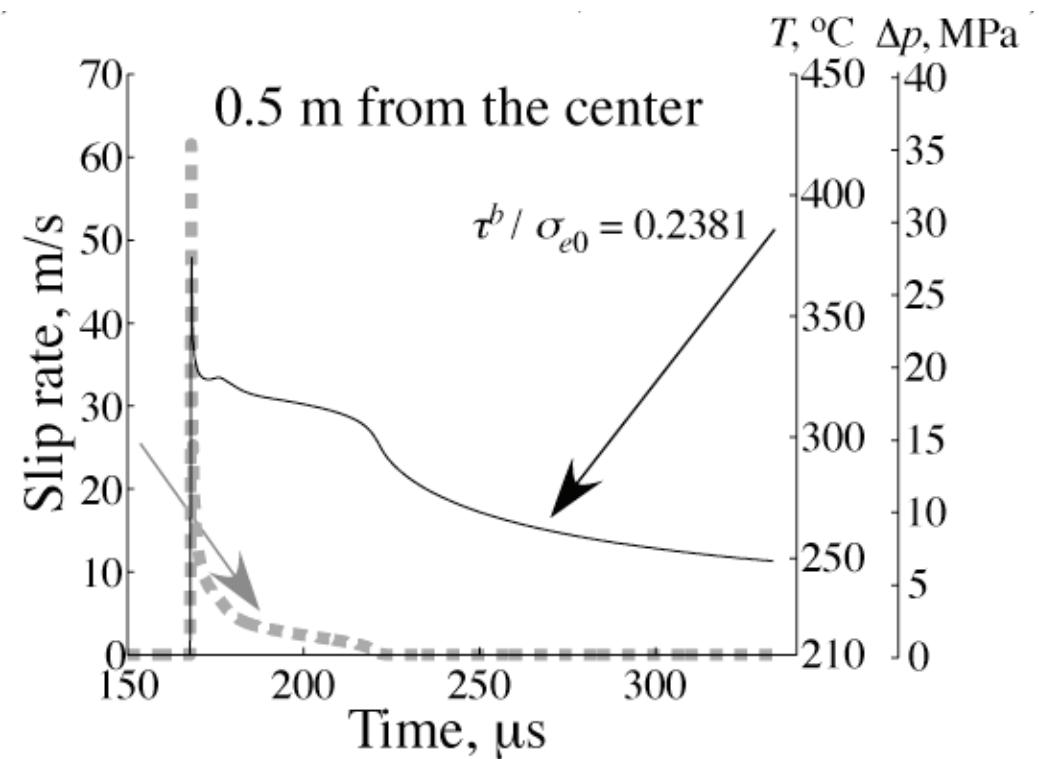
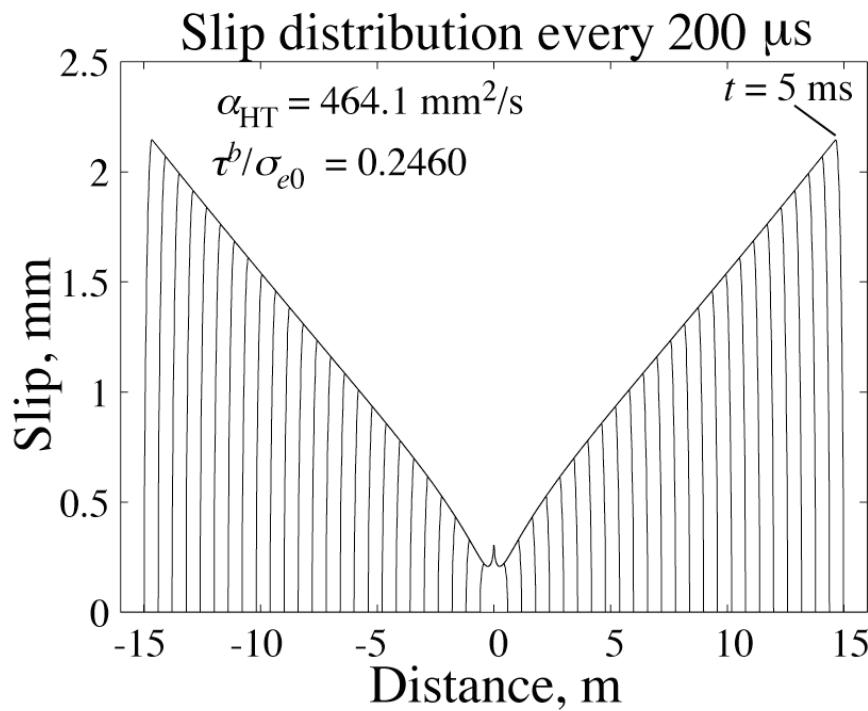


# Incorporating Dynamic Weakening Mechanisms into Spontaneous Rupture Models

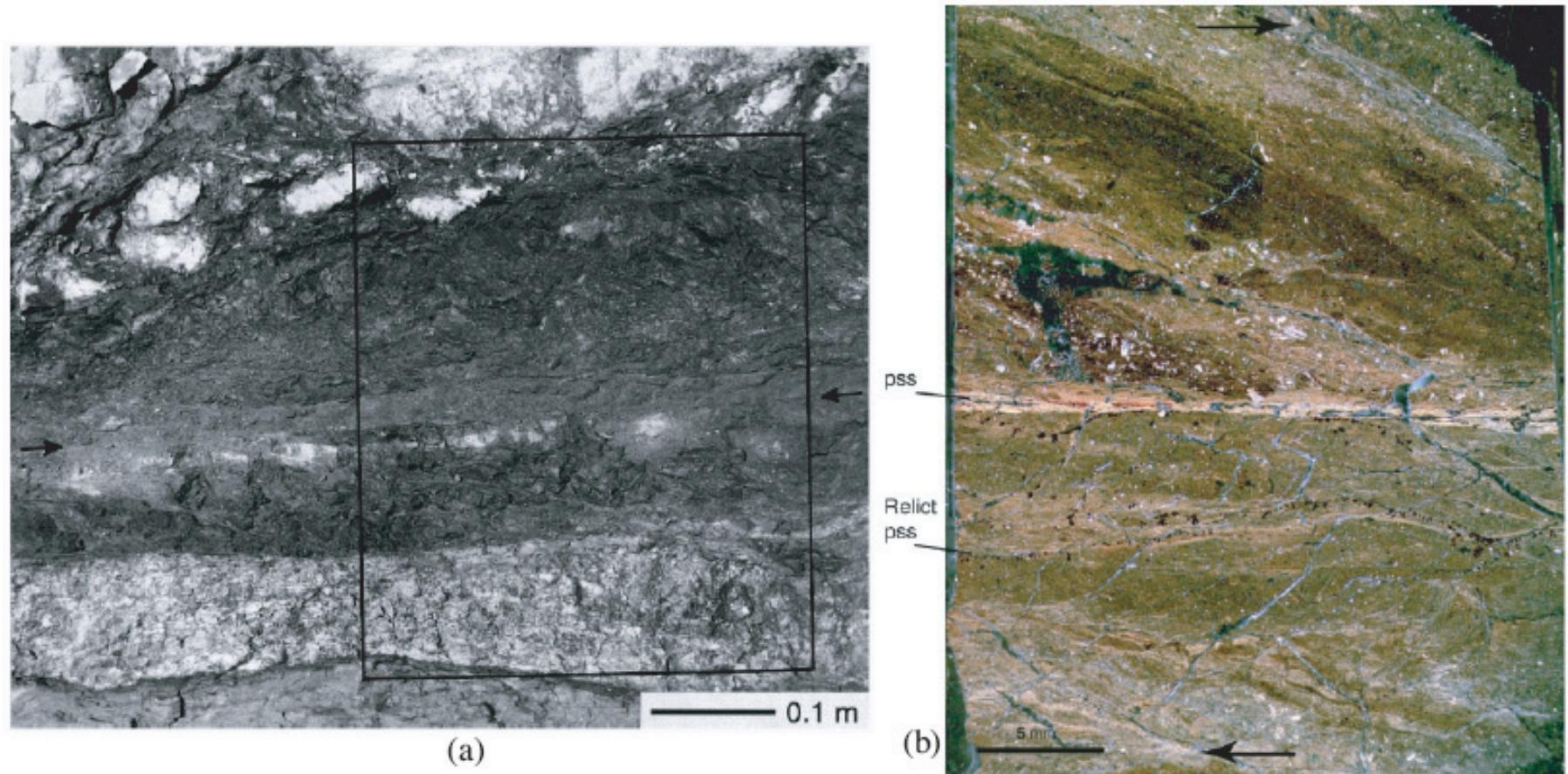
Eric Dunham, Hiro Noda, Jim Rice

Harvard University



# Context for Dynamic Weakening

Extreme localization of seismic slip on mature fault—Punchbowl fault  
[F. Chester & J. Chester, 1998; J. Chester et al., 2003, 2005; J. Chester and D. Goldsby, 2003]



**Figure 1:** Principal slip surface (pss) along the Punchbowl fault. (a) From Chester and Chester [1998]: Ultracataclasite zone with pss marked by black arrows; note 100 mm scale bar. (b) From Chester et al. [2005a] (also, Chester et al. [2003] and Chester and Goldsby [2003]): Thin section; note 5 mm scale bar and ~1 mm localization zone (bright strip when viewed in crossed polarizers due to preferred orientation), with microshear localization of most intense straining to ~100-300  $\mu\text{m}$  thickness.

[Rice, 2006]

# Context for Dynamic Weakening

Weakening of fault shear strength  $\tau$  due to changes in:

$f$  = coefficient of friction

$\sigma$  = normal stress

$p$  = pore pressure

$$\tau = f(\sigma - p)$$

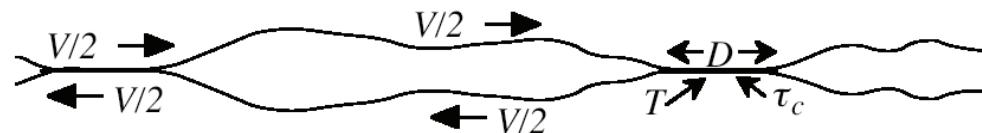
High temperatures expected from sliding at standard friction coefficients ( $f \sim 0.6$ ) and effective normal stresses ( $\sigma - p \sim 100$  MPa),

but evidence for melt (pseudotachylites) is not universally present.

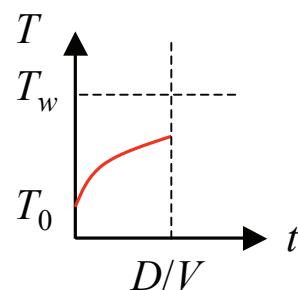
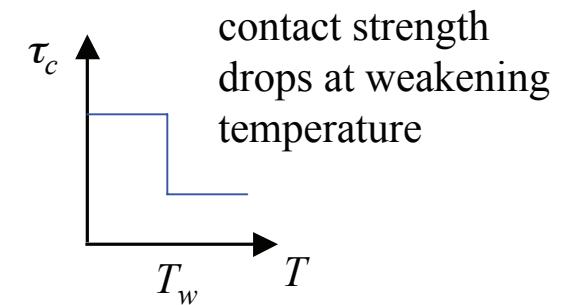
Dynamic weakening (decrease in  $f$  and increase in  $p$ ) reduces  $\tau$ , but only during rapid sliding ( $\sim \text{m/s}$ ).

Recent laboratory friction experiments and measurements of thermal and hydraulic properties of fault-zone materials constrain models of dynamic weakening (flash heating and thermal pressurization).

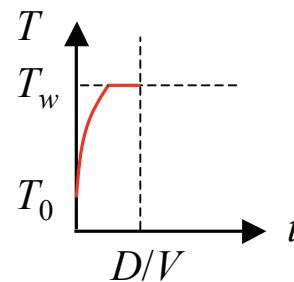
# Flash Heating of Microscopic Asperity Contacts



energy balance  $\underbrace{\tau_c V t}_{\text{work by shear heating}} \sim \underbrace{\rho c(T - T_0)}_{\text{thermal energy storage}} \sqrt{\underbrace{\alpha_{th} t}_{\text{thermal diffusion length}}}$



slow speeds:  $V < V_w$



high speeds:  $V > V_w$

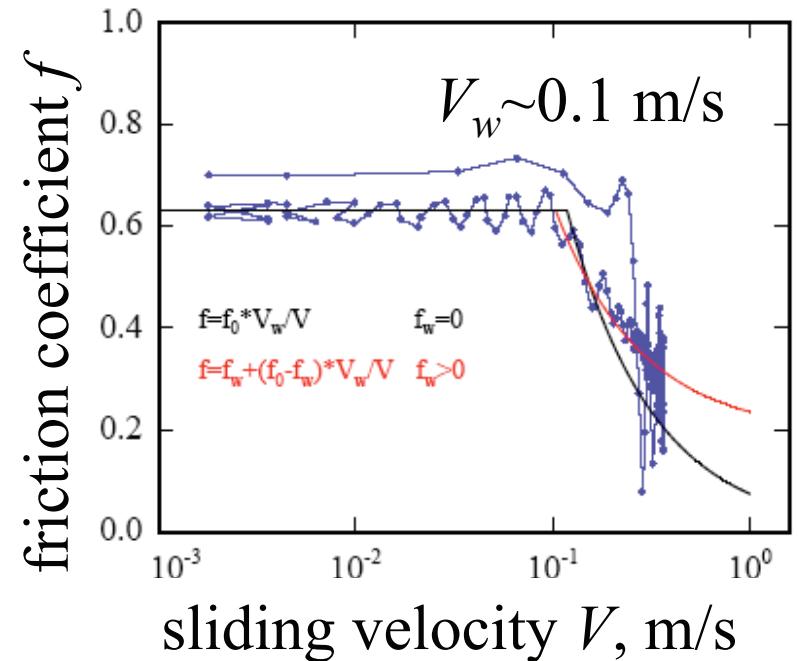
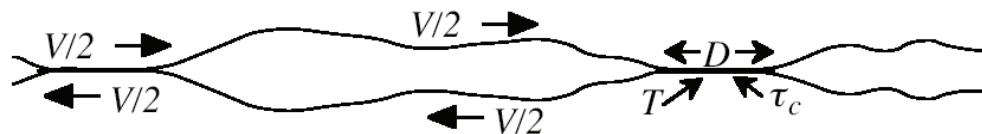
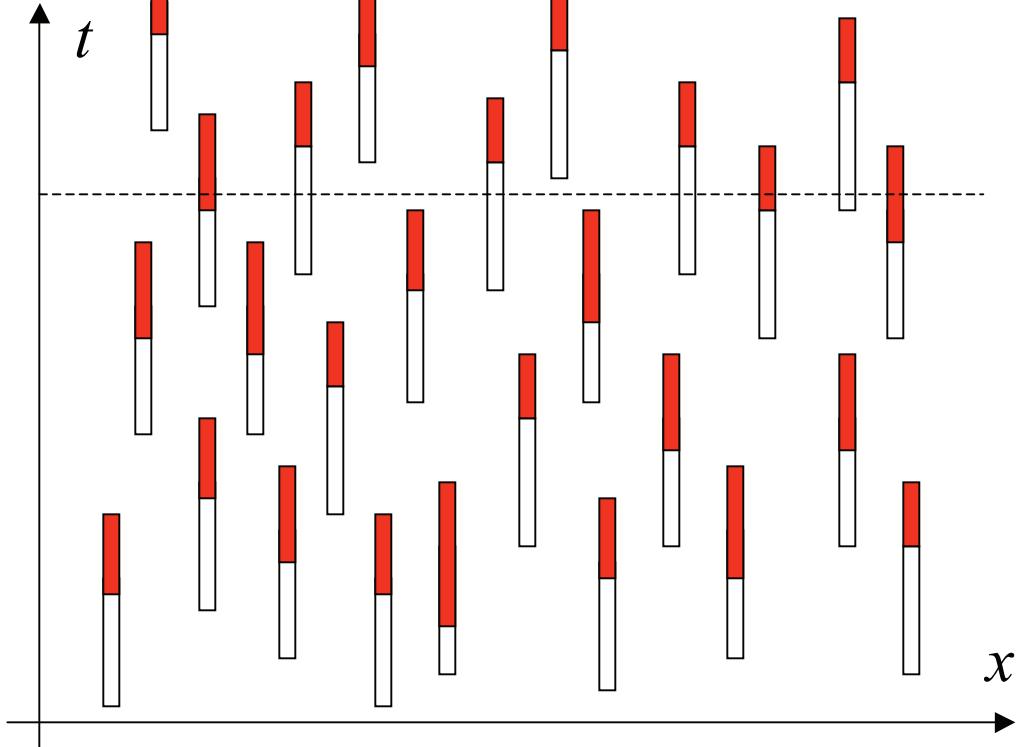
$V_w$  (weakening velocity) is  $V$  at which asperity reaches  $T = T_w$  (weakening temperature at which  $\tau_c$  abruptly drops) exactly at  $t = D/V$  (asperity lifetime)

$\tau_c$  = contact strength  
 $V$  = slip velocity  
 $\rho c$  = heat capacity  
 $T$  = temperature  
 $\alpha_{th}$  = thermal diffusivity  
 $D$  = asperity length

# Ensemble of Contacts and Model for $f(V)$

macroscopic strength determined  
by current asperity population





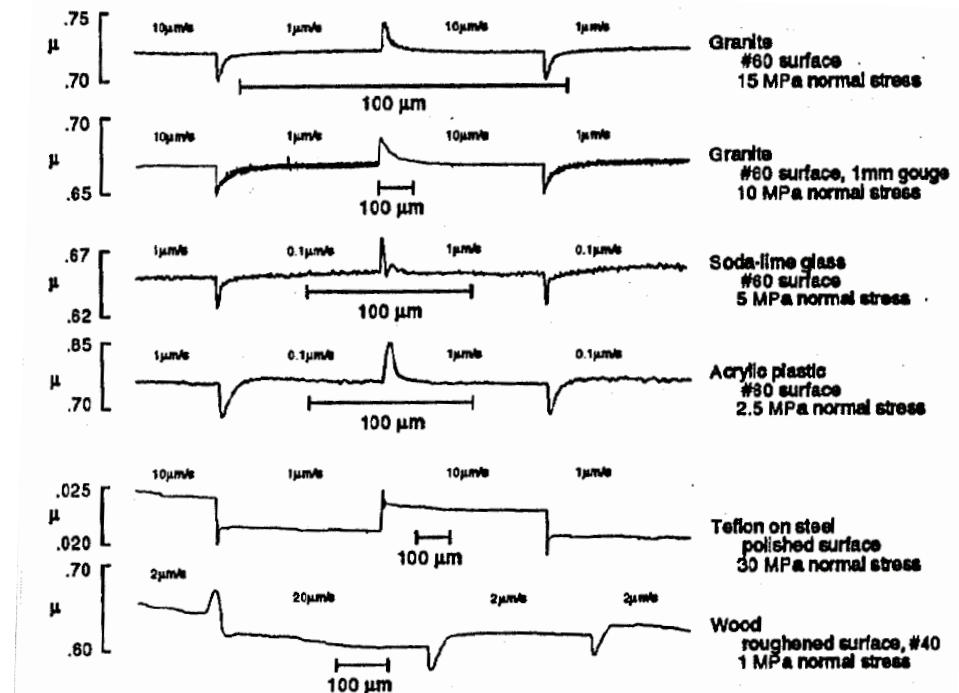
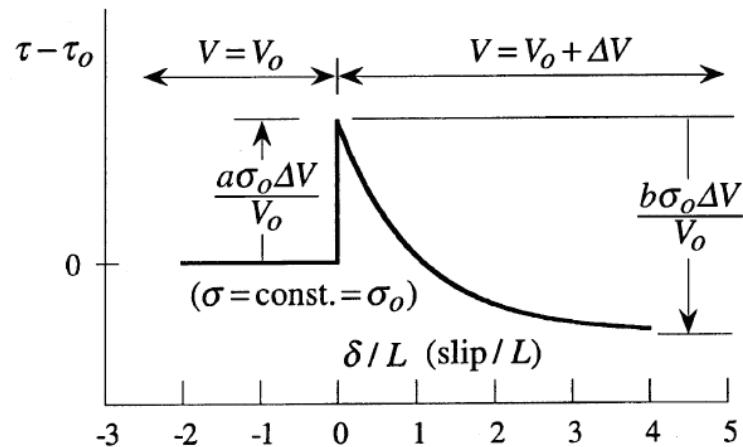
experimental results of Tullis and Goldsby [2003] and fits to theoretical model of flash heating by Rice [1999] and its extension by Beeler [unpublished]

# Rate-and-State Framework for $f$

Framework for coefficient of friction  $f$  includes:

1. flash heating model for  $f_{ss}(V)$
2. direct effect (parameter  $a$ )—evidence for thermally activated process (dislocations) at asperity contacts
3. evolution to new steady state over slip  $L$

$$\frac{df}{dt} = \frac{a}{V} \frac{dV}{dt} - \frac{V}{L} [f - f_{ss}(V)]$$



[Dieterich and Kilgore, 1994]

# Thermal Pressurization: Model for $p$

*Conservation of energy:*

$$\frac{\partial T}{\partial t} = \alpha_{th} \frac{\partial^2 T}{\partial y^2} + \frac{\tau \dot{\gamma}}{\rho c}, \quad \int \dot{\gamma}(y) dy = V$$

$T$  = temperature  
 $\alpha_{th}$  = thermal diffusivity  
 $\dot{\gamma}$  = strain rate (over finite shear zone)  
 $V$  = slip velocity

*Conservation of fluid mass:*

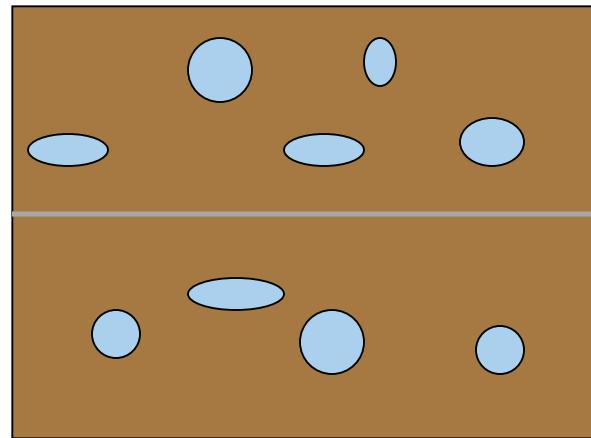
$$\frac{\partial p}{\partial t} = \Lambda \frac{\partial T}{\partial t} + \alpha_{hy} \frac{\partial^2 p}{\partial y^2}$$

$p$  = pore pressure  
 $\alpha_{hy}$  = hydraulic diffusivity  
 $\Lambda$  = pressure-temperature coupling

treat thermodynamic properties as constants (i.e., neglect pressure dependence of permeability, etc.)

[Rice, 2006; building on Sibson, 1973 and many others; thermal and hydraulic properties from variety of laboratory studies of fault-zone materials (from exhumed faults and drilling projects)]

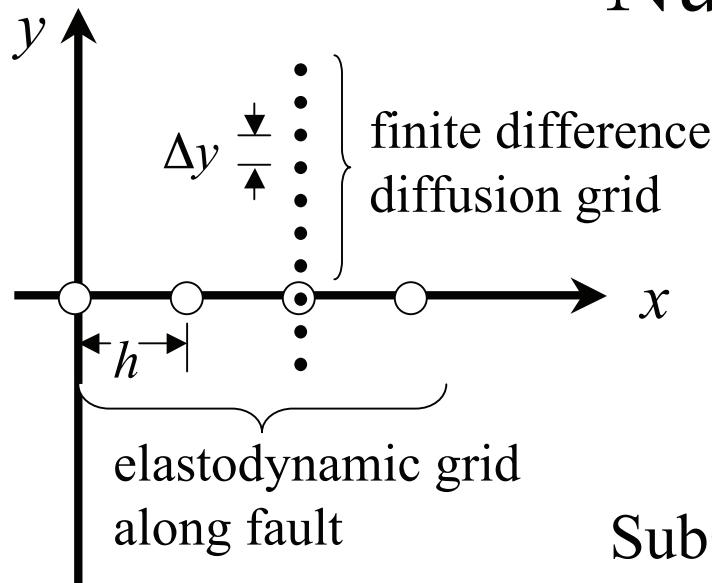
heat while holding fluid mass  $m$  fixed (undrained response)



- thermal expansion coefficient of water ( $\sim 10^{-3} \text{ K}^{-1}$ )  $\gg$  pores
- water and pores equally compressible ( $\sim \text{GPa}^{-1}$ )

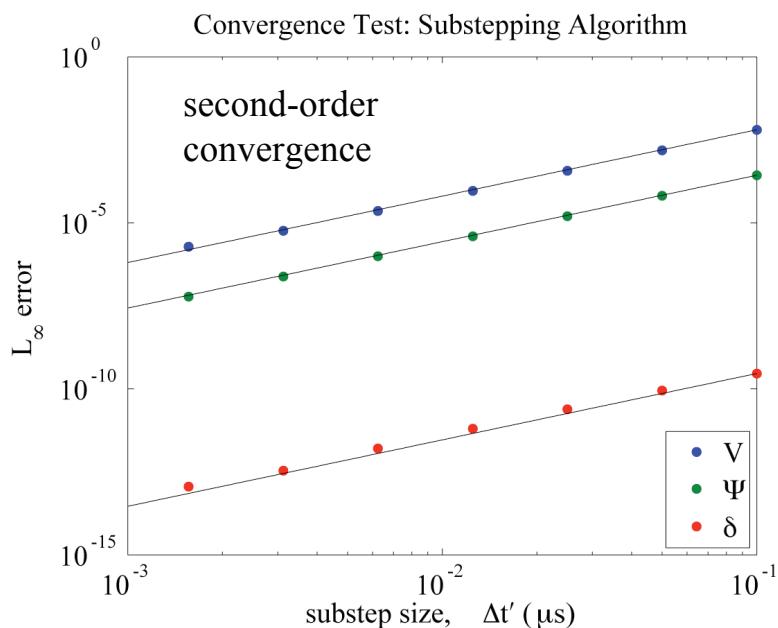
$$\Lambda = \left( \frac{\partial p}{\partial T} \right)_m \sim \text{MPa/K}$$

# Numerical Methodology



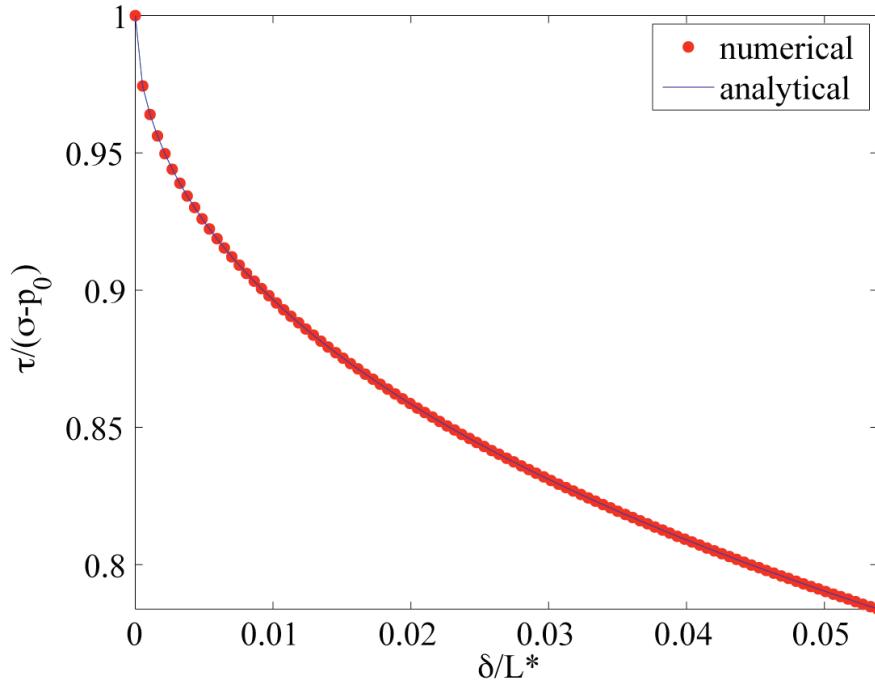
elastodynamic response currently from boundary integral equation method, although similar implementation in finite difference / finite element codes

Substepping: elastodynamic time step  $\sim h/c_s$  larger than diffusive time step  $\sim \Delta y^2/\alpha_{hy}$

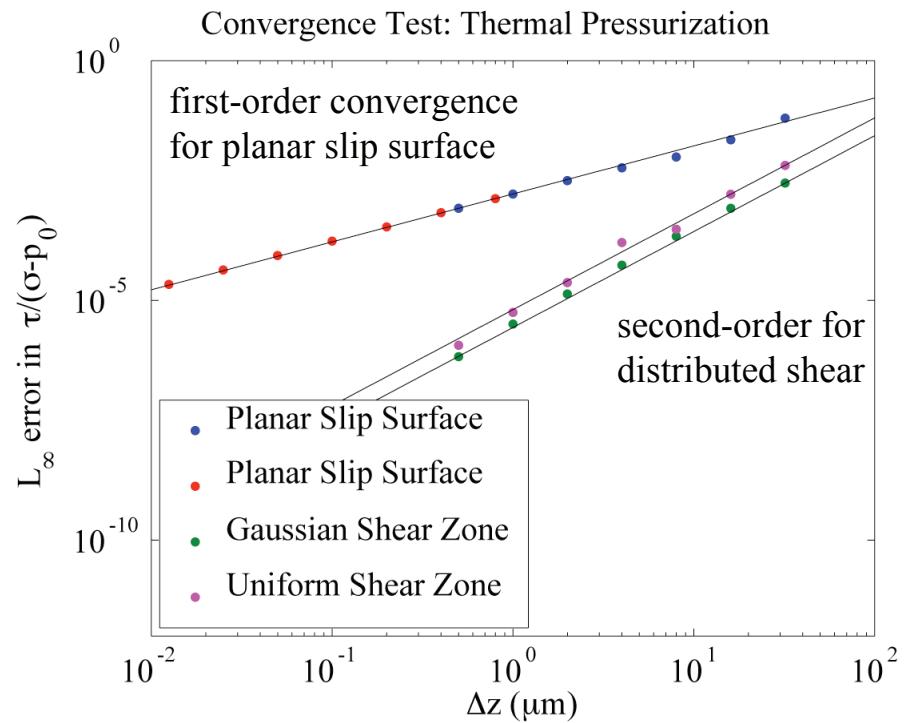


integrate diffusion equations and friction law with adaptive time steps via embedded Runge–Kutta methods

# Finite Differences for Thermal Pressurization



analytical solution for  
weakening over slip  $\delta$  due  
to thermal pressurization of  
planar fault at constant  $f$   
and  $V$  [Rice, 2006]

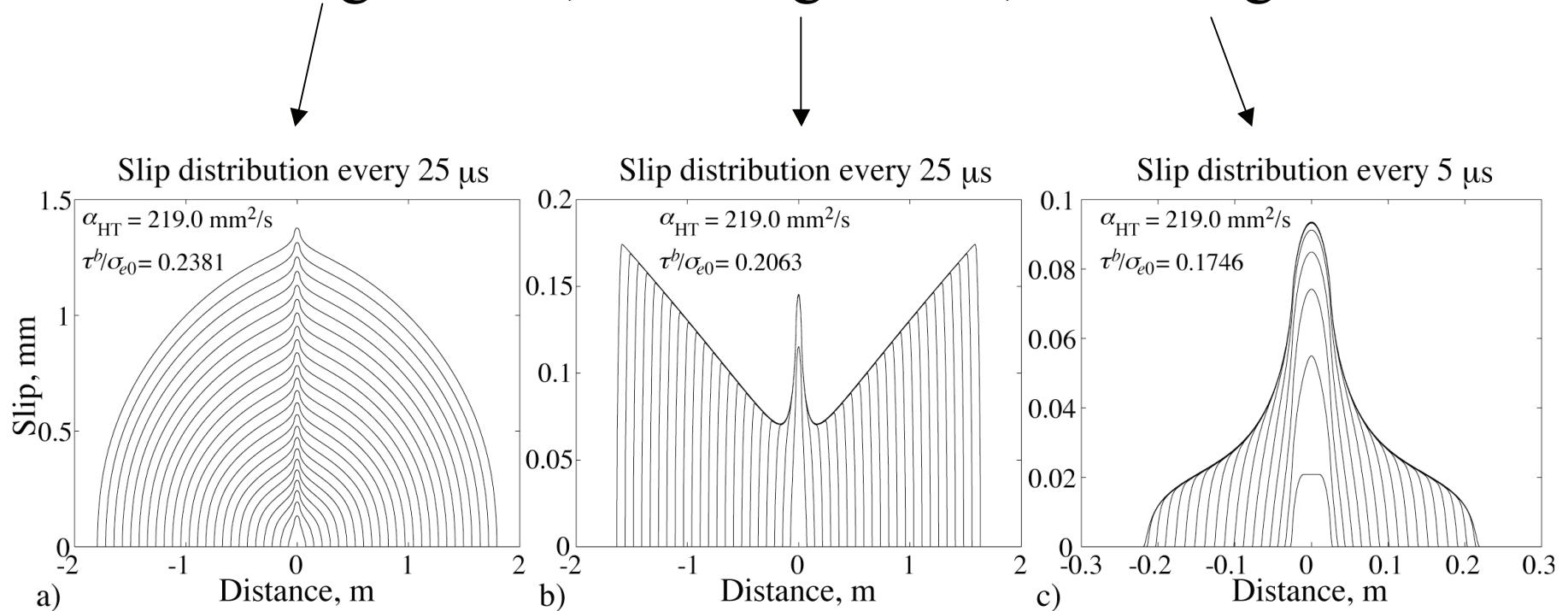


$$\tau \sim f(\sigma - p_0) \sqrt{\frac{L^*}{\pi \delta}} \text{ for large } \delta$$

$$L^* = \frac{4}{f^2} \left( \frac{\rho c}{\Lambda} \right)^2 \frac{\left( \sqrt{\alpha_{hy} + \alpha_{th}} \right)^2}{V} \approx 4 - 30 \text{ mm}$$

continual weakening allows fracture energy to increase  
with slip, as indicated by seismic observations

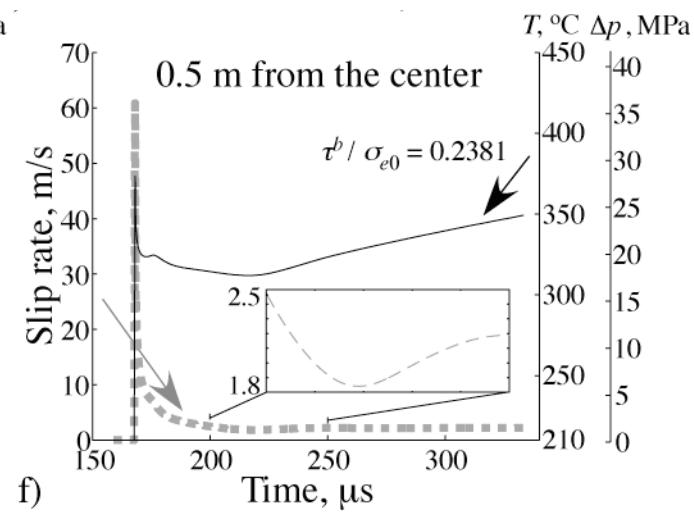
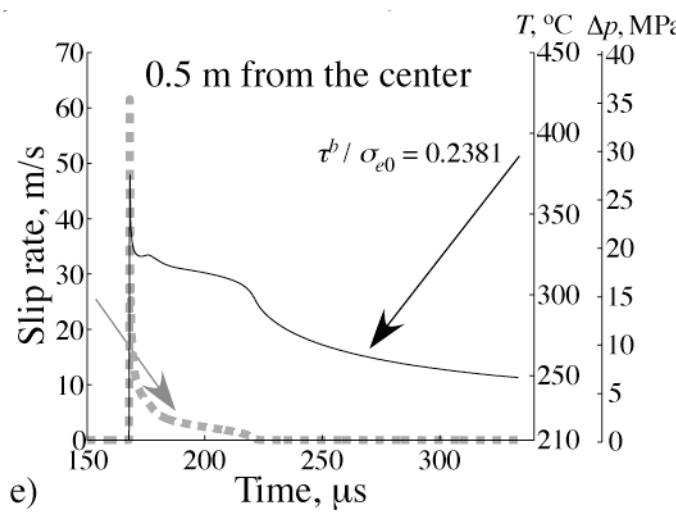
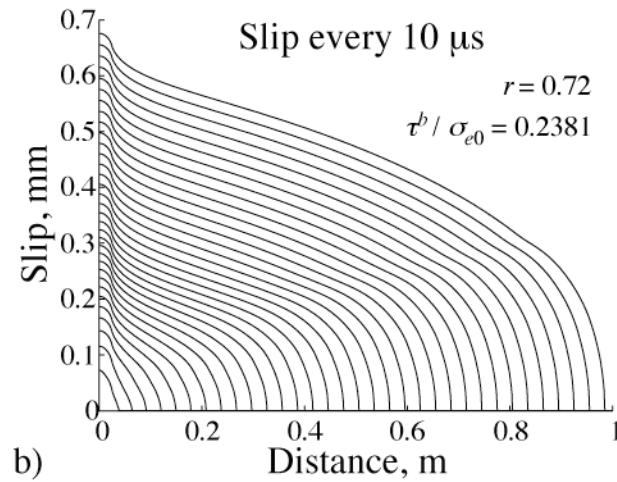
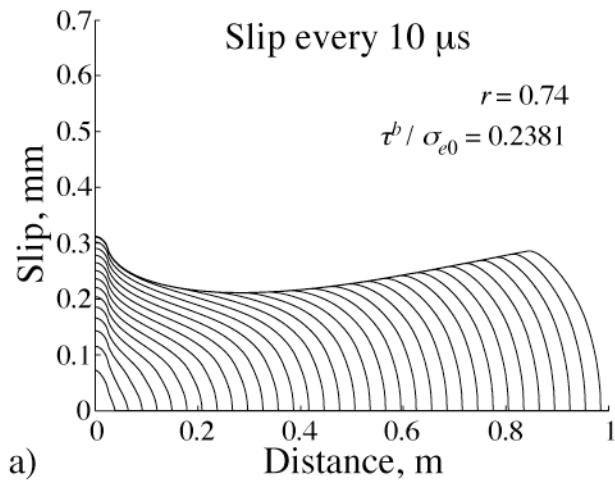
# Rich Phenomenology: Growing Cracks, Growing Pulses, Arresting Pulses



nucleation procedure: overstress small asperity in center

[Noda, Dunham, and Rice, in preparation, 2007]

# Properties of Pulses and Cracks



[Noda, Dunham, and Rice, in preparation, 2007]

# Pulse Generation by Under-Stressing

Cracks only exist when solution exists to:

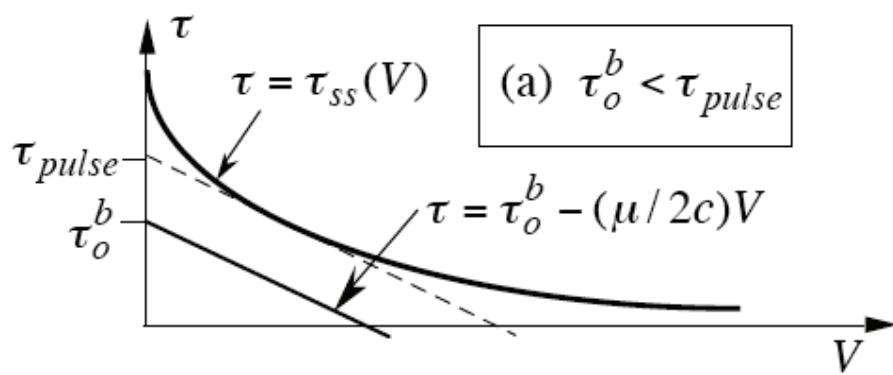
Long-wavelength elastodynamic response:

$$\tau \approx \tau_0 - \frac{\mu}{2c_s} V$$

$\tau_0$  = initial stress on fault  
 $\mu$  = shear modulus  
 $c_s$  = shear-wave speed  
 $V$  = slip velocity

Steady-state friction:

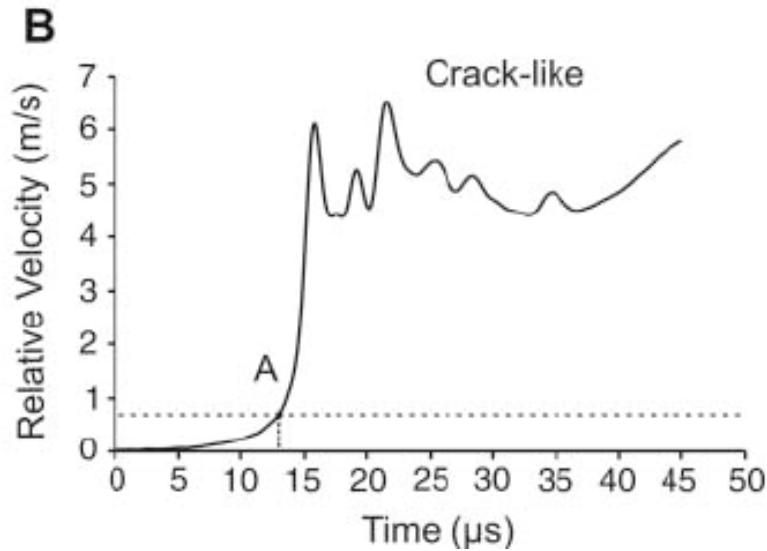
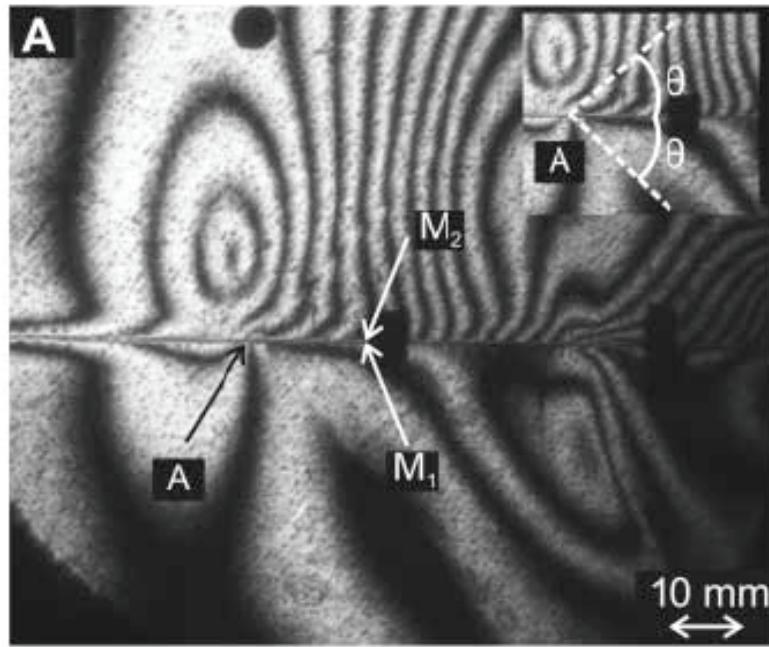
$$\tau = \tau_{ss}(V)$$



By decreasing  $\tau_0 < \tau_{pulse}$ , solution ( $V \neq 0$ ) ceases to exist and only slip pulses are found on fault.

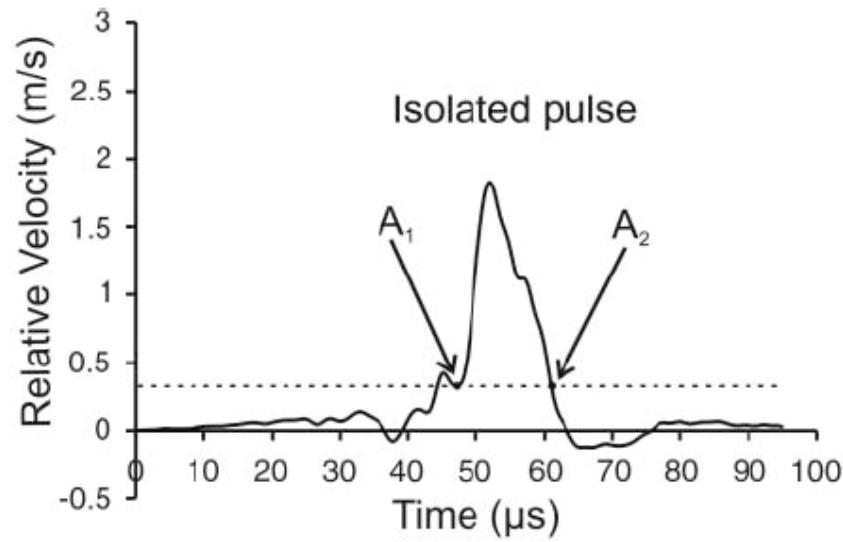
$\tau_0$ , a free parameter in single earthquake simulations, is constrainable only by modeling earthquake cycle.

[Zheng and Rice, 1998]



## Theory Consistent with Laboratory Experiments

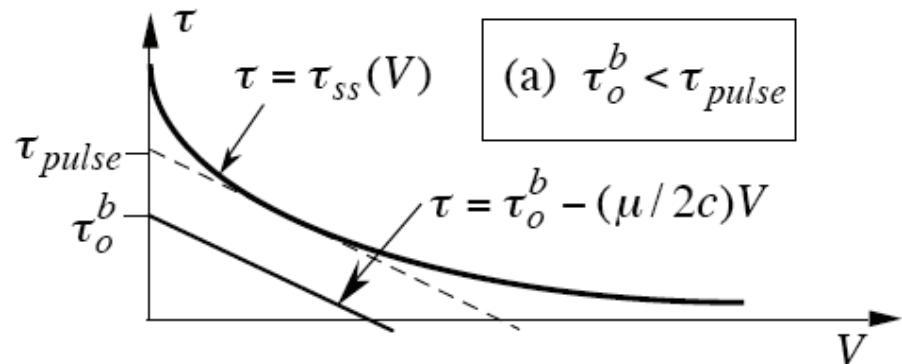
(transition from crack to pulse as shear/normal load decreases)



[Lykotrafitis et al., 2006]

# Generalizing the Theory

$$\begin{aligned}\tau &= \tau_{ss}(V) \rightarrow \\ \tau &= f_{ss}(V)(\sigma - p)\end{aligned}$$



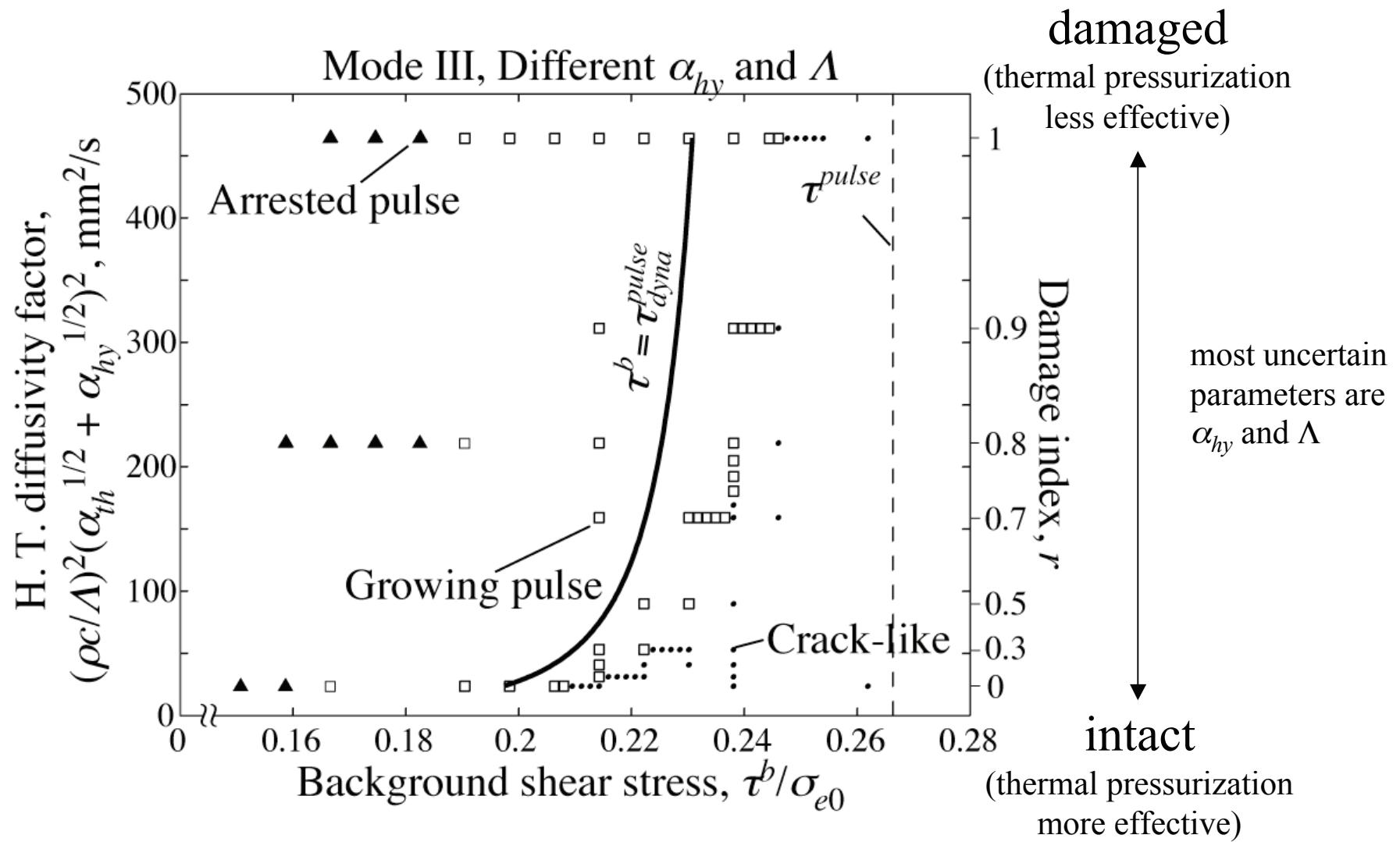
Increasing  $p$  lowers  $\tau_{ss}(V)$ , potentially bringing crack solution into existence, appropriate value of  $p$  exploits scale separation between thermal pressurization ( $L^* \sim 10$  mm) and flash heating ( $L \sim 10$  μm) by permitting use of  $f_{ss}(V)$

characteristic slip for thermal pressurization [Rice, 2006] is

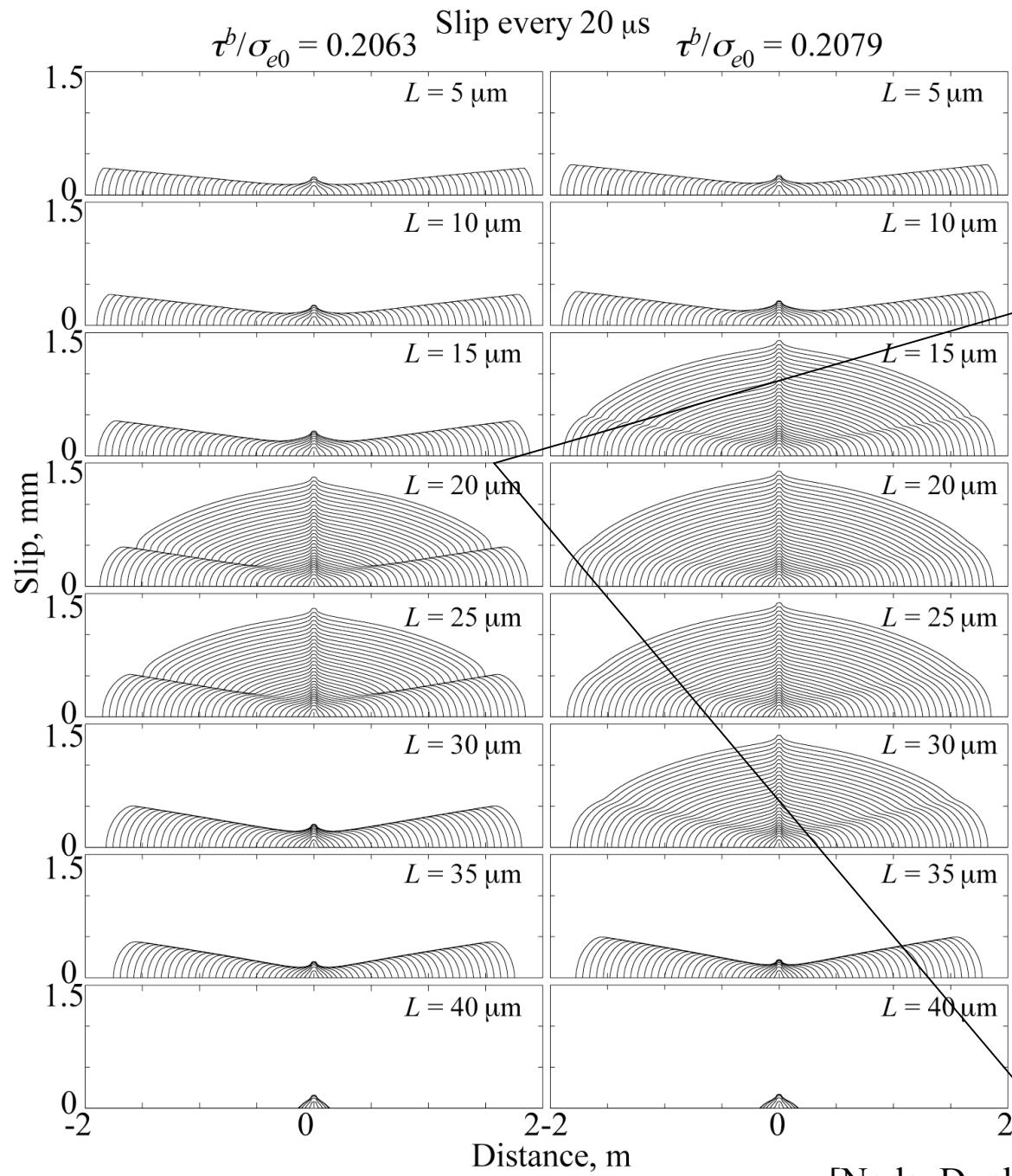
$$L^* = \frac{4}{f^2} \left( \frac{\rho c}{\Lambda} \right)^2 \frac{\left( \sqrt{\alpha_{hy} + \alpha_{th}} \right)^2}{V} \approx 4 - 30 \text{ mm}$$

(and finite width shear zone introduces another scale...)

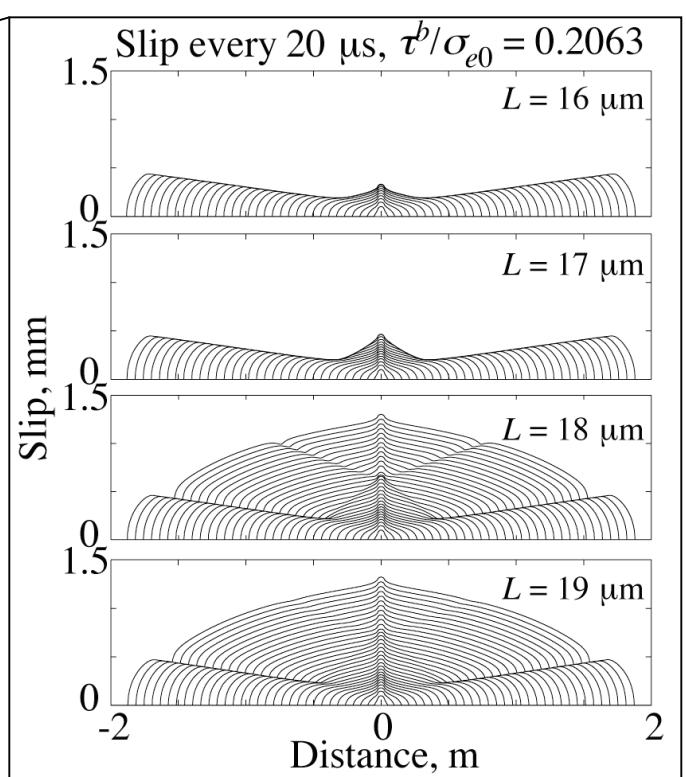
# Mapping Parameter Space: Effect of Hydrothermal (H.T.) Properties



[Noda, Dunham, and Rice, in preparation, 2007]

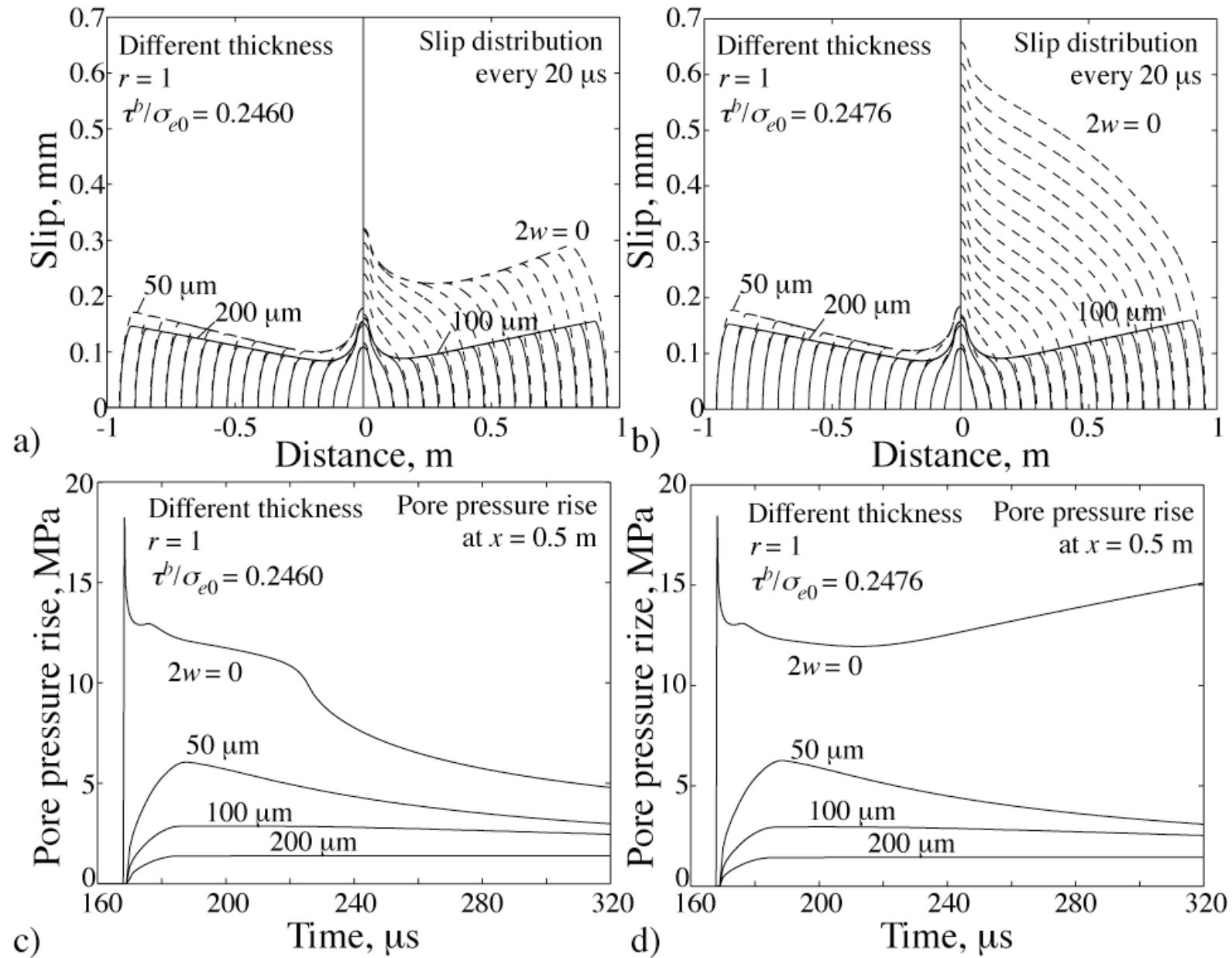


Varying State  
Evolution Distance:  
Small Scales Matter



Multiple Pulses at  
Crack-Pulse Boundary

# Shear Zone Thickness Matters

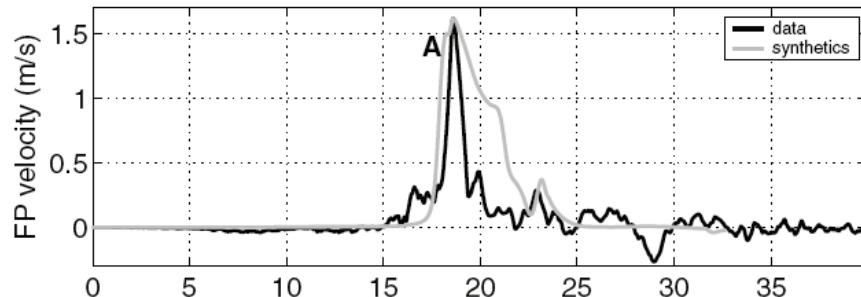


[Noda, Dunham, and Rice, in preparation, 2007]

# Consistency with Natural Events

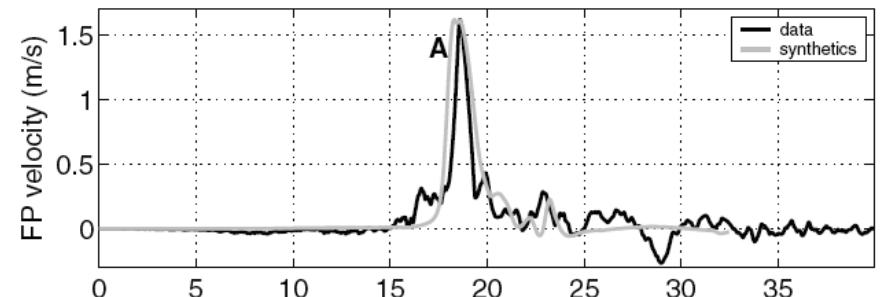
cracklike rupture from  
slip-weakening friction

a. Model I

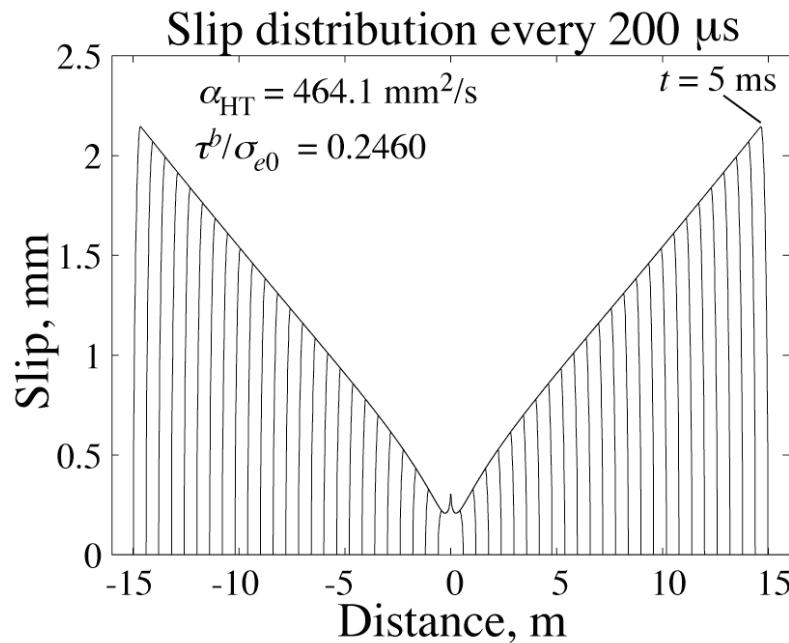


slip pulse from friction with  
velocity-weakening steady state

b. Model II



slip pulses observed in earthquakes: evidence from near-source ground motion records  
(example above 3 km from 2002 Denali Fault earthquake [Dunham and Archuleta, 2004])



proper scaling with event size:  
mm slip over 10 m fault  
m slip over 10 km fault

[Noda, Dunham, and Rice, in preparation, 2007]

## Conclusions:

Dynamic weakening mechanisms permit faults to operate at far lower average stress levels ( $\tau/\sigma \sim 0.25$ ) than expected from static friction measurements ( $\tau/\sigma \sim 0.6$ ); helps solve heat flow problem

Thermal pressurization gives proper scaling of fracture energy with event size, and velocity-weakening friction generates pulses

- reasonable static stress drops ( $\sim \text{MPa}$ )
- faults can host consecutive large events (stress not reduced to zero after event)
- huge slip velocities ( $> 10 \text{ m/s}$ ) last only  $\sim 10 \mu\text{s}$  (unobservable)

## Overlap with Quasi-static Community:

Initial stress levels (from earthquake cycle models)

Hydrology over interseismic time scales (3D diffusion problem)