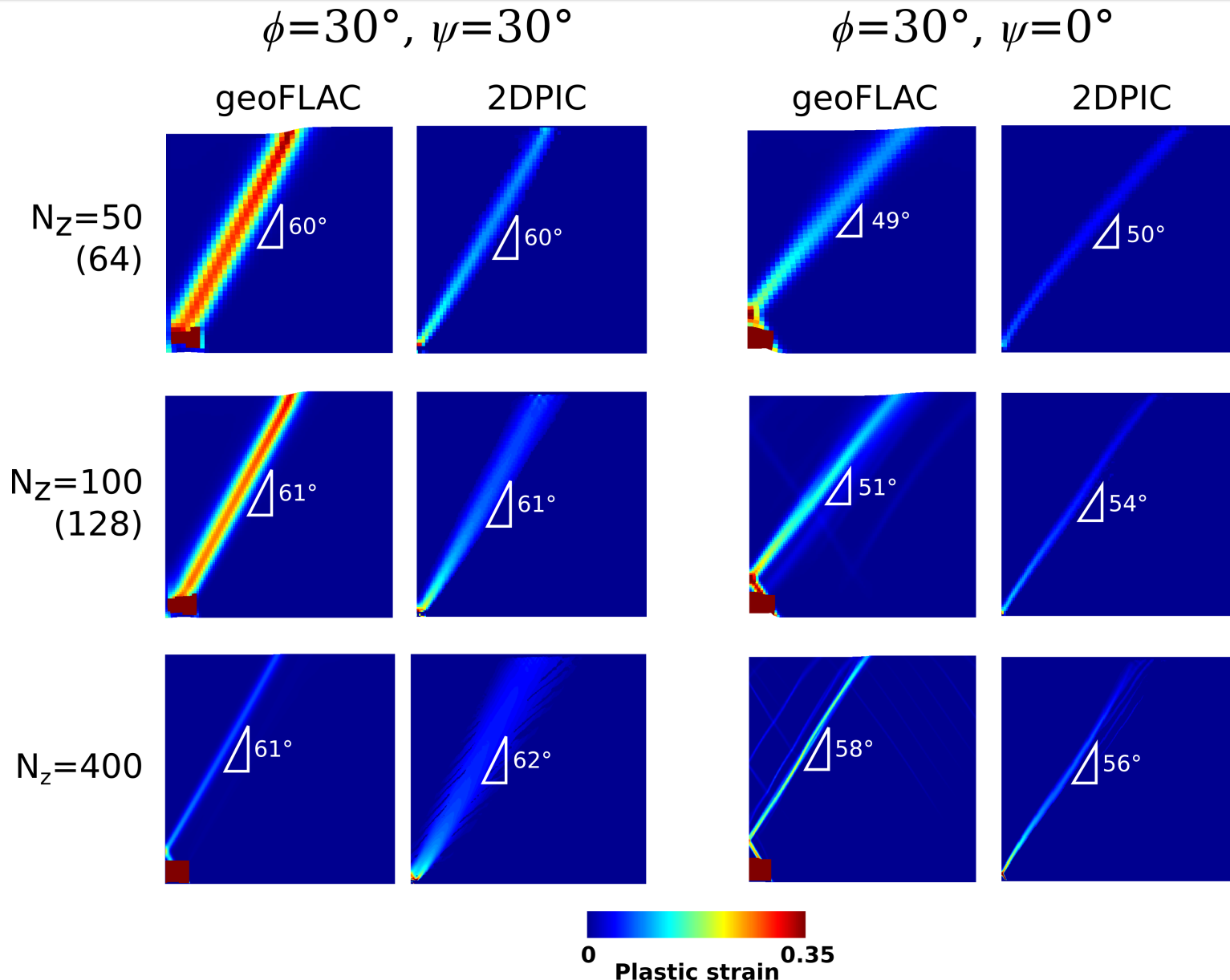
$$H^* = \frac{H}{2G} = \frac{(\sin \psi - \sin \phi)^2 - (2 \cos 2\theta - \sin \psi - \sin \phi)^2}{8(1 - \nu)\sqrt{(1 + \sin^2 \psi)(1 + \sin^2 \phi)}}$$



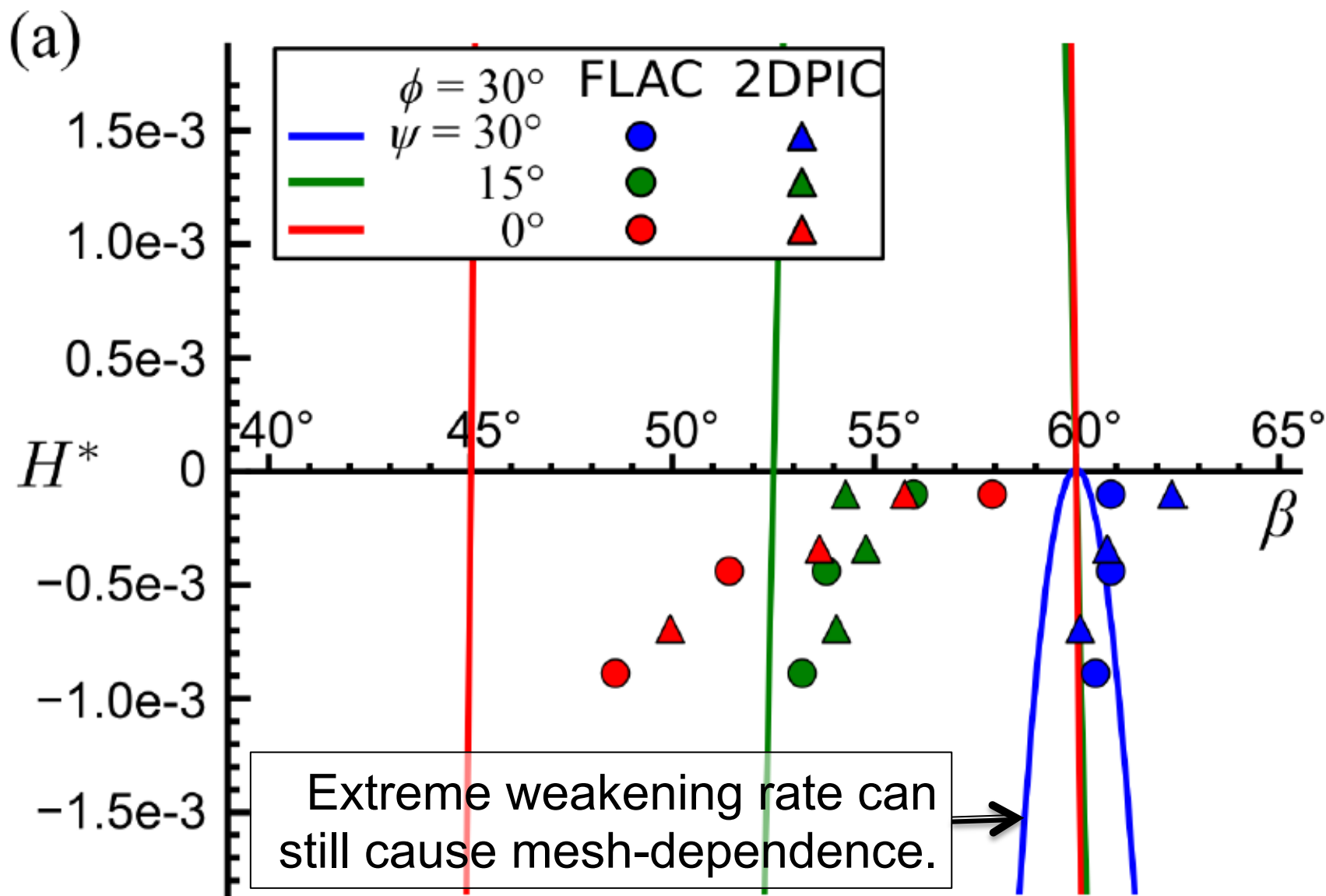
Strain Localization at Coulomb Angle



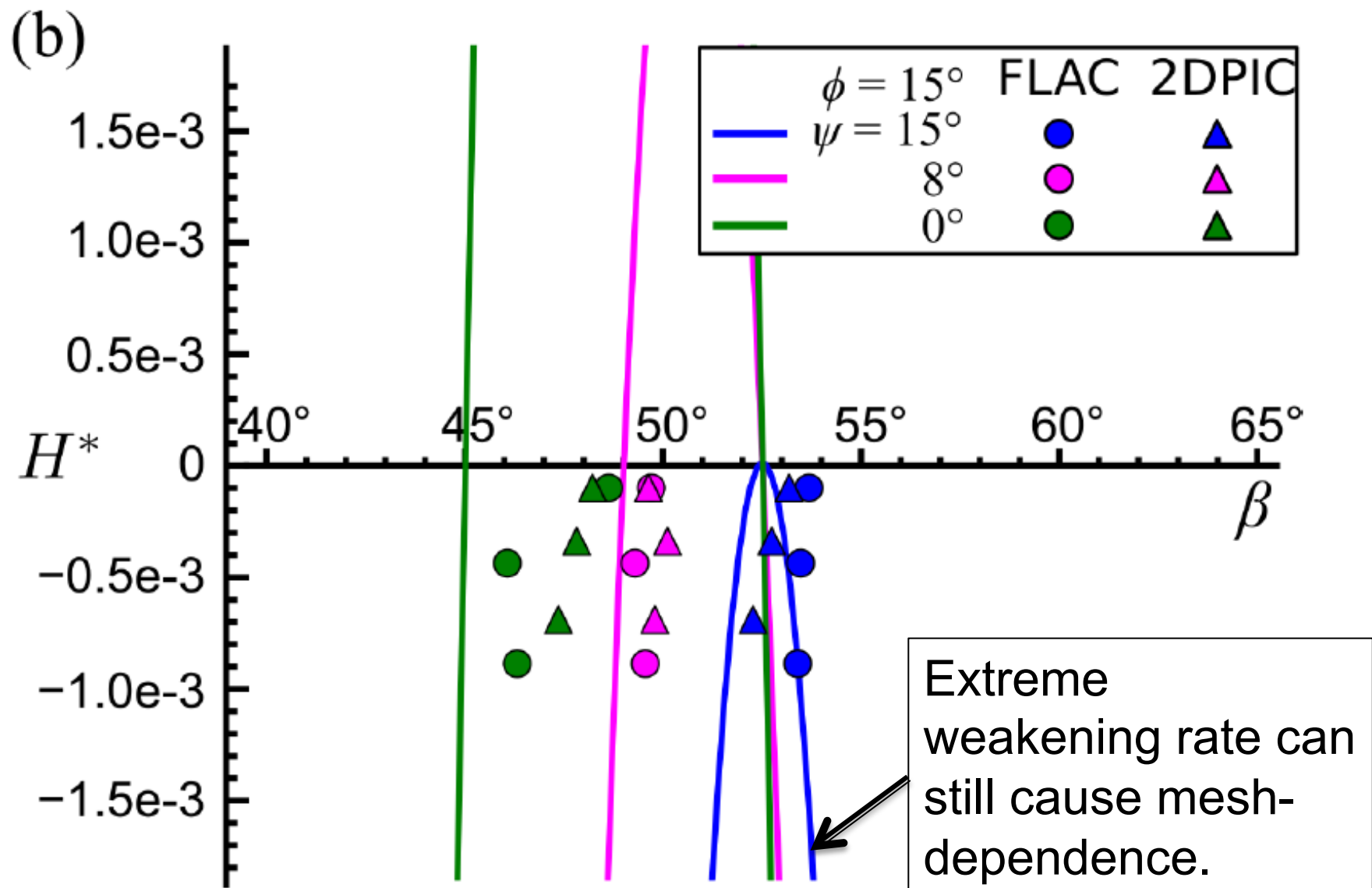
Strain Localization at Coulomb Angle



Strain Localization at Coulomb Angle



Strain Localization at Coulomb Angle



Strain Localization at Coulomb Angle

- In summary, the combination of **associated flow rule** and **modest H** is a sufficient condition for Coulomb angle-oriented shear bands.
 - Seems insensitive to mesh resolution and inhomogeneity resolution.
- Caveat: A constant dilation angle means non-stopping expansion of shear band
 - Need to decrease gradually.
 - Might correspond to the process of asperity abrasion.

Strain Localization at Coulomb Angle

- Dilation angle reduction also necessary for modeling long-term evolution.

