

Exchanger - coupling multiple solvers for mantle convection

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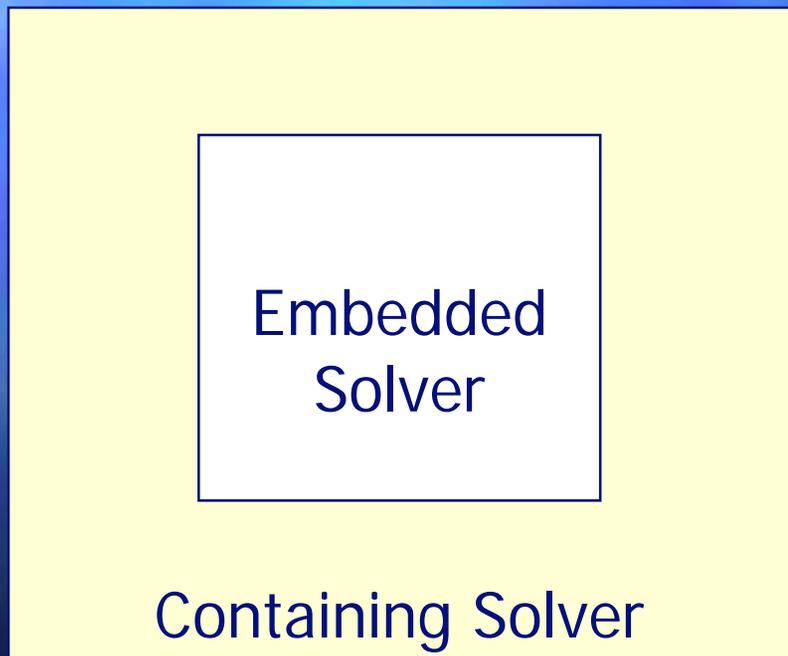
CACR, Caltech

2008 Davis, Workshop for Advancing
Numerical Modeling of Mantle
Convection & Lithospheric Dynamics

What is “solver coupling”?

- Two solvers, with disjointed memory addresses but overlapping physical domains, computing a joint problem

Coupling

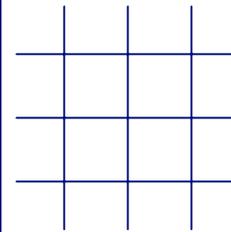


Resolution vs. computation time

- Optimal Stokes solver scales with $O(N) \sim O(1/h^3)$
- Number of time steps $\sim O(1/\Delta t)$
 $\sim O(1/h)$ for advection-dominant problems
- Total computation time = Number of time steps x Computation time per step
 $\sim O(1/h) \times O(1/h^3) \sim O(1/h^4)$
 - Double the resolution, $h \rightarrow h/2$
16x computation time

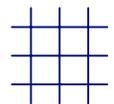
Resolution vs. computation time

- Partially alleviated by local mesh refinement
 - decrease effective h without increasing N too much
- Restriction on Δt still apply



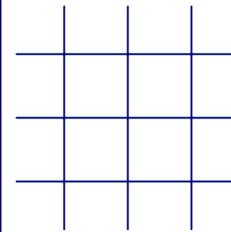
coarser resolution

finer resolution
small Δt

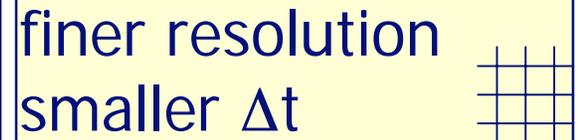


Local Time Stepping

- With solver coupling
 - local mesh refinement
 - Δt 's of solvers are independent
- Synchronization issue

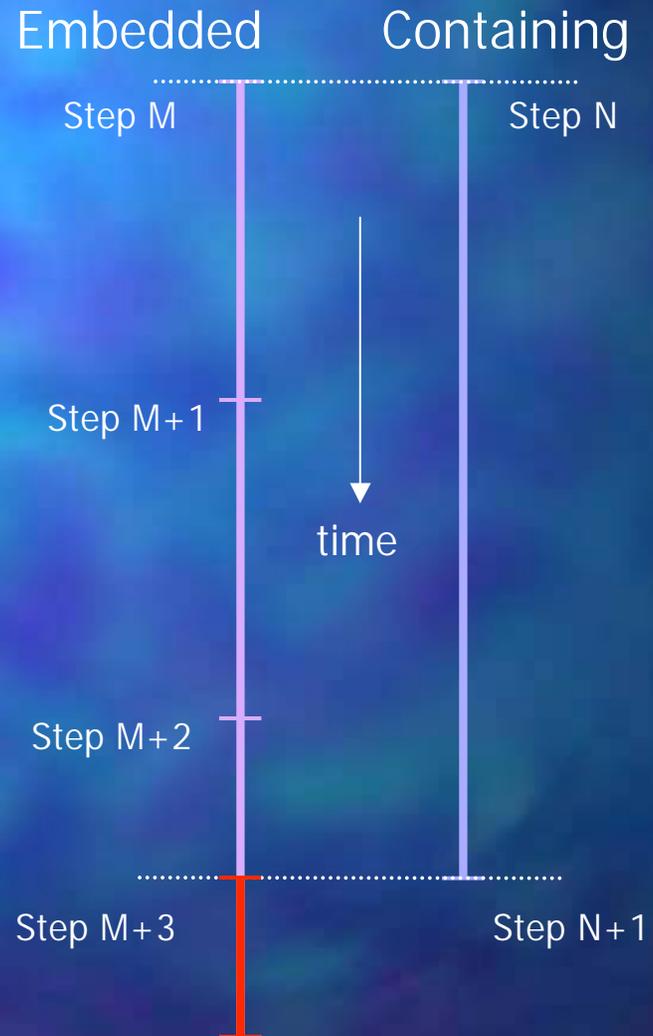


coarser resolution
larger Δt



finer resolution
smaller Δt

Time Synchronization

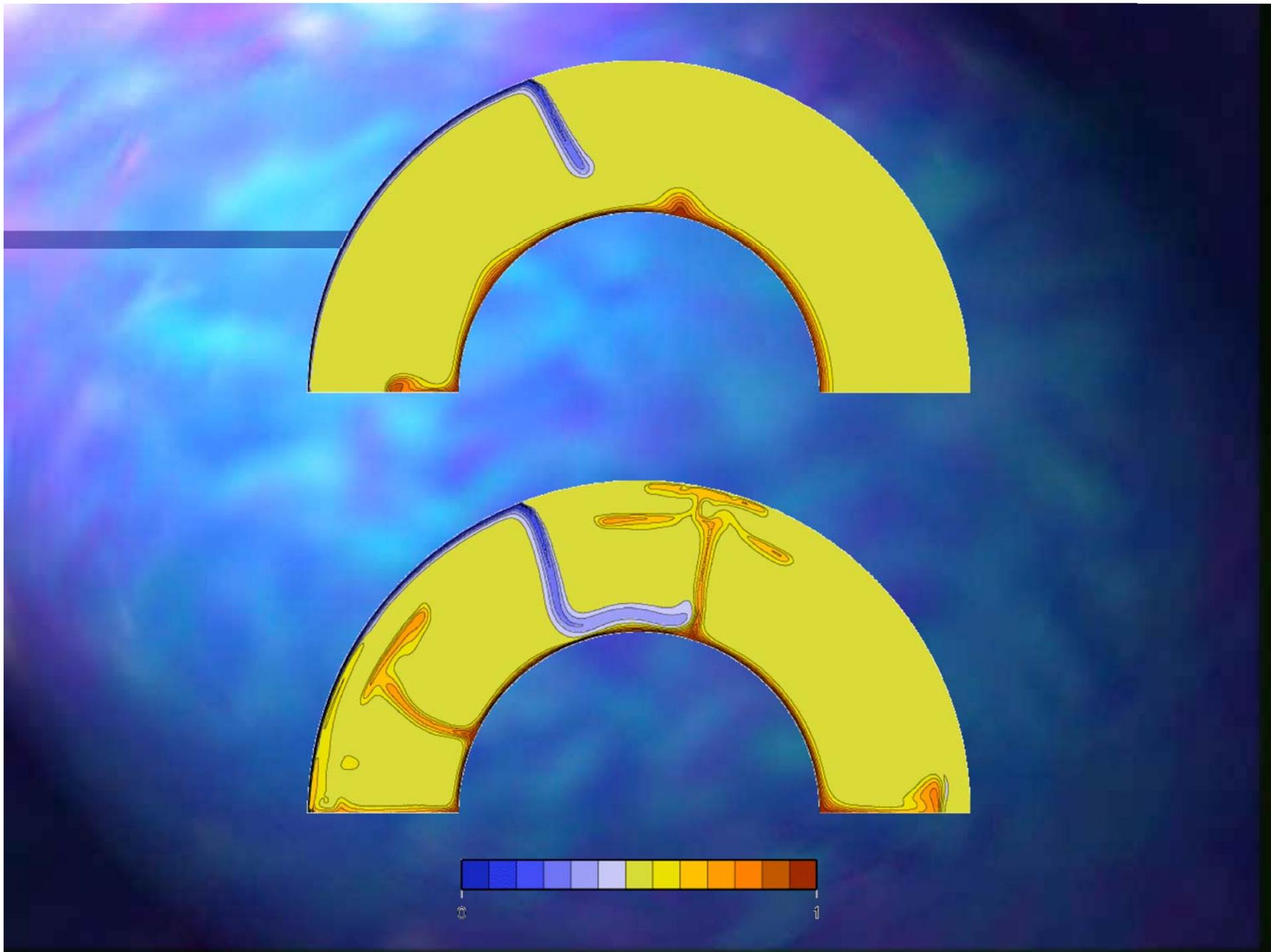


Boundary conditions

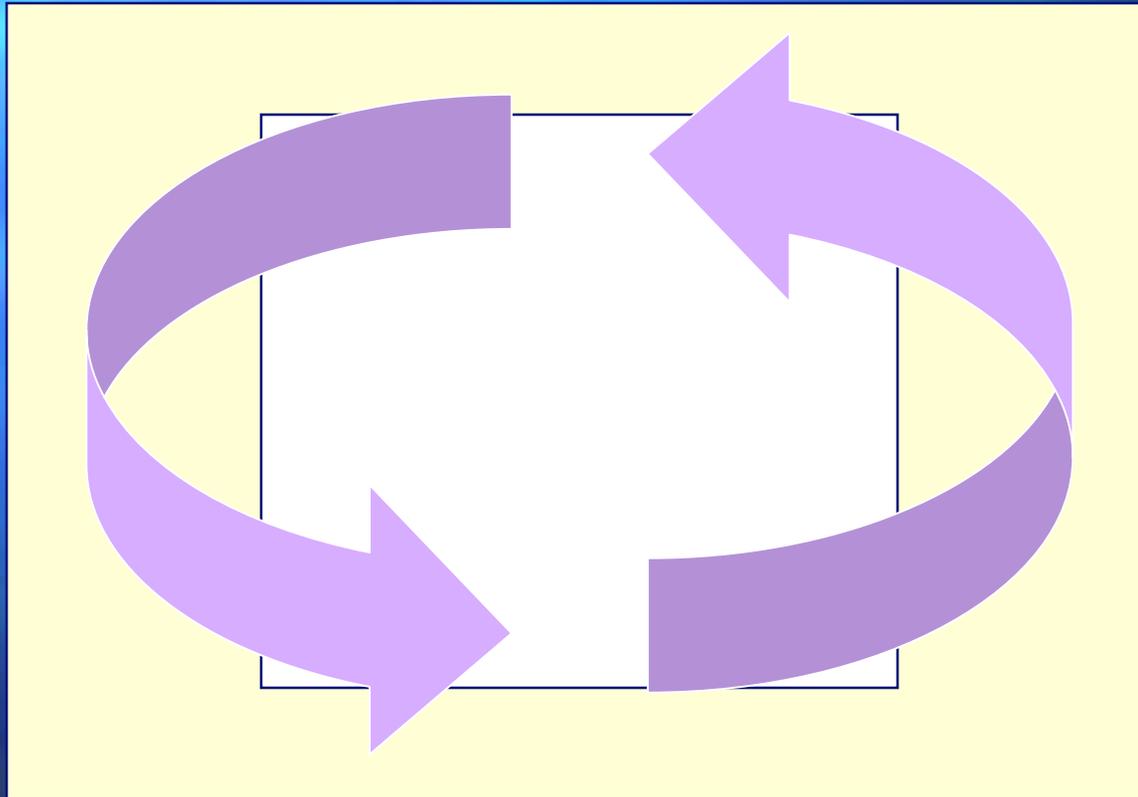
- Boundary conditions are important for Stokes problems
- Boundary is usually put far away from the region of interest
 - local mesh refinement

Self-consistent boundary conditions

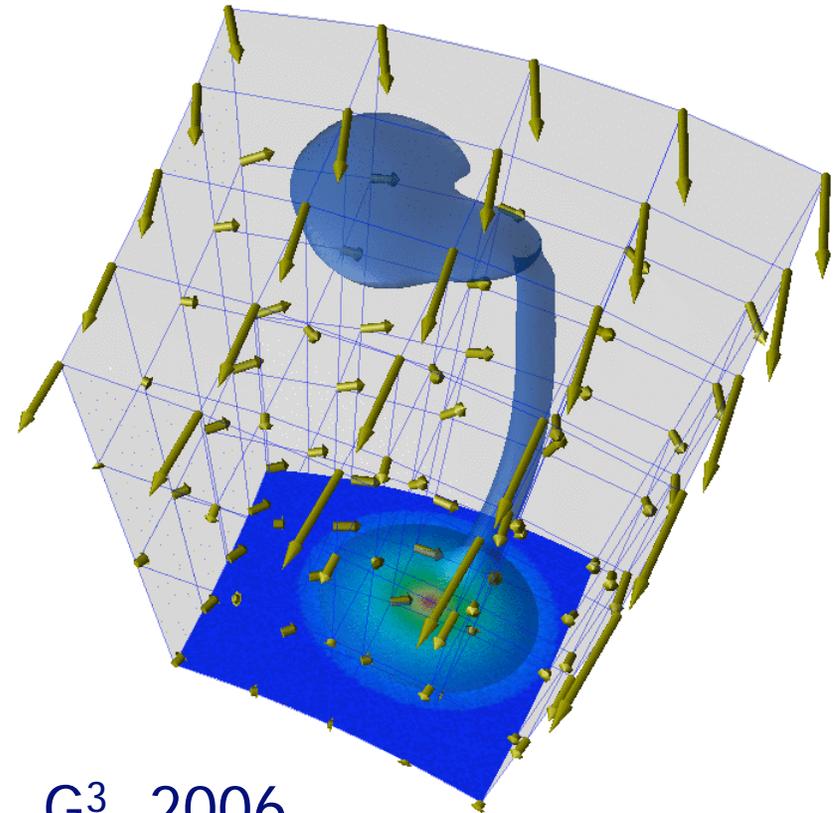
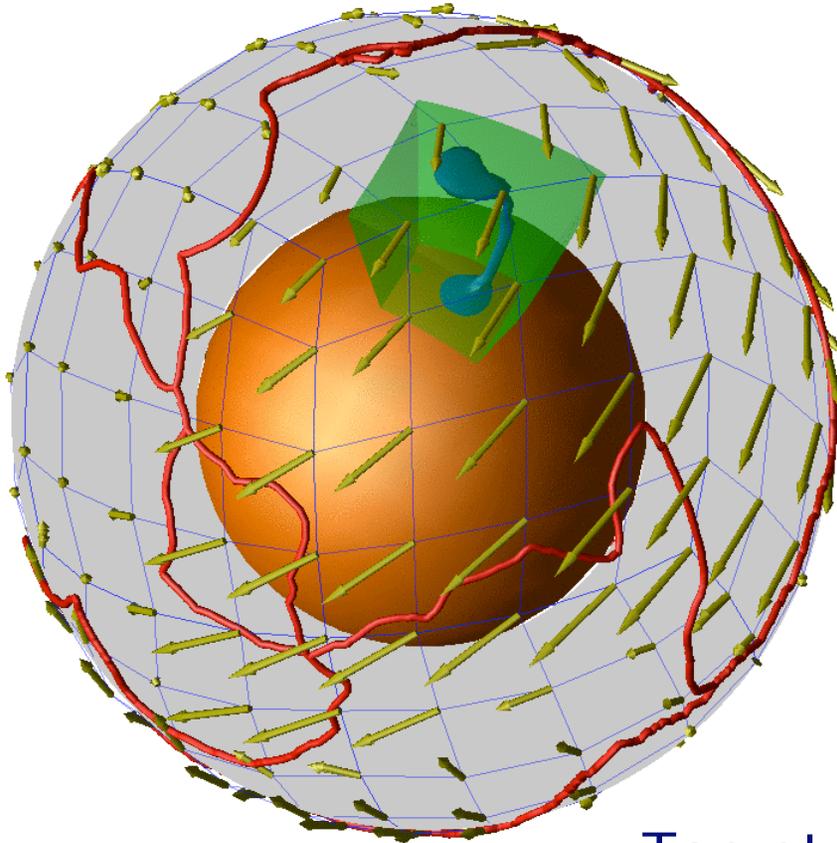
- Types of BCs for Stokes problems:
 - pinned ($V=0$), fixed velocity ($V=\text{const}$), free ($\sigma=0$), traction ($\sigma=\text{const}$)
 - usually BCs are not varying in time
- Changes in the region of interest can potentially change the BCs



Self-consistent boundary conditions



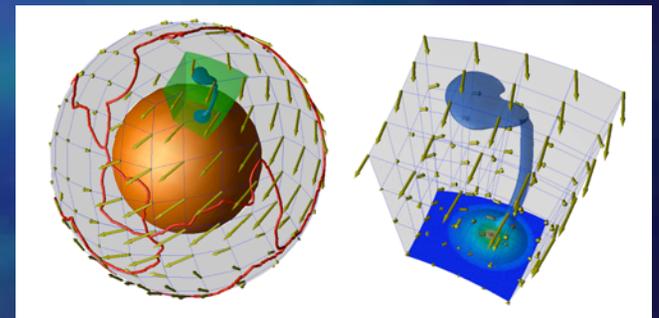
CitcomS-CitcomS Coupling



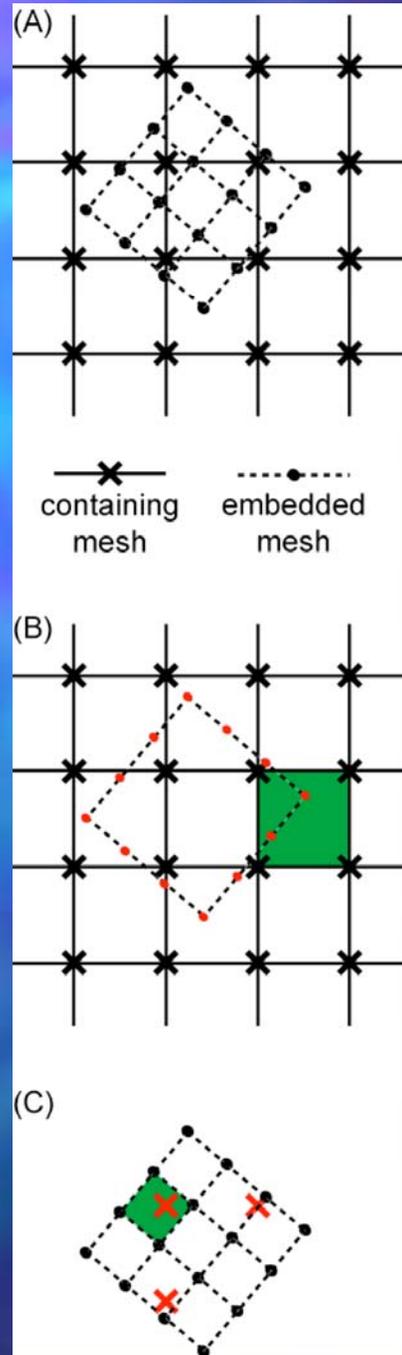
Tan et al., G³, 2006

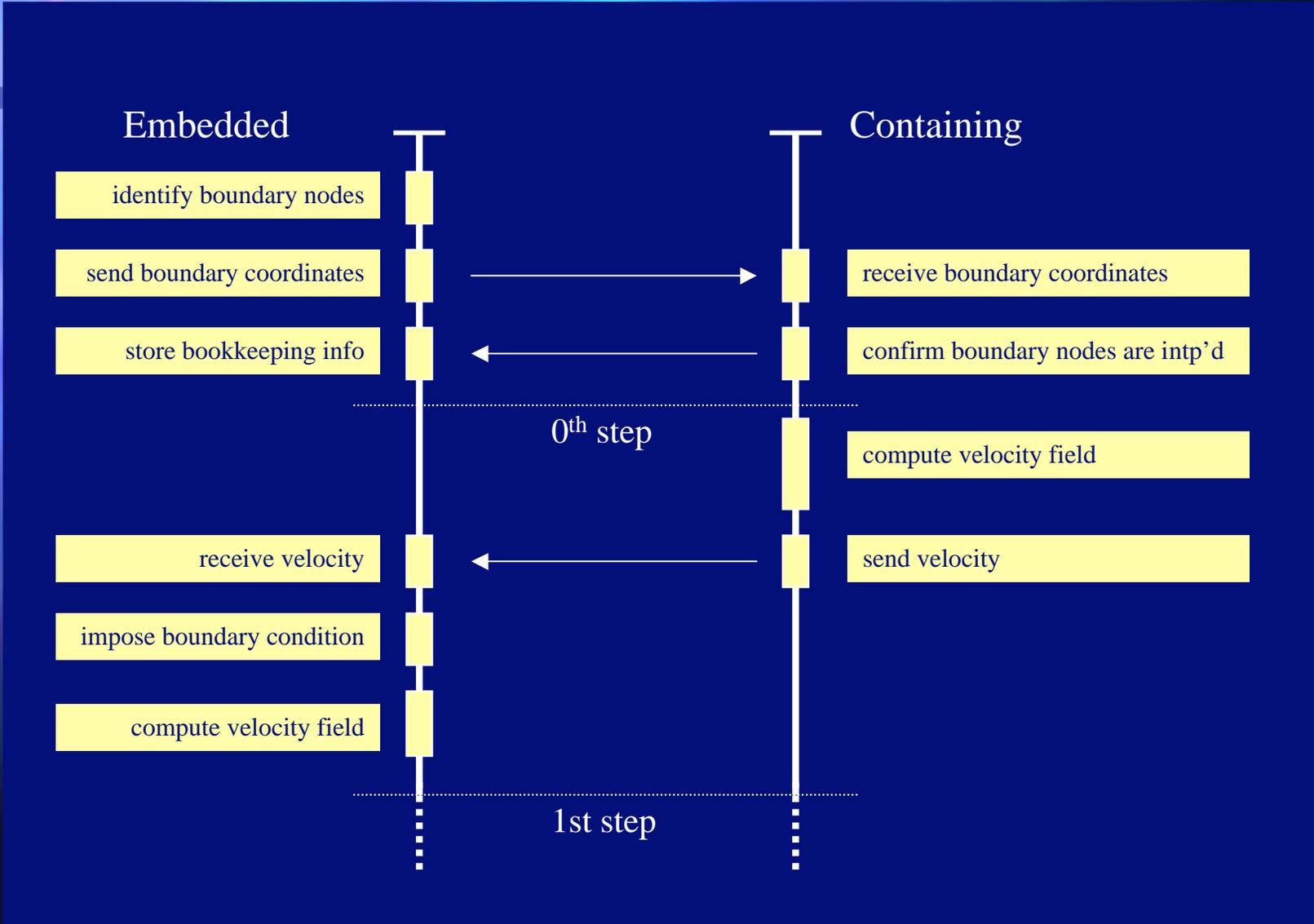
CitcomS-CitcomS Coupling

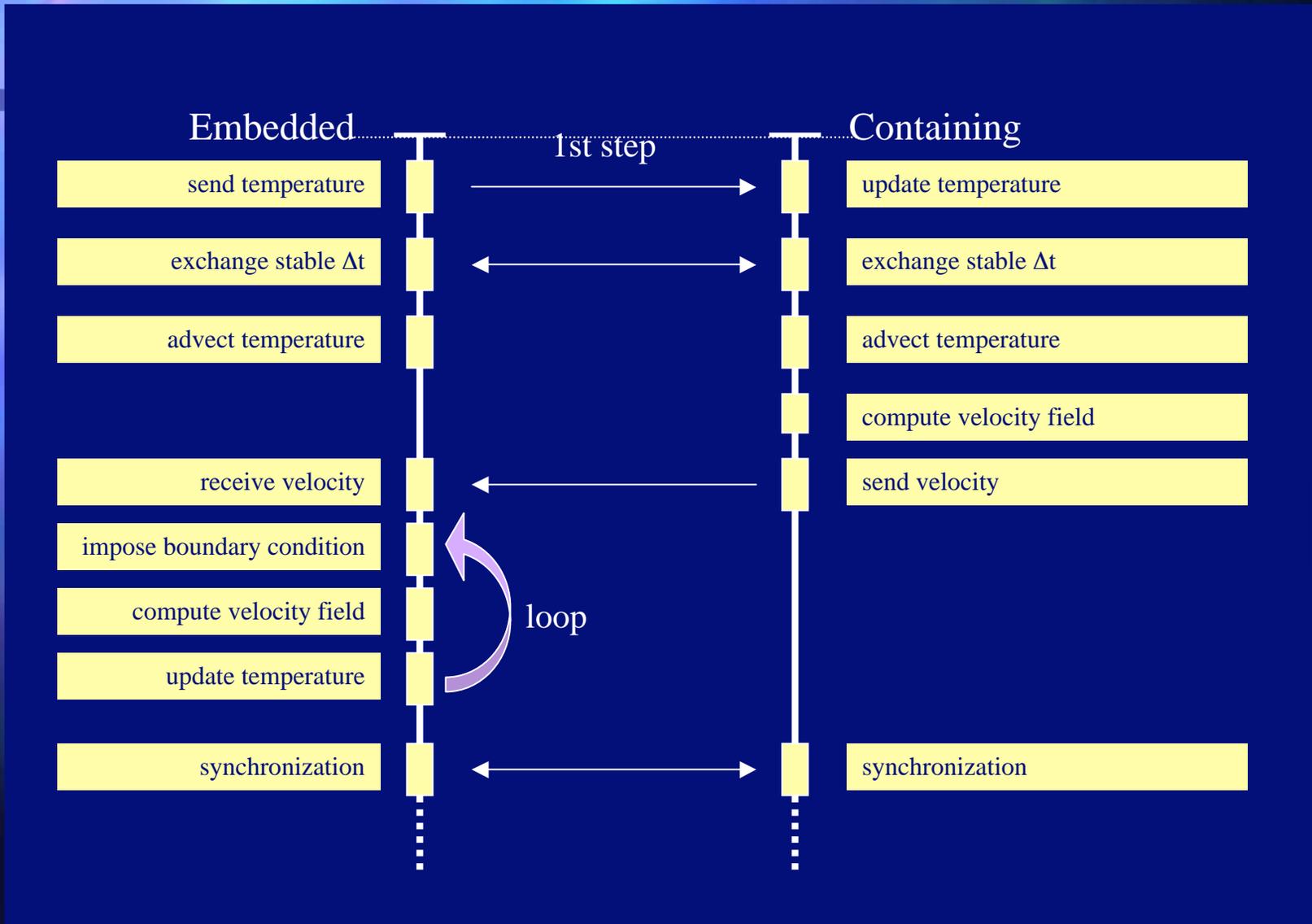
- Containing -> Embedded
 - boundary conditions: fixed temperature + normal velocity + shear stress
 - using 3 components of velocity for BCs will cause mesh locking
- Embedded -> Containing
 - temperature field



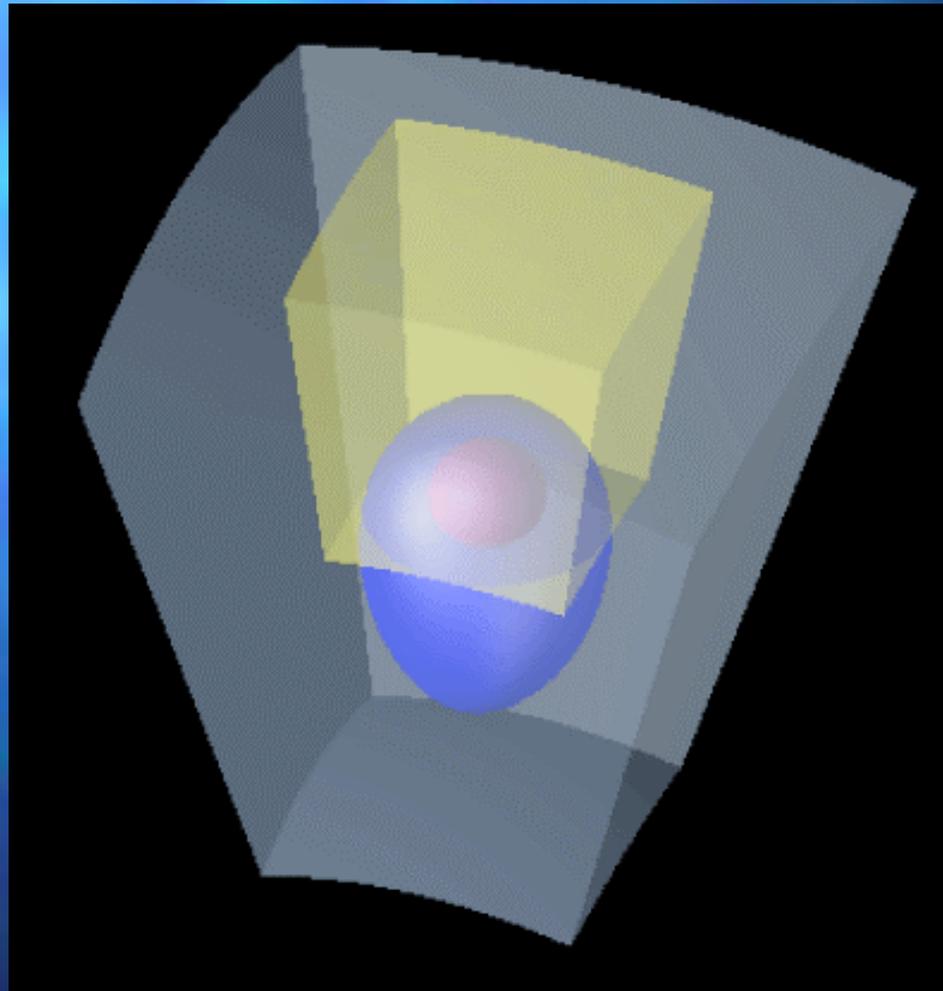
Interpolation

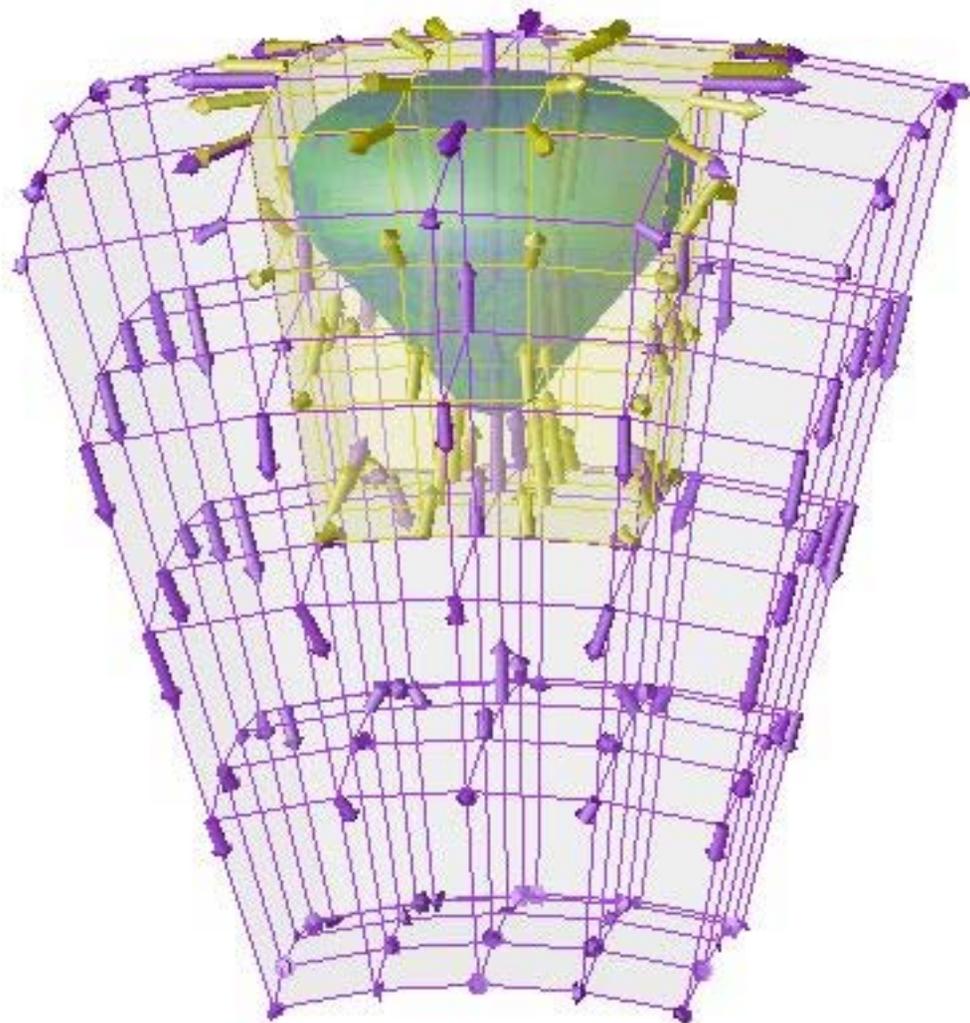


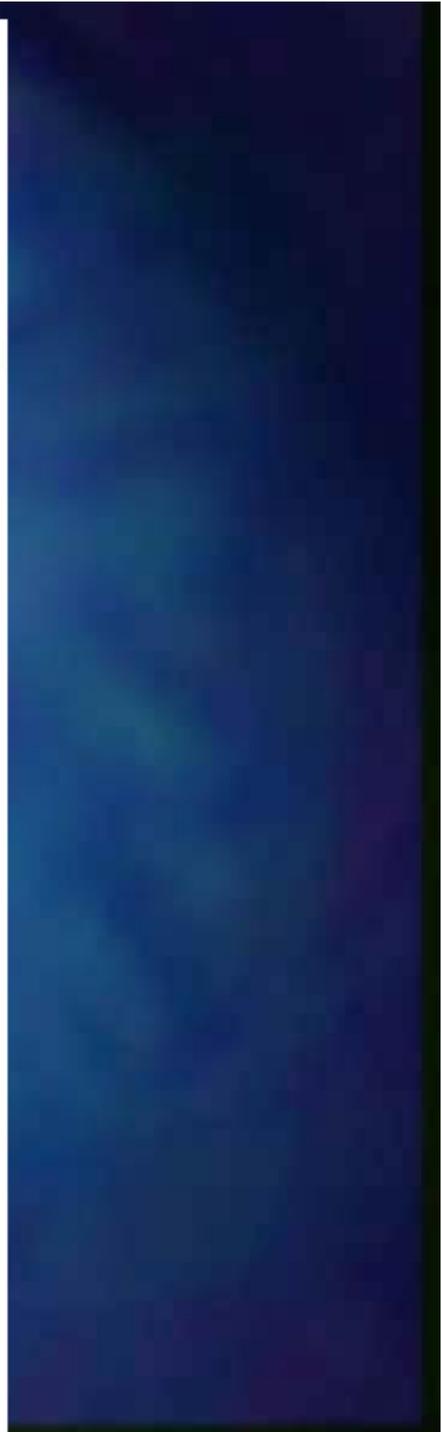
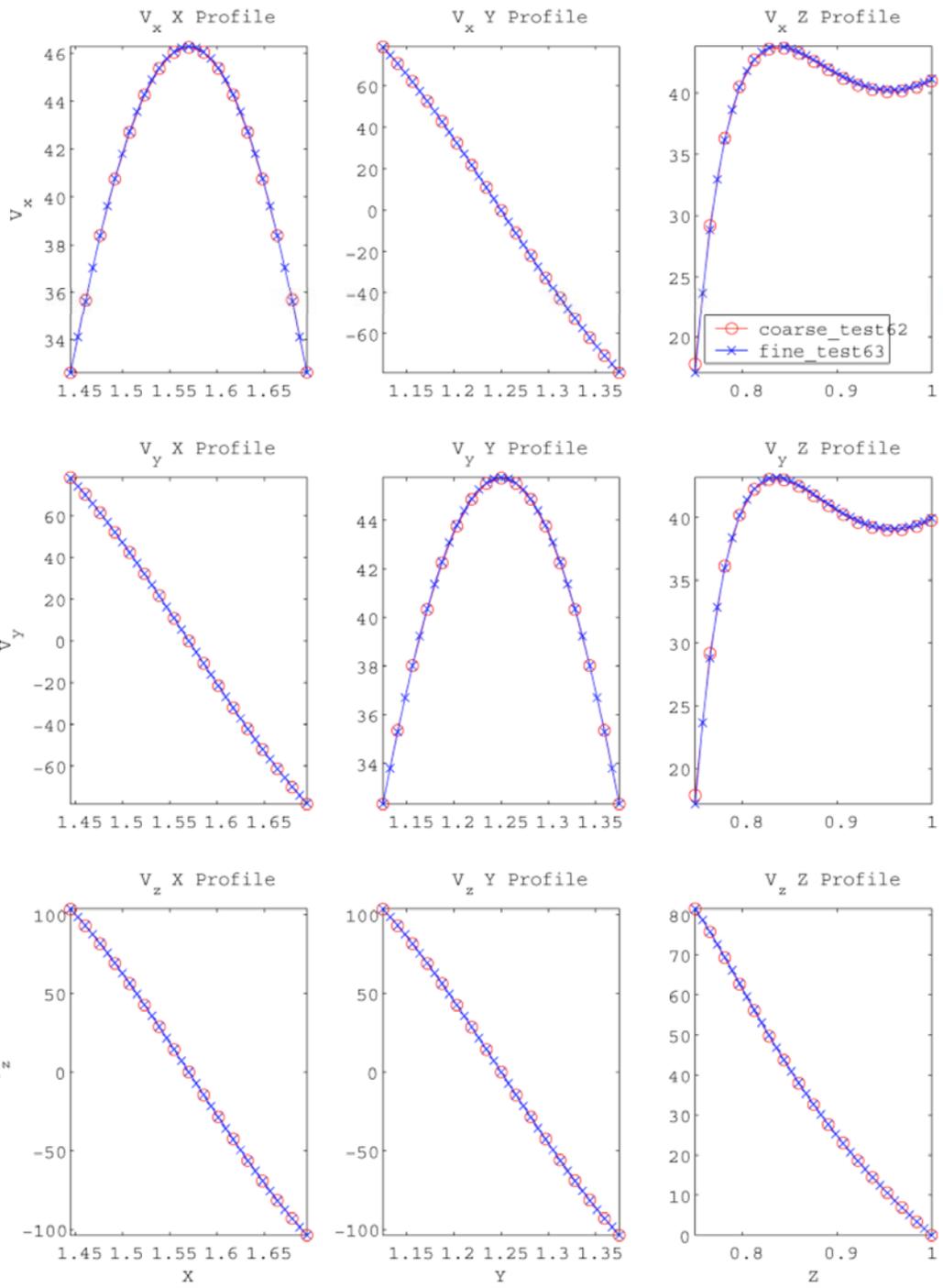




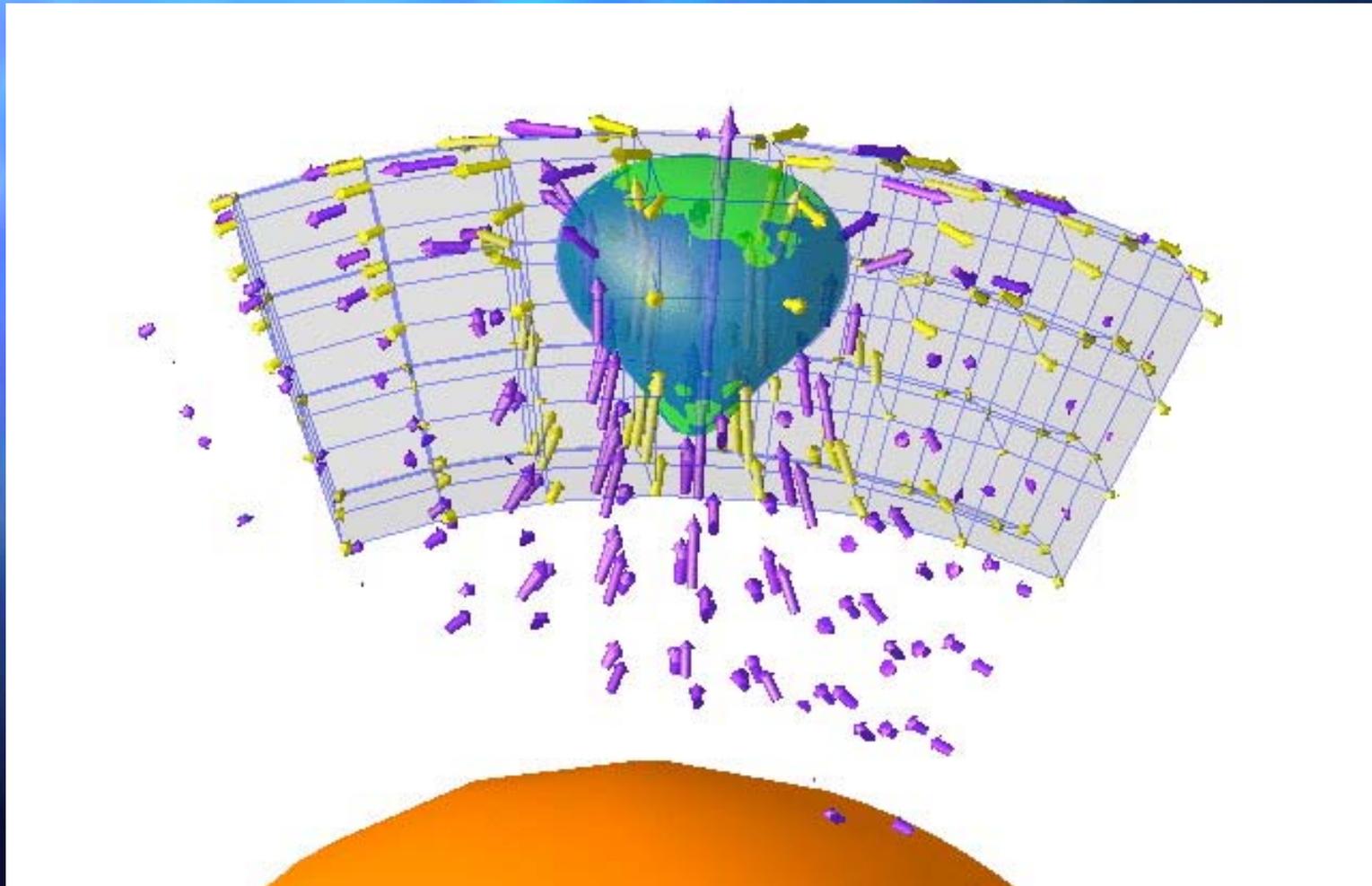
Validation (Regional-Regional)

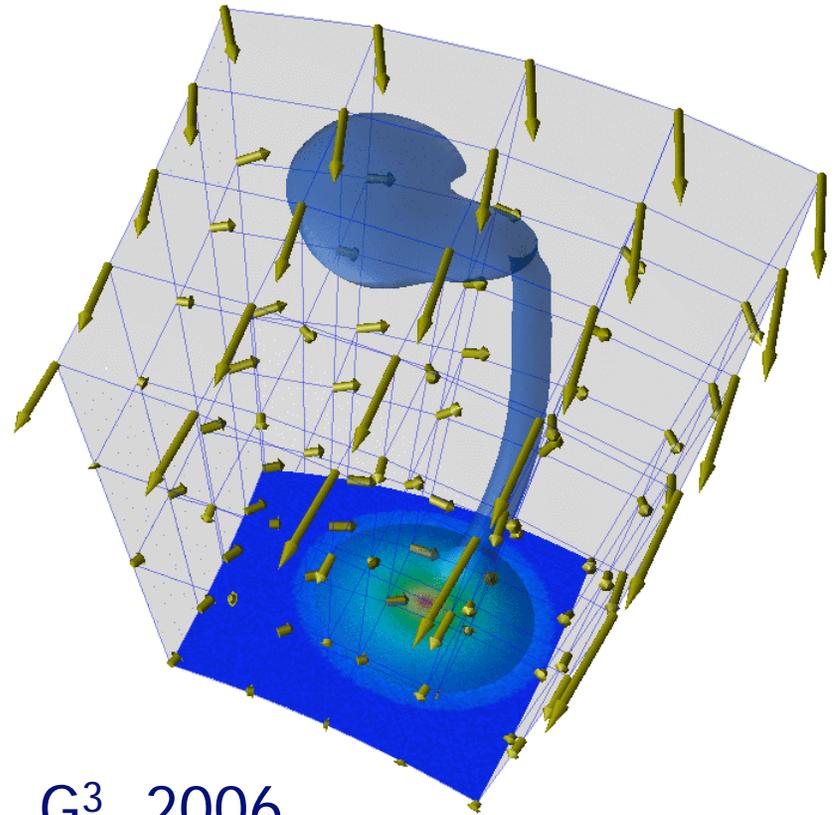
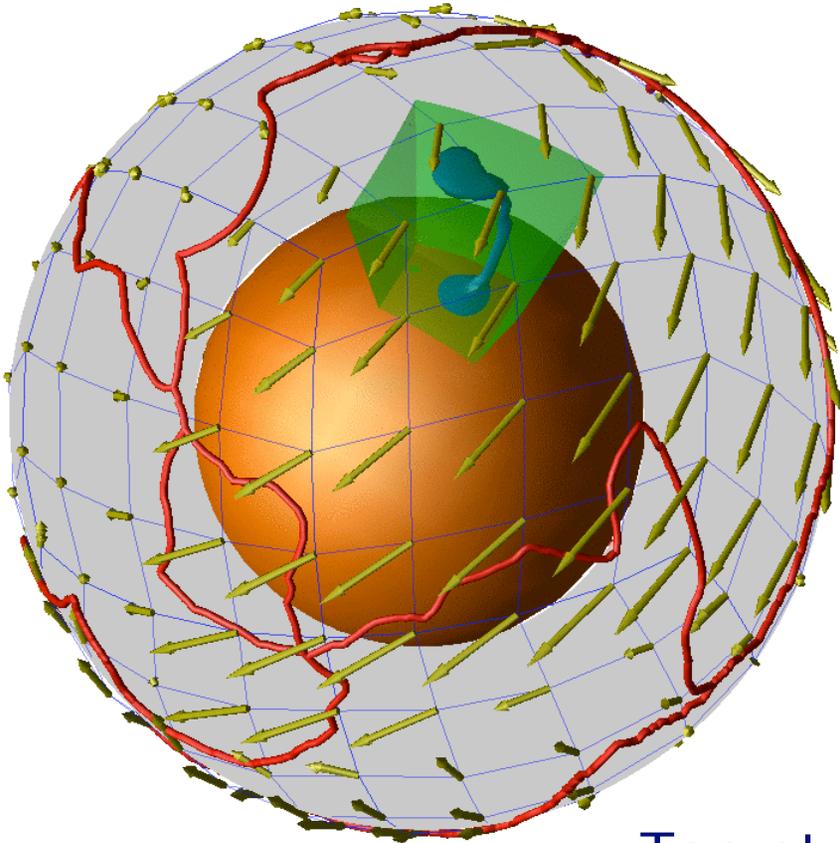






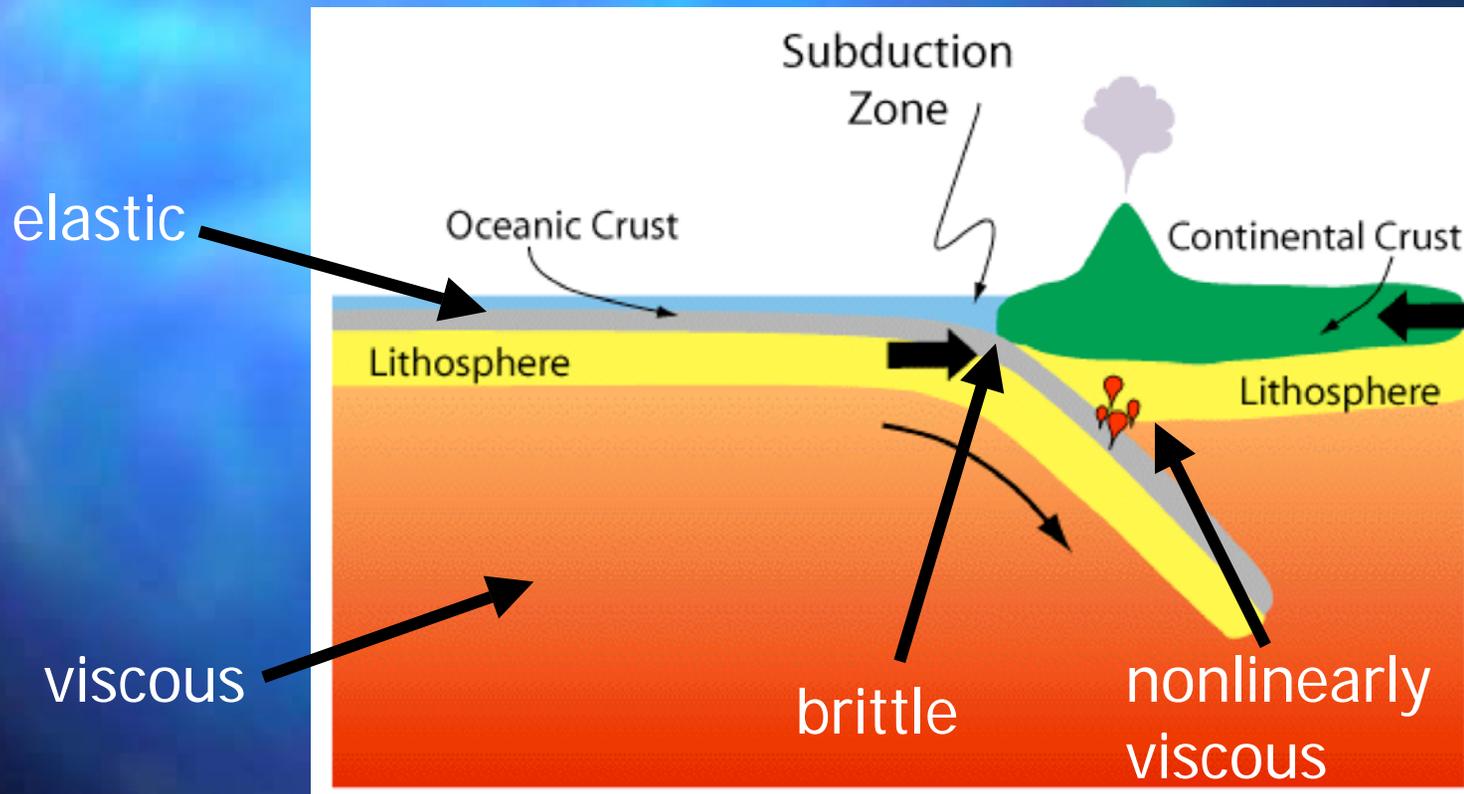
Validation (Global-Regional)



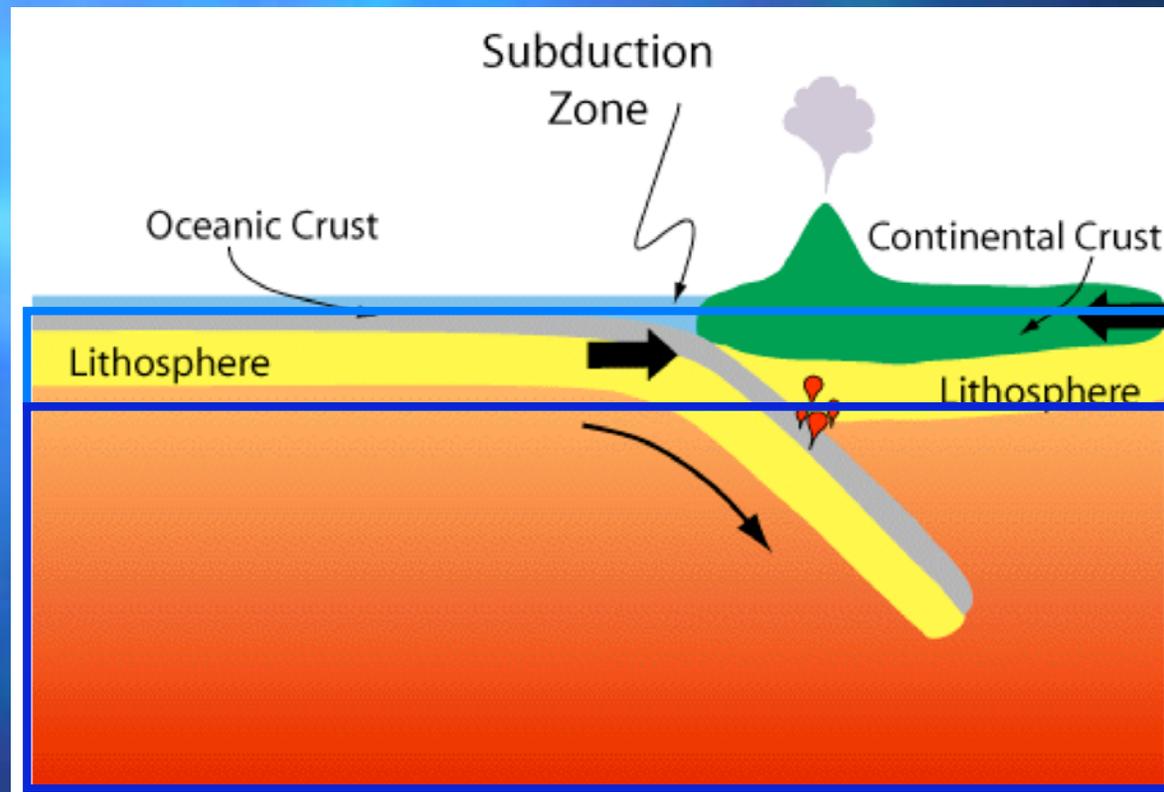


Tan et al., G^3 , 2006

Multi-physics

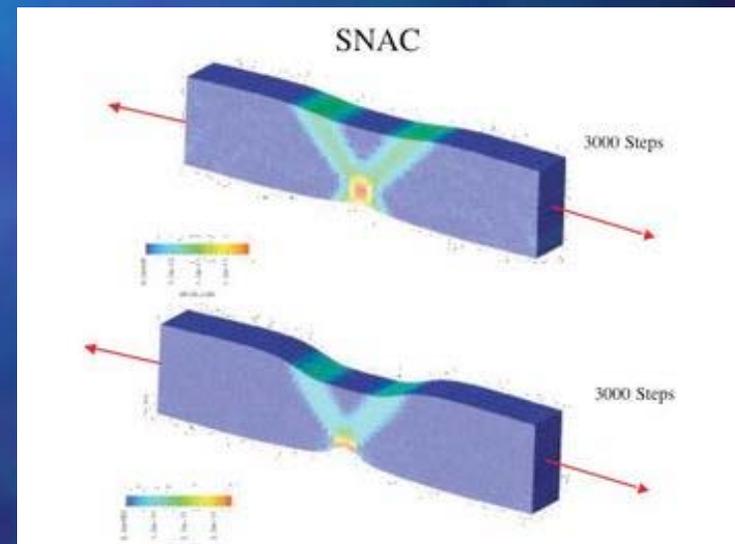


Multi-physics

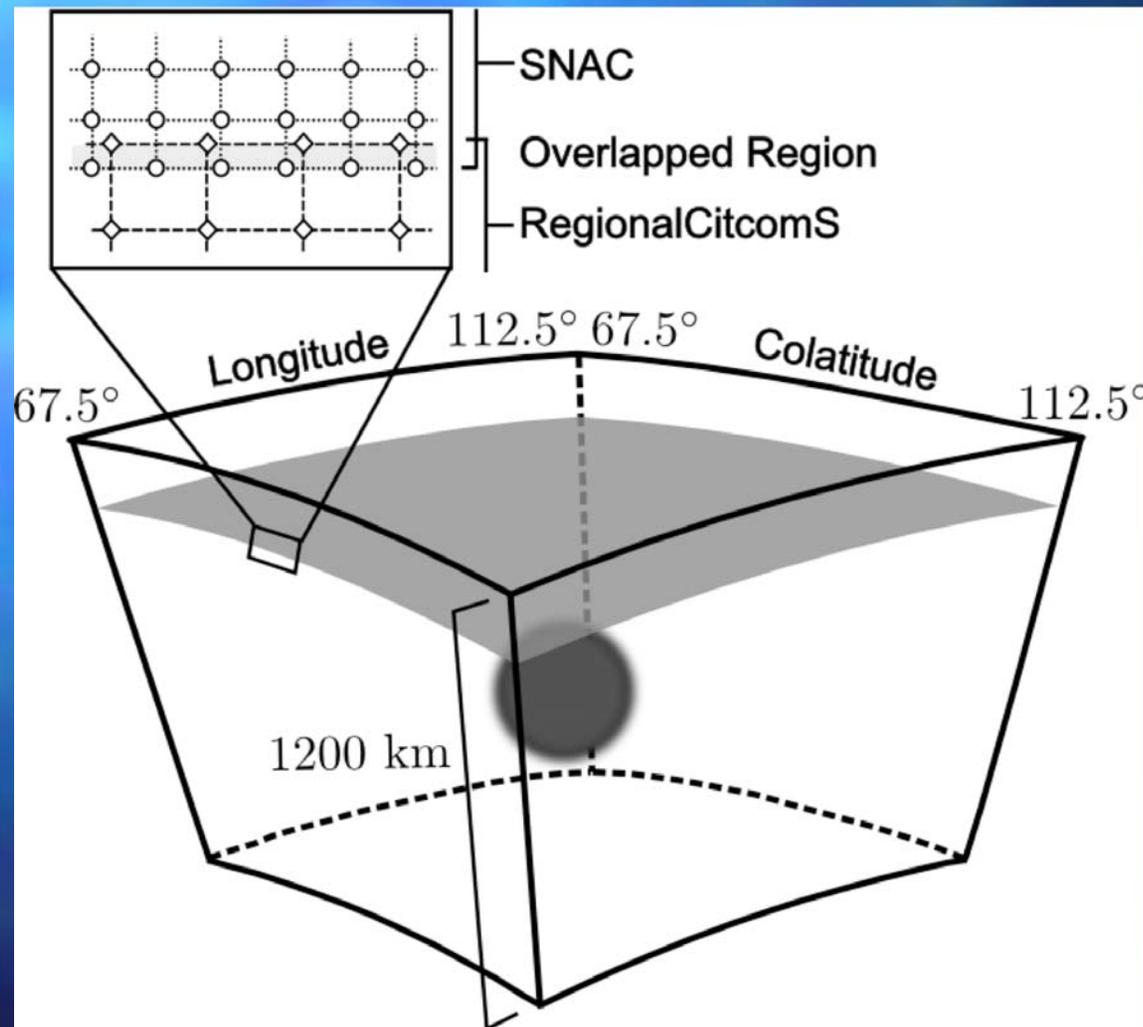


SNAC

- 3D Lagrangian visco-plasto-elastic FD code (Choi & Gurnis, EPSL, 2008)
- FLAC algorithm for Stokes solver
 - explicit solver, pseudo inertia
 - quasi-static equilibrium state



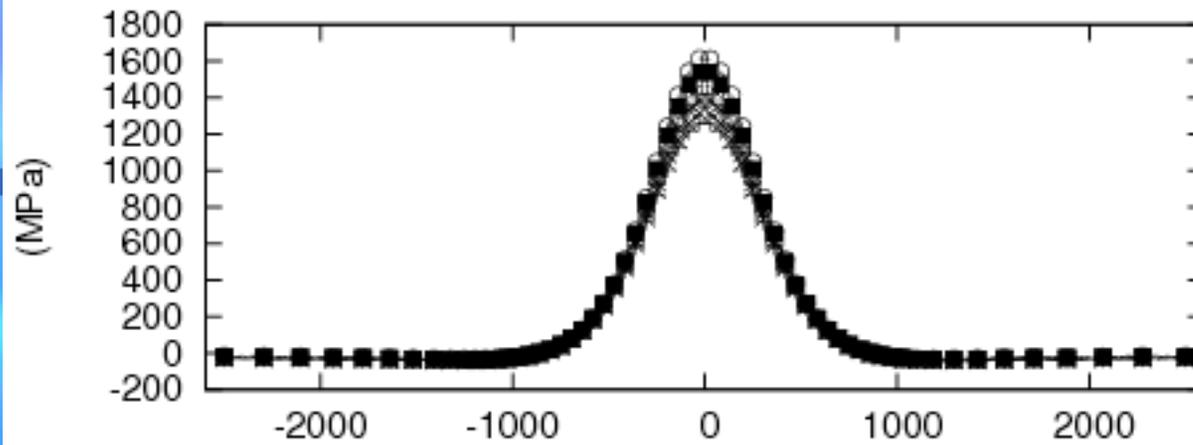
SNAC-CitcomS coupling



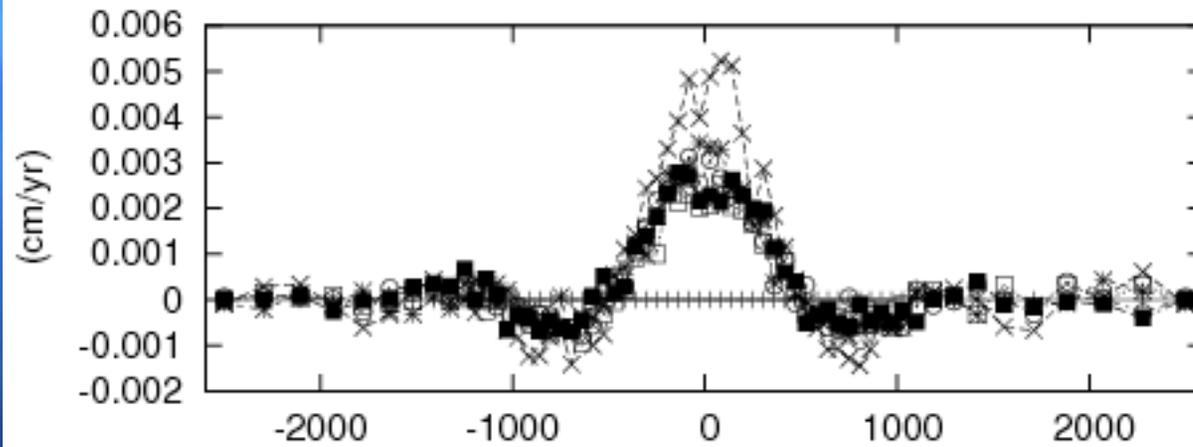
SNAC-CitcomS coupling

- CitcomS -> SNAC:
 - boundary conditions for bottom nodes: stress (traction) & temperature
- SNAC -> CitcomS:
 - velocity boundary conditions for top nodes
- All exchanged quantities are in Cartesian coordinates and SI units

Traction (radial component from CitcomS)

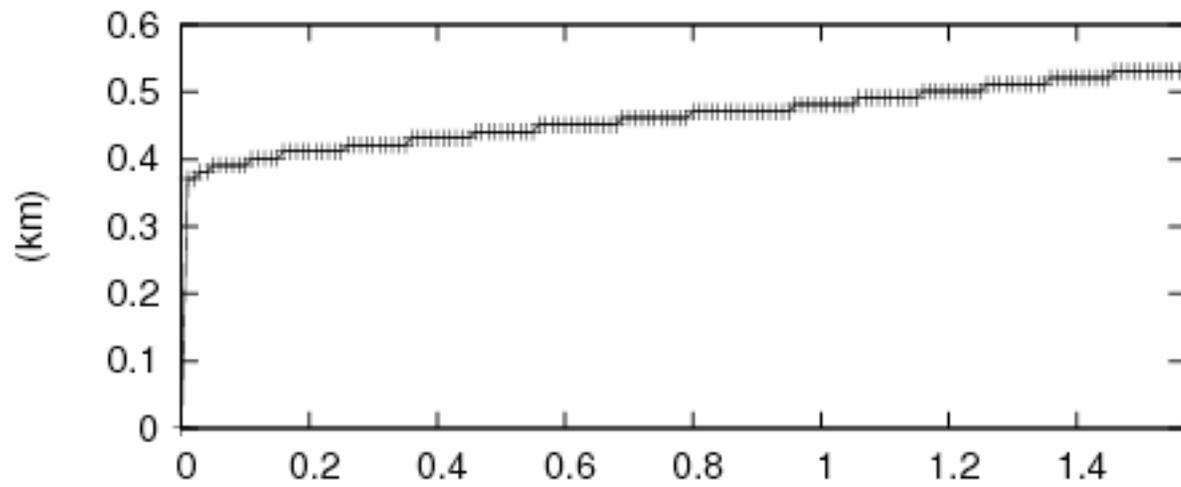


Velocity (radial component)

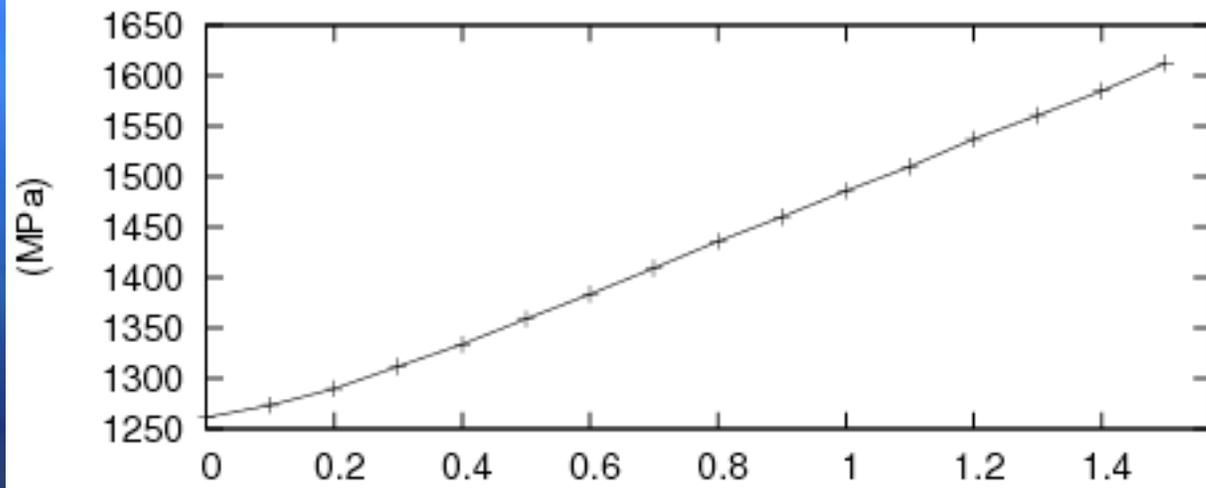


0.0 Myr	—+—	0.6 Myr	---*---	1.2 Myr	---■---
0.3 Myr	---x---	0.9 Myr	---□---	1.5 Myr	---○---

Topography



Traction (radial component)



Limitation

- Stokes solver: implicit (CitcomS) vs explicit (SNAC)
 - SNAC solution is not in a steady state
- Each CitcomS time step $\sim 10^4$ SNAC time steps
- Computing 1.5 Myrs took 10 days
 - 2 months for the hot blob to rise to surface

CitcomS Scaling Performance

Multi-core

- FE codes are memory bandwidth hungry
- Performance will degrade if run on multi-core machines
- Test: regional CitcomS 2x2x2 processors, total run time
 - 8 CPUs, 1 core/CPU, 688 sec., 100%
 - 4 CPUs, 2 cores/CPU, 771 sec., 89%
 - 2 CPUs, 4 cores/CPU, 975 sec., 70%

Parallel scaling (weak scaling)

- Fixed number of elements (32^3) per processors, constant viscosity, 50 time steps
- Not a right test for scaling. Take with a grain of salt.

# of proc.	run time	# of Uzawa iterations	time per iterations
12 (1x1x1)	60.53	112	0.54
24 (1x1x2)	54.33	95	0.57
48 (2x2x1)	43.99	73	0.60
96 (2x2x2)	45.17	74	0.61
192 (4x4x1)	35.94	55	0.65
384 (4x4x2)	37.02	55	0.67
768 (4x4x4)	42.36	58	0.73
1536 (8x8x2)	42.23	60	0.70
3072 (8x8x8)	41.53	54	0.77