

Overview and Schedule

Session 1. Introduction to ASPECT Basics

Session 2. Modifying and Coding in ASPECT

Session 3. Lithospheric Deformation*

- Overview of Viscoelasticity, Nonlinear Viscous Flow and Plasticity
- Example: (Bending Beam)
- Example: Continental Extension
- **Example: Brittle Thrust Wedge**
- Example: Subduction

Slides:

<https://bit.ly/aspect-tutorial-slides>

Questions:

post in Zoom chat 😊

Session 4. Two-Phase Flow

Session 5. Complex Model Design with the World Builder



Example: Brittle thrust wedge

Instructions:

1. Open a terminal and cd to the tutorial directory:

```
$ cd ~/aspect-tutorials/2020-tectonics-modeling-  
tutorial/session-3/
```

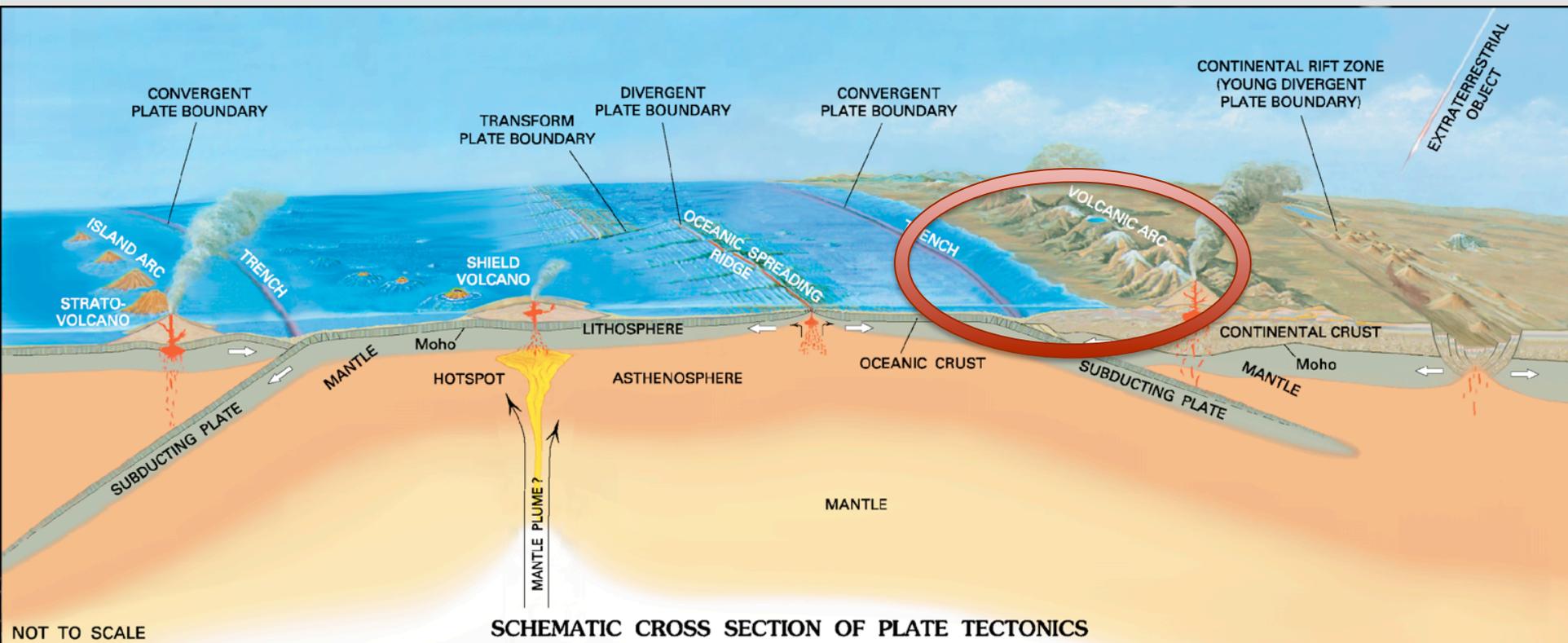
2. Run the model:

```
$ mpirun -np 2 ~/aspect/aspect-release  
brittle_thrust_wedge.prm
```

3. Running will take about 15 min



Compressional settings

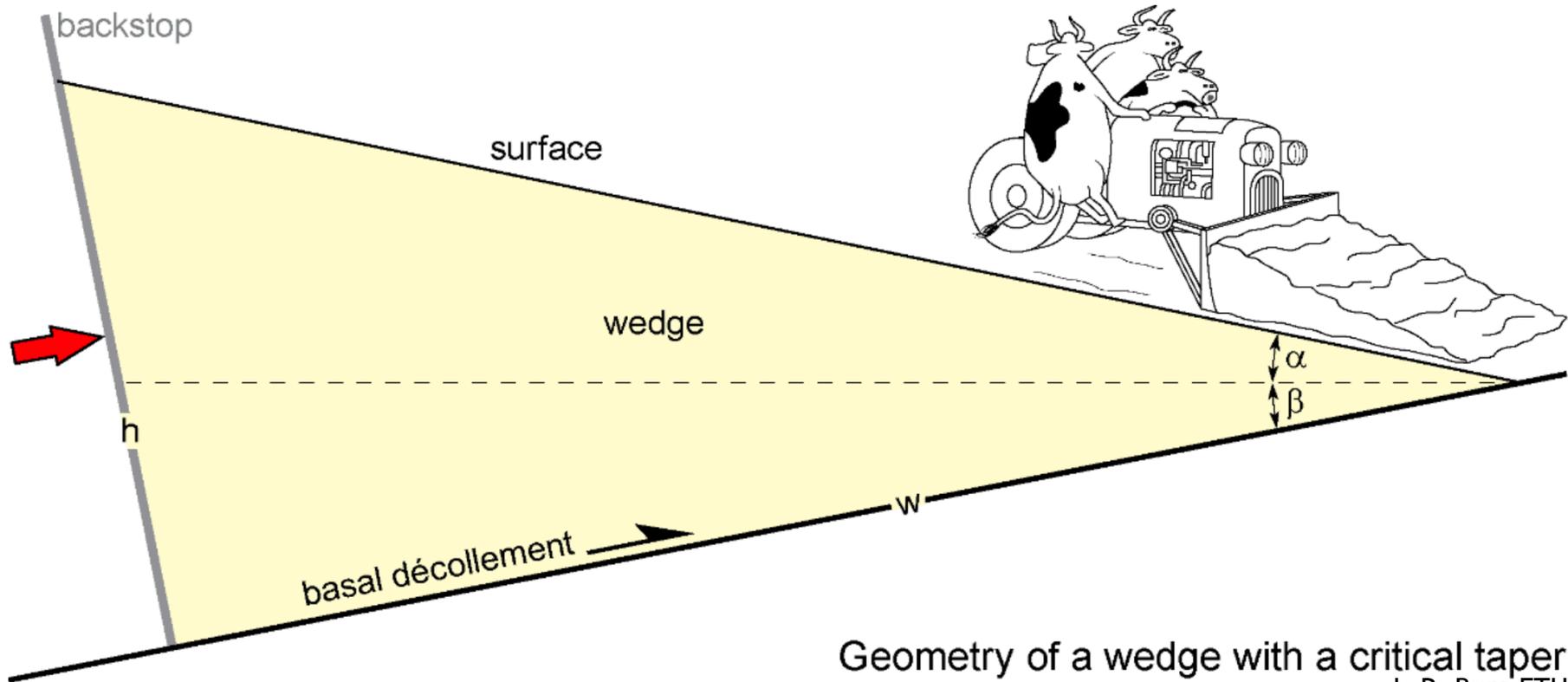


Fold-and-thrust belts and accretionary wedges form by offscraping of sediments and crustal materials from a lower plate and stacking these in the foreland of an orogen or at a subduction zone trench (Buiter et al. 2016)



Critical taper theory

A wedge of sediments or crustal material in front of “bulldozer” will deform until a certain critical angle is reached, the critical taper $\theta = \alpha + \beta$.



Geometry of a wedge with a critical taper

Mendeley Desktop

J.-P. Burg ETH



Based on the benchmark effort of [Buiter et al. \(2016\)](#):

- 11 numerical codes
- 15 analog labs
- 3 experimental setups:
 1. Translation of a 20° stable wedge
 2. Formation of unstable subcritical wedge that goes to critical taper
 3. Formation of unstable wedge through initial deformation away from the mobile wall



Based on the benchmark effort of Buiter et al. (2016):

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Time



pTatin 256x64 Q2P1



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Time

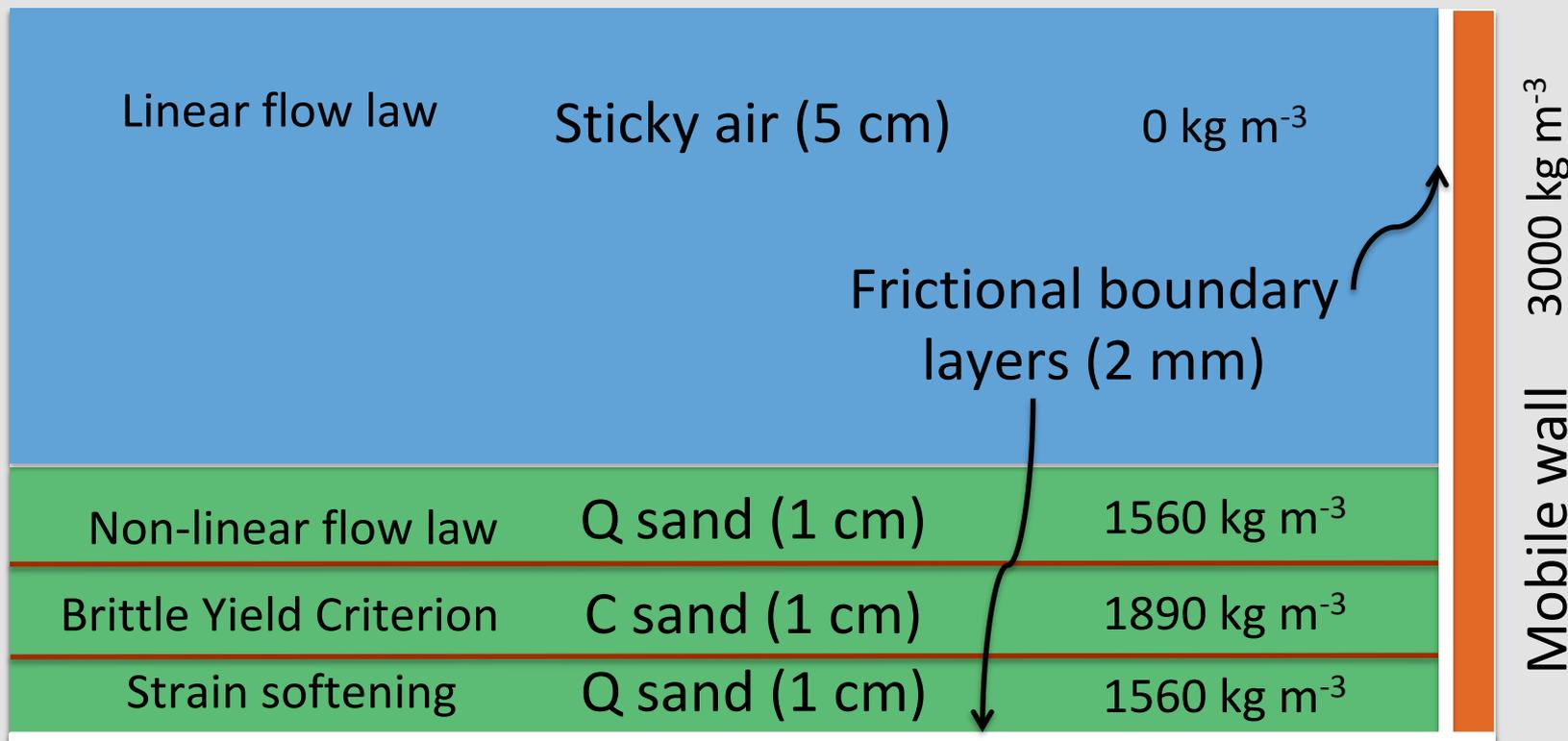


pTatin 256x64 Q2P1



Initial composition & material properties

$y = 8 \text{ cm}$



$x = 0 \text{ cm}$

$y = 0 \text{ cm}$

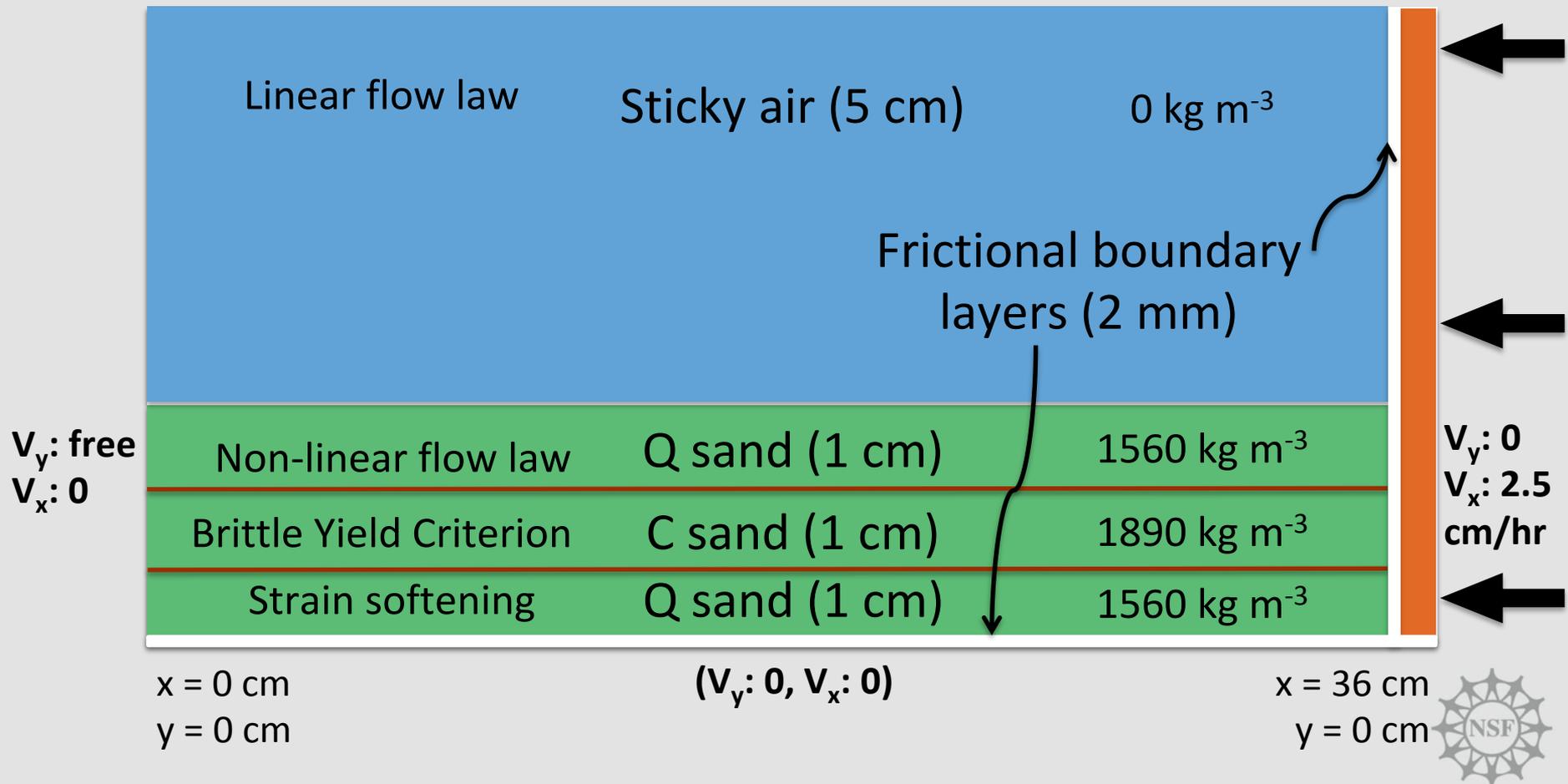
$x = 36 \text{ cm}$

$y = 0 \text{ cm}$



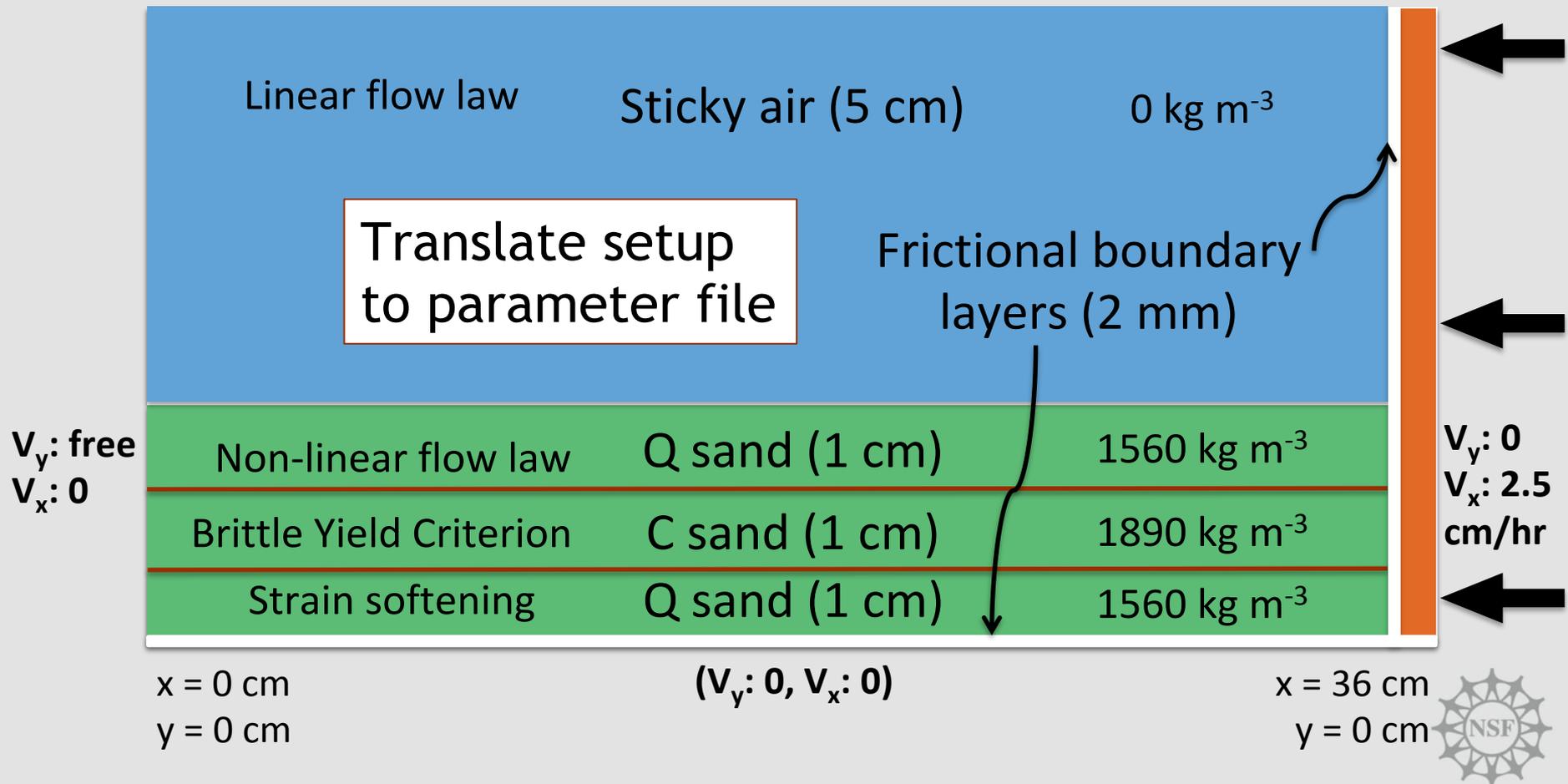
Velocity Boundary Conditions

$y = 8 \text{ cm}$ **Open Surface** \rightarrow Zero stress ($V_y = \text{free}$, $V_x = \text{free}$)



Velocity Boundary Conditions

$y = 8 \text{ cm}$ **Open Surface** \rightarrow Zero stress ($V_y = \text{free}$, $V_x = \text{free}$)



Parameter file: Global parameters

Open brittle_thrust_wedge.prm in ~/aspect-tutorials/2020-tectonics-modeling-tutorial/session-3/ with vi or leafpad

```
$vi brittle_thrust_wedge.prm
```

which is an adapted version of

```
$ASPECT_DIR/benchmarks/buiter_et_al_2016_jsg/  
exp_2_low_resolution.prm
```

```
set Dimension = 2  
set Start time = 0 [seconds]  
set End time = 14400 #10 cm  
set Use years in output instead of seconds = false  
set CFL number = 0.8  
set Pressure normalization = surface
```

Pressure at top boundary is zero on average



Parameter file: Solver settings

```
set Nonlinear solver scheme      = single Advection,  
                                iterated Stokes
```

```
set Nonlinear solver tolerance  = 1e-7
```

```
set Max nonlinear iterations    = 100
```

Viscosity depends on solution variables
pressure and velocity (i.e. strain rate)
→ iterative solver

```
subsection Solver parameters
```

```
subsection Stokes solver parameters
```

```
set Linear solver tolerance      = 1e-8
```

```
set Number of cheap Stokes solver steps = 200
```

Try poor, but cheaper preconditioner for GMRES solver

```
set GMRES solver restart length  = 200
```

```
end
```

```
end
```

Increase length of solver history taken into account;
helps with localized viscosity jumps.



Time steps:

Nonlinear iterations:

In *Material model*:

1. Calculate an effective viscous viscosity η_{eff}^v
2. Calculate the viscous stress $\sigma^v = 2\eta_{eff}^v \dot{\epsilon}_{eff}$
3. Calculate the plastic yield strength

$$\sigma_y^p = C \cos \phi + P \sin \phi$$

4. If $\sigma^v > \sigma_y^p \rightarrow$ return $\eta_{eff}^{vp} = \frac{\sigma_y^p}{2\dot{\epsilon}_{eff}}$
5. If $\sigma_y^p > \sigma^v \rightarrow$ return η_{eff}^v

Solve Stokes equations with updated η_{eff}
to get updated P and \mathbf{v}

Inner iterations

Exit iterations when tolerance or max met.



Time steps:

Nonlinear iterations:

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Solve Stokes equations with updated η_{eff}^v
to get updated

Inner it

Linear solver tolerance
Number of cheap Stokes solver steps
GMRES solver restart length

Nonlinear solver tolerance
Max nonlinear solver iterations



subsection Discretization

```
set Temperature polynomial degree = 1  
set Use discontinuous composition discretization = true
```

Discontinuous Galerkin (DG) for compositional fields instead of continuous discretization
→ preserves compositional boundaries better

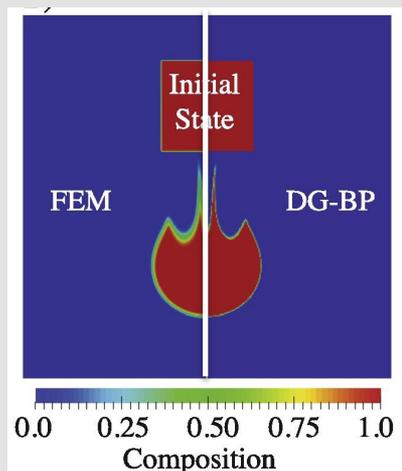
subsection Stabilization parameters

```
set Use limiter for discontinuous composition solution = true  
set Global composition maximum = 1, 1, 1, 1, 100  
set Global composition minimum = 0, 0, 0, 0, 0
```

end

I.c.w. DG: set global min and max limit for each compositional field

end



[He et al. 2017, PEPI](#)



Parameter file: Geometry

```
subsection Geometry model
  set Model name           = box

  subsection Box
    set X extent           = 0.36
    set Y extent           = 0.08
    set X repetitions      = 45
    set Y repetitions      = 10
  end
end
```

Dimensions: 36x8 cm

Divide the coarse grid to get 1:1 aspect ratio of mesh cells.



Parameter file: Composition

```
subsection Compositional fields
  set Number of fields = 5
  set Names of fields = qsand,csand, bound, block, total_strain
end
```

```
subsection Initial composition model
  set Model name = function
  subsection Function
    set Variable names = x,y
    set Function constants = w1=0.35, w2=0.355, h1=0.002, \
                             h2=0.012, h3=0.022, h4=0.032
    set Function expression = if((x<w1 & y<=h2 & y>h1) \
                                || (x< w1 & y>h3 & y<=h4), 1,0);\
                             if((x<w1 & y>h2 & y<=h3), 1,0); \
                             if((x>=w1 & x<=w2 & y>h1) \
                                ||(y<=h1), 1, 0); \
                             if(x>w2 & y>h1,1,0); \
                             0
  end
end
```

Use backslash \ to continue expression on a newline

total_strain is zero everywhere

Parameter file: Composition

```
subsection Boundary composition model  
  set Fixed composition boundary indicators = right  
  set List of model names                = initial composition  
end
```

Fix composition at inflow boundary,
but not elsewhere because material will move and strain will increase over time



Parameter file: Temperature

```
subsection Initial temperature model
  set Model name = function

  subsection Function
    set Function expression = 293
  end

end

subsection Boundary temperature model
  set Fixed temperature boundary indicators = bottom,top,\
                                             right
  set List of model names = initial temperature
end
```

Temperature plays no role,
but we should set boundary conditions for inflow boundaries.



Parameter file: Velocity & stress BC

```
subsection Boundary velocity model
  set Zero velocity boundary indicators      = bottom
  set Tangential velocity boundary indicators = left
  set Prescribed velocity boundary indicators = right: function

  subsection Function
    set Variable names      = x,y
    set Function constants  = cm=0.01, h=3600, th=0.002
    set Function expression = \
                                if(y>th, -2.5*cm/h, -(y/th)*2.5*cm/h); 0
```

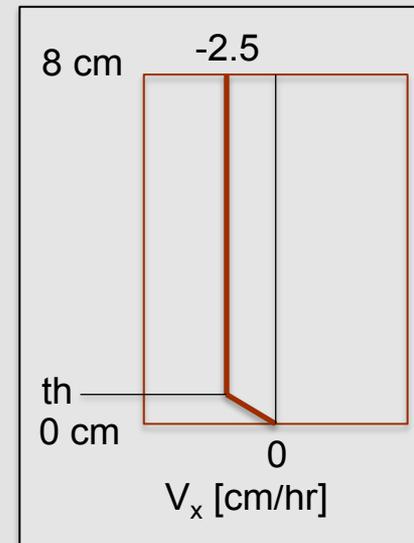
end
end

Prescribe the motion of mobile wall on the right boundary, with a gradual transition to zero towards the bottom of the domain. NB: velocity is interpreted in m/s.

```
subsection Boundary traction model
  set Prescribed traction boundary indicators =
    top: zero traction
```

end

Top boundary is open to flow leaving the domain to compensate for prescribed inflow.



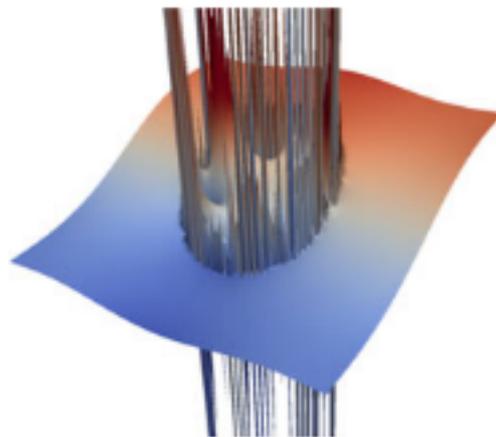
Parameter file: Material parameters

```
subsection Material model  
set Material averaging  
set Model name
```

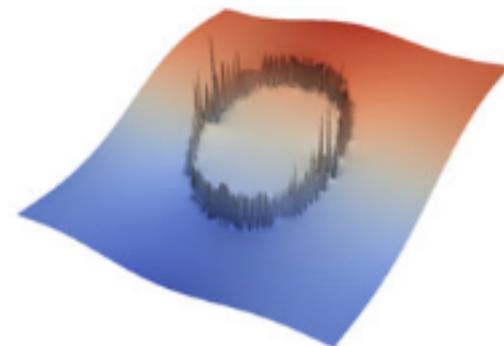
= harmonic average
= visco plastic

Average material
properties over
mesh cell when
assembling.

P field of sinker benchmark with strong density and viscosity contrast.



$[-45.2, 45.2]$



$[-2.67, 2.67]$

[Heister et al. 2017, GJI](#)



Parameter file: Material parameters

```
subsection Material model
  set Material averaging           = harmonic average
  set Model name                  = visco plastic

subsection Visco Plastic
  set Reference temperature       = 293
  set Reference viscosity         = 1e8
  set Minimum strain rate         = 1e-20
  set Reference strain rate       = 2e-5
  set Minimum viscosity           = 1e5
  set Maximum viscosity           = 1e12

  set Thermal diffusivities       = 1e-6
  set Heat capacities             = 750
  set Densities                   = 0, 1560, 1890, 1560, 3000, 1e5
  set Thermal expansivities       = 0
  set Viscosity averaging scheme = harmonic
```

Average material properties over mesh cell when assembling.

Same value used for all compositions.

Supply values for n_compositions+1 fields

Average contributions of all compositions to viscosity in evaluated points harmonically.



Parameter file: Material parameters

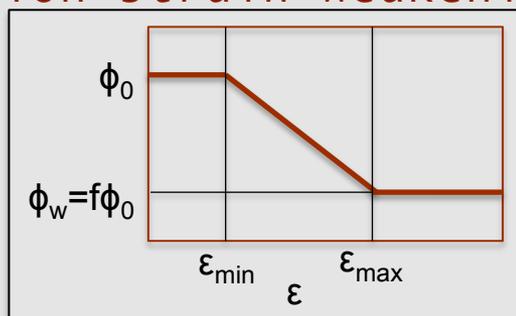
```
set Viscous flow law = dislocation
set Prefactors for dislocation creep = 5e-5,
    5e-15, 5e-15, 5e-15, 5e-18, 5e-18
set Stress exponents for dislocation creep = 1
set Activation energies for dislocation creep = 0
set Activation volumes for dislocation creep = 0

set Angles of internal friction = 0, 36, 36, 16, 0, 1e18
set Cohesions = 1e18, 30, 30, 30, 1e18, 1e18

set Strain weakening mechanism = total strain
set Start plasticity strain weakening intervals = 0.5
set End plasticity strain weakening intervals = 1
set Cohesion strain weakening factors = 1
set Friction strain weakening factors = 1, 0.861,
    0.861, 0.875, 1, 1
```

Manipulate
dislocation
parameters
to provide
constant
viscosities.

end
end



Use the total strain (strain rate integrated over time)
to weaken the internal friction angle on the strain
interval [0.5,1.0].

Parameter file: Mesh refinement

subsection Mesh refinement

```
set Initial adaptive refinement = 2
set Initial global refinement = 0
set Minimum refinement level = 0
set Normalize individual refinement criteria = true
set Refinement criteria merge operation = plus
set Coarsening fraction = 0.10
set Refinement fraction = 0.9
set Run postprocessors on initial refinement = false
set Skip solvers on initial refinement = true

set Skip setup initial conditions on initial refinement = \
  false

set Strategy = minimum \
  refinement function, density, maximum refinement function
set Time steps between mesh refinement = 2
```

2 levels of AMR

Coarsen as well
as refine

Save time by not solving on the coarse grid,

but do setup initial conditions, because
refinement is based on density(T, c_i).



Parameter file: Mesh refinement

```
subsection Minimum refinement function
  set Coordinate system = cartesian
  set Variable names    = x,z,t
  set Function constants = bound=0.0025, crust=0.037, \
                          block=0.34, block_r=0.36, \
                          cm=0.01, hour=3600
  set Function expression = \
    if((z<=crust & x>0.08 & x<=block-3*cm/hour*t) | \
      (x>block-3.5*cm/hour*t & x<block_r-2*cm/hour*t) | \
      z<=bound,2, \
      if(z<=crust&x<=0.08,1,0))
```

Time-dependent function that follows the boundary layer along the mobile wall.

end

```
subsection Maximum refinement function
  set Coordinate system = cartesian
  set Variable names    = x,z,t
  set Function constants = crust=0.037
  set Function expression = if(z>crust&x<=0.08,0, \
                              if(z<=crust&x<=0.08,1,2))
```

Save time by setting a lower max resolution in undeforming sand.

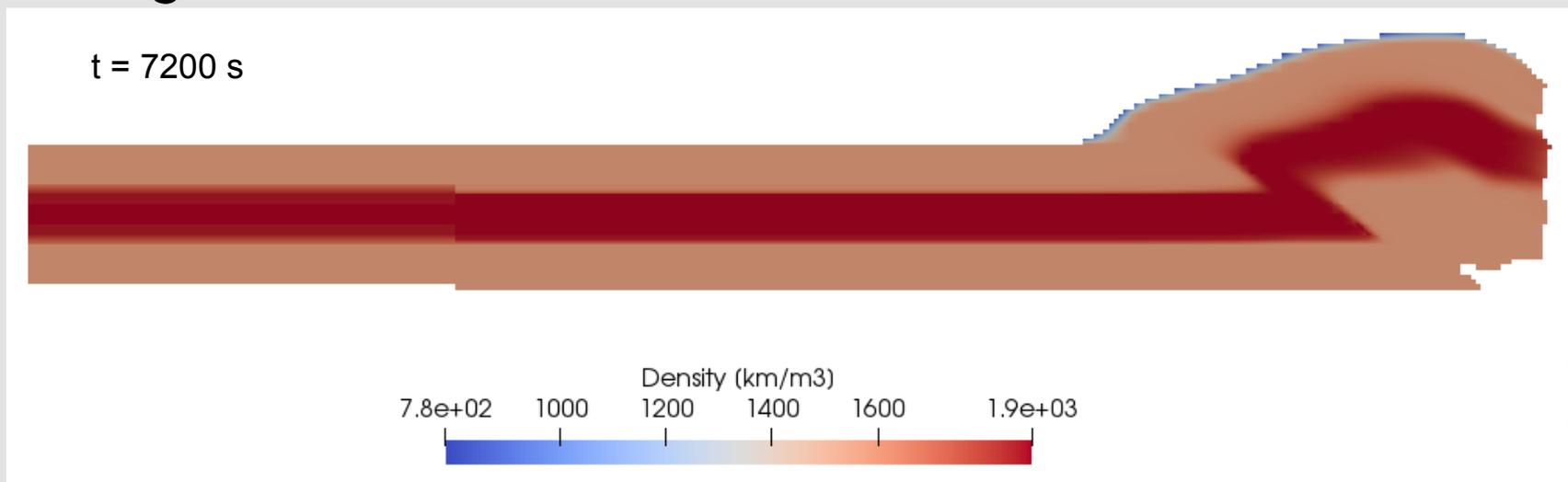
end

end

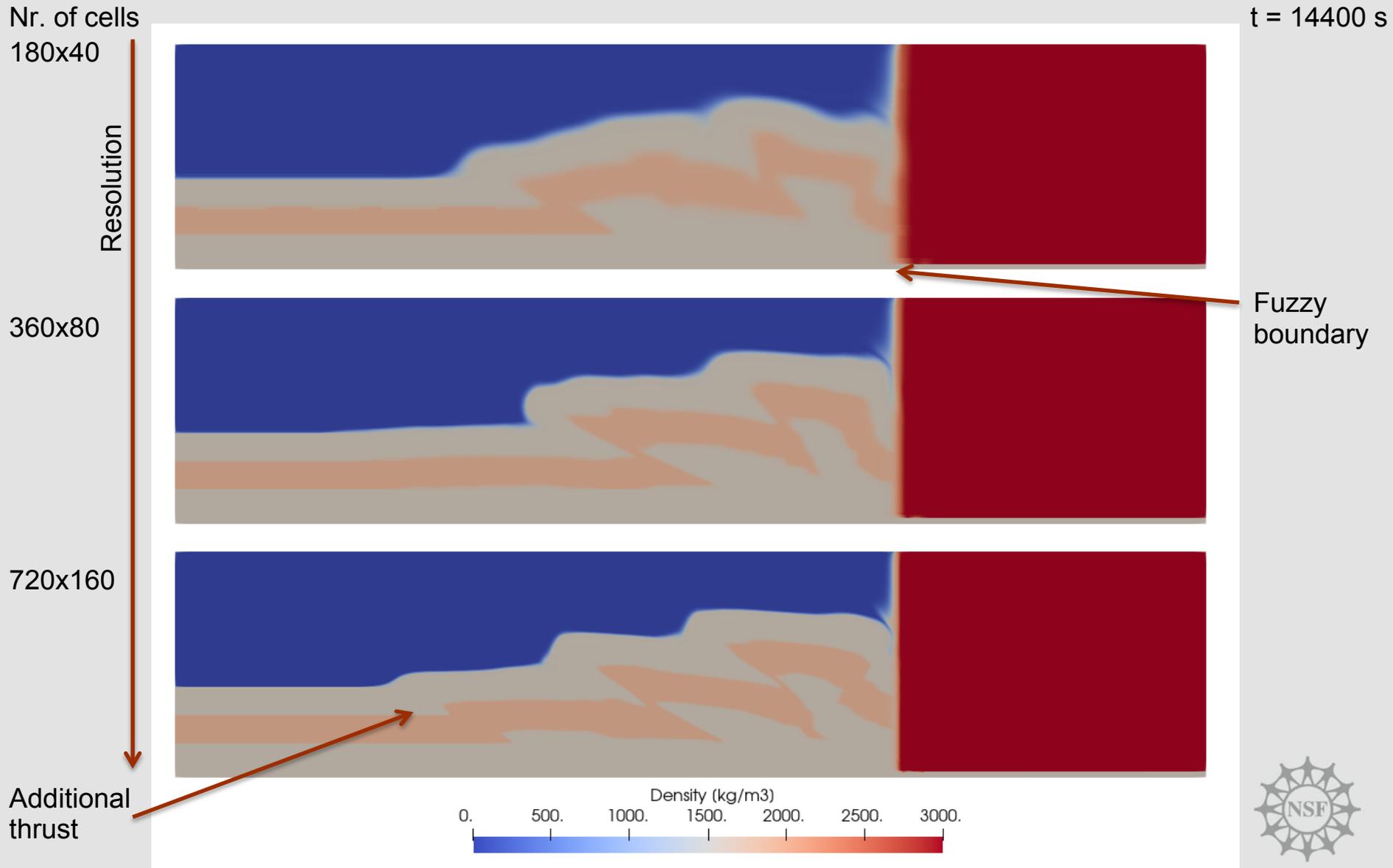


Visualizing the results

1. Start ParaView by typing `paraview &` in the terminal
2. Load `solution.pvd`
3. Let's cut off the sticky air and mobile wall block:
 1. Use the *Calculator* to sum *qsand* and *csand*
 2. Use the *Threshold* filter with 0.5 minimum on the result
 3. Select the *density* field to display
4. Press play!
5. Make snapshots at 2 and 6 cm compression ($t = 2880$ and 8640 s)
6. Investigate strain and strain rate. Are all faults still active?

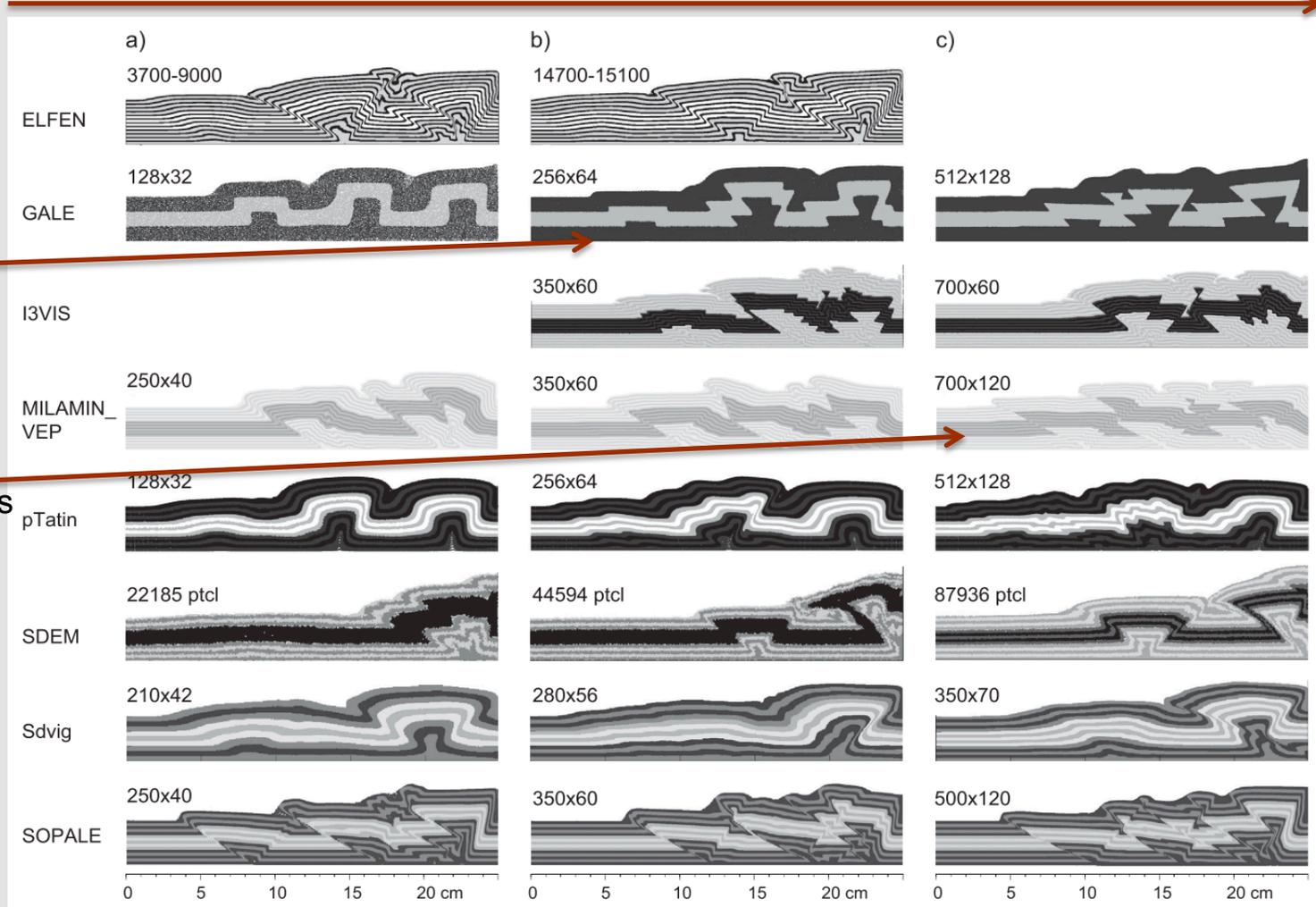


Sensitivity analysis: Resolution



Comparing to other codes: Resolution

Resolution



Different shear zone location

More shear zones

Different shear zone width



Comparing to other codes: Evolution

Two modes of deformation:

1. Series of thrust popups
2. Mainly forward dipping thrusts

Converge to critical taper

Other variations in:

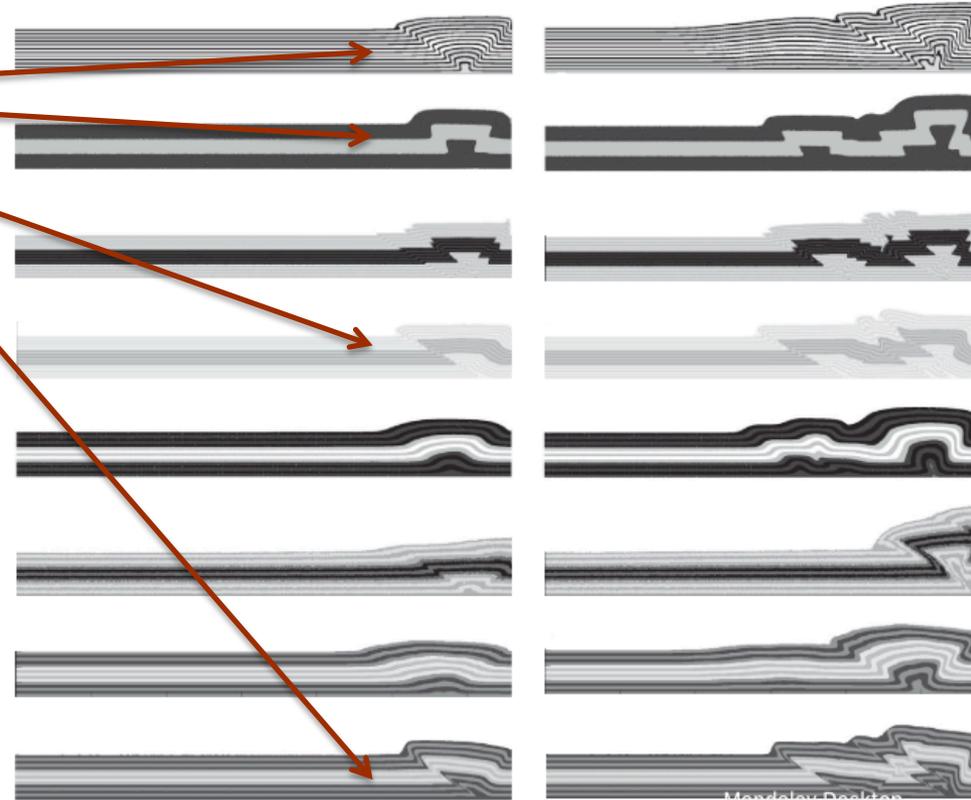
1. rate of thrust formation
2. nr of thrusts
3. dip angle
4. thrust spacing

Differences due to:

1. numerical solution techniques
2. resolution
3. **boundary friction implementation**
4. remeshing methods

b) 2 cm

c) 6 cm



numerical

analog

Parameters

- ✓ Grid resolution: keep uniform, higher resolution throughout the sand layer
- ✓ Particles instead of fields: less diffusion of the boundary layer
- ✓ Time step size: the official benchmark uses $dt = 3.6$ s
- ✓ Strain-weakening: only the plastic strain
- ✓ Higher viscosity ratio
- ✓ 3D



Parameters

- ✓ Grid resolution: keep uniform, higher resolution throughout the sand layer
- ✓ Particles instead of fields: less diffusion of the boundary layer
- ✓ Time step size: the official benchmark uses $dt = 3.6$ s
- ✓ Strain-weakening: only the plastic strain
- ✓ Higher viscosity ratio
- ✓ 3D

Try to change the material model parameters to only use plastic strain instead of the total strain.

Have a look at the manual p. 467 for the parameter options.



Parameters

- ✓ Grid resolution: keep uniform, higher resolution throughout the sand layer
- ✓ Particles instead of fields: less diffusion of the boundary layer
- ✓ Time step size: the official benchmark uses $dt = 3.6$ s

Only use plastic strain:

✓ Strain-weaken

✓ Higher viscos

✓ 3D

```
subsection Compositional fields
  set Number of fields           = 5
  set Names of fields            = qsand, csand, bound, block, \
                                total_strain
end
subsection Material model
  subsection Visco Plastic
    set Strain weakening mechanism = total strain
```



```
subsection Compositional fields
  set Compositional field methods = particles
  set Compositional field methods = particles, particles, \
    particles, particles, \
    particles
  set Mapped particle properties = qsand:initial qsand,csand:initial csand, \
    bound:initial bound, block:initial block, \
    total_strain:total_strain
end

subsection Postprocess
  subsection Particles
    set Number of particles = 1e6
    set Integration scheme = rk4
    set Particle generator name = random uniform
    set List of particle properties = composition, initial composition, \
      viscoplastic strain invariants
  set Maximum particles per cell = 200
  set Minimum particles per cell = 195
  set Interpolation scheme = nearest neighbor
  set Allow cells without particles = true
  set Load balancing strategy = remove and add particles
  set Update ghost particles = true
  set Time between data output = 144
end
end
```

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- Example: (Bending Beam)
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- **Example: Subduction**

Slides:

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Questions:

post in Zoom chat 😊

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Example: Prescribed subduction

Instructions:

1. Open a terminal and cd to the tutorial directory:

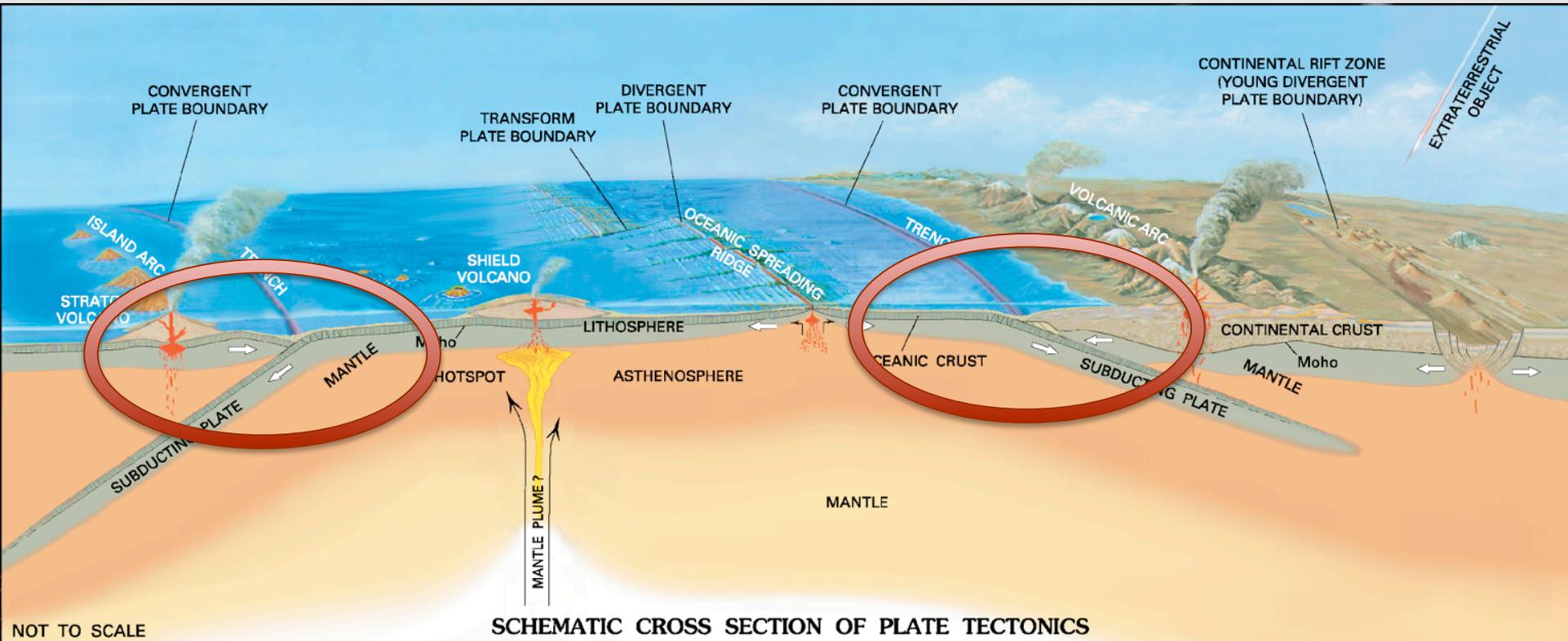
```
$ cd ~/aspect-tutorials/2020-tectonics-  
modeling-tutorial/session-3/
```

2. Run the model:

```
$ mpirun -np 2 ~/aspect/aspect-release  
prescribed_subduction.prm
```



Convergent settings



At convergent boundaries, plates can subduct underneath the overlying plate. This can be accompanied by mountain building, volcanism, earthquakes, fluid release into the overlying mantle, mantle melting, metamorphism, exhumation, phase changes...

Minimum requirements:

1. A weak zone that decouples the subducting plate from the overriding plate
 2. A weak layer (e.g. crust) that decouples the subducting plate from the surface and allows it to go down
 3. Something to initiate subduction, i.e. a negatively buoyant slab tip or prescribed plate motions or far-field forces
- Construct simple model of oceanic-oceanic plate subduction



Be aware of...

- ✦ Diffusion of the weak zone
- ✦ Dependency of results on mesh element aspect ratio and resolution in the weak zone
- ✦ Dependency on averaging methods of the compositional contributions to viscosity
- ✦ Shape (e.g. round vs. angular) and thickness of the weak zone can affect model evolution



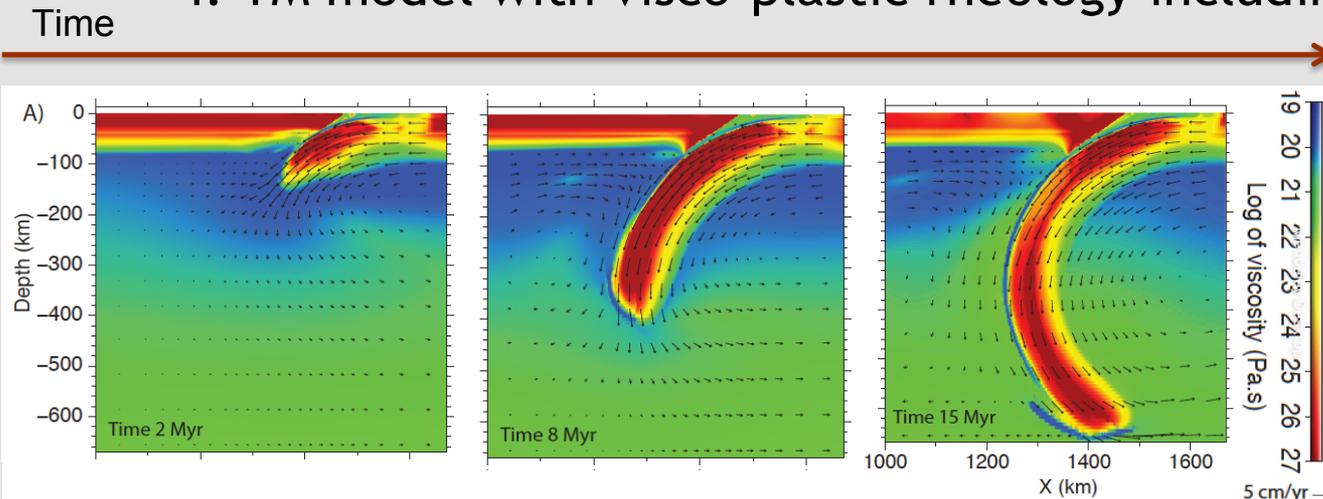
Based on the benchmark effort of Quinquis (2014):

- 7 numerical codes
- 4 experimental setups:
 1. Linear viscous rheology
 2. Linear viscous rheology with temperature advection
 3. Thermo-mechanical (TM) model with simplified visco-plastic rheology
 4. TM model with visco-plastic rheology including strain weakening



Based on the benchmark effort of Quinquis (2014):

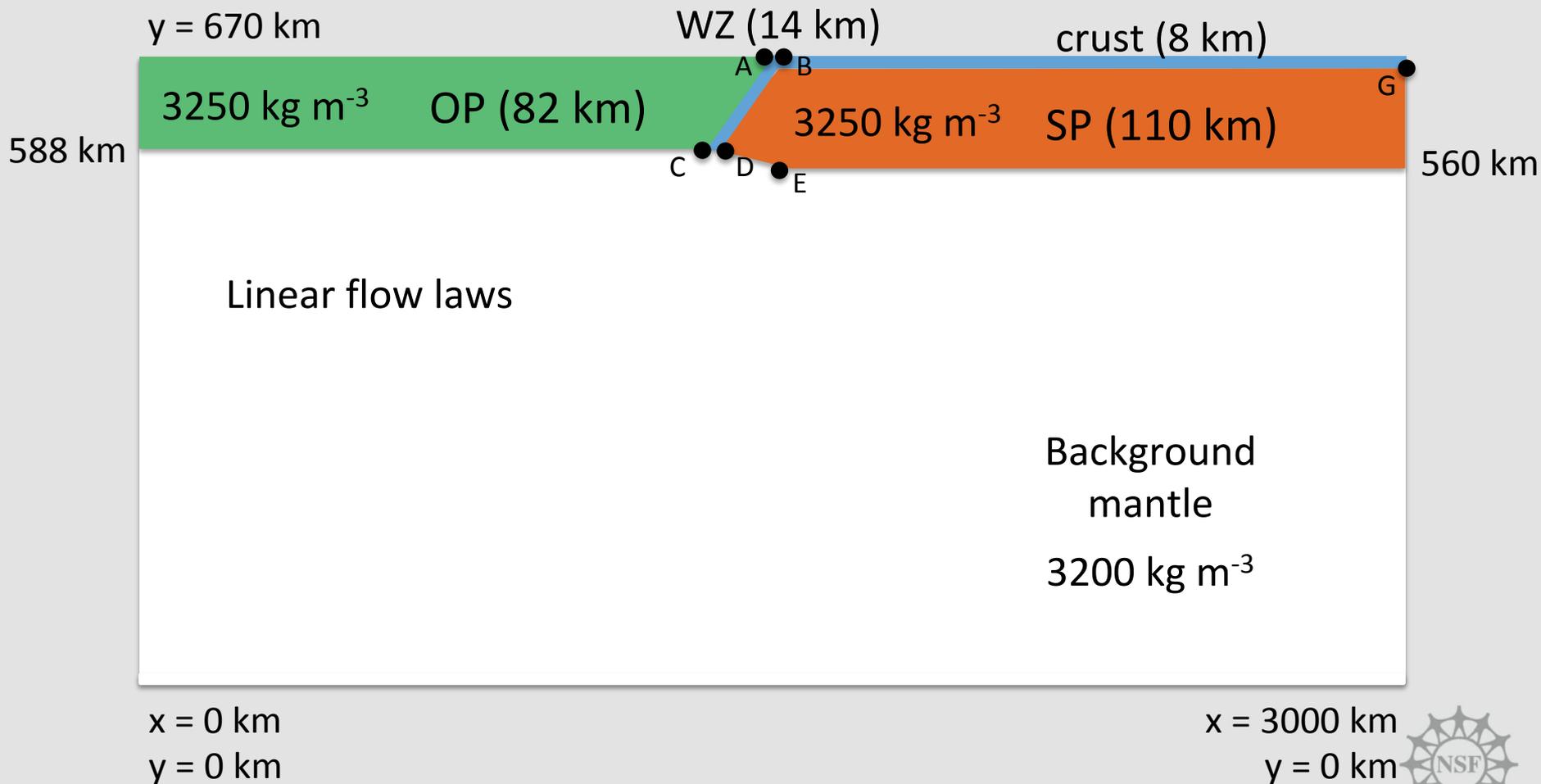
- 7 numerical codes
- 4 experimental setups:
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 2. Linear viscous rheology with temperature advection
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Case 4

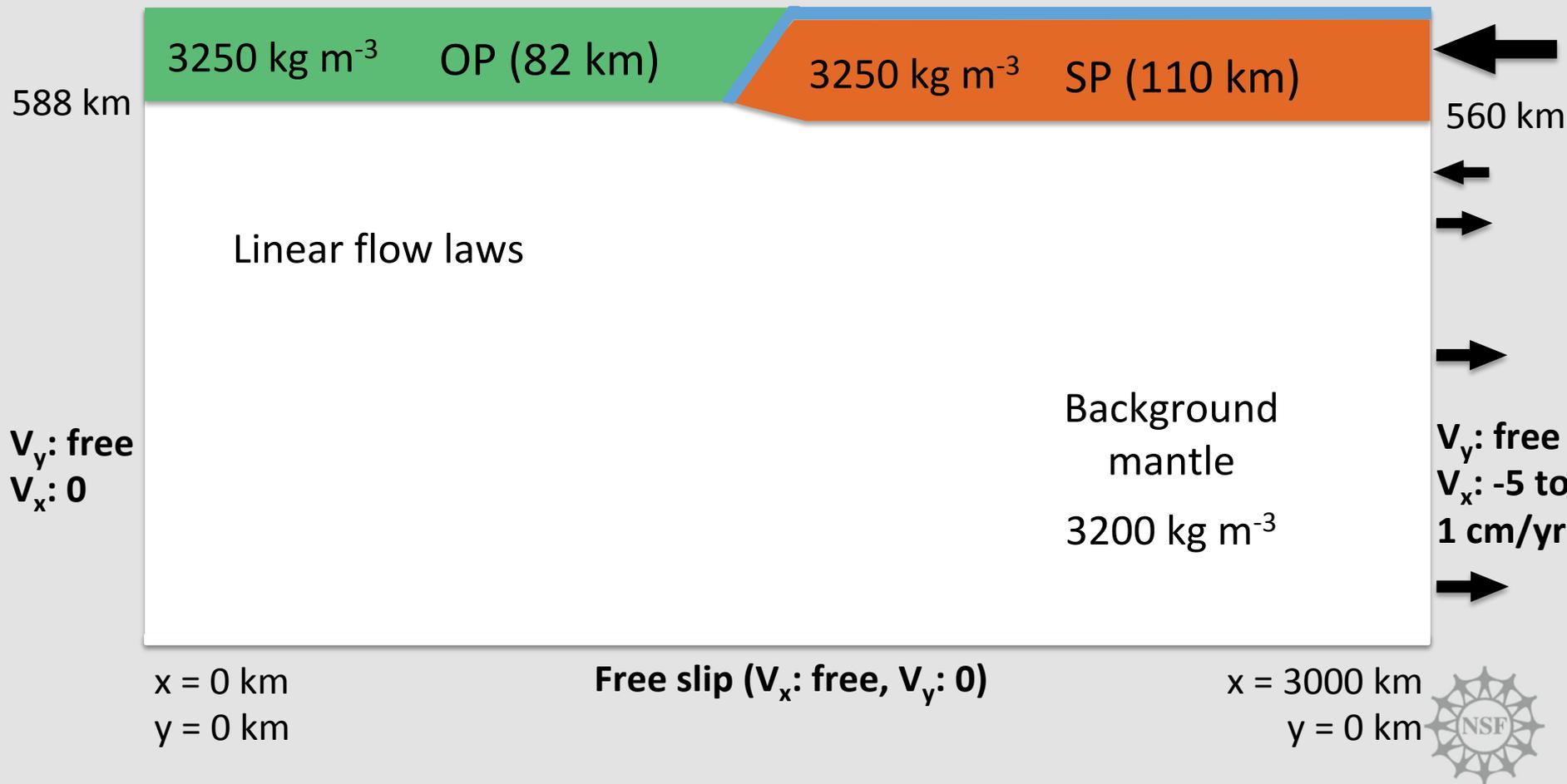


Initial composition & material properties



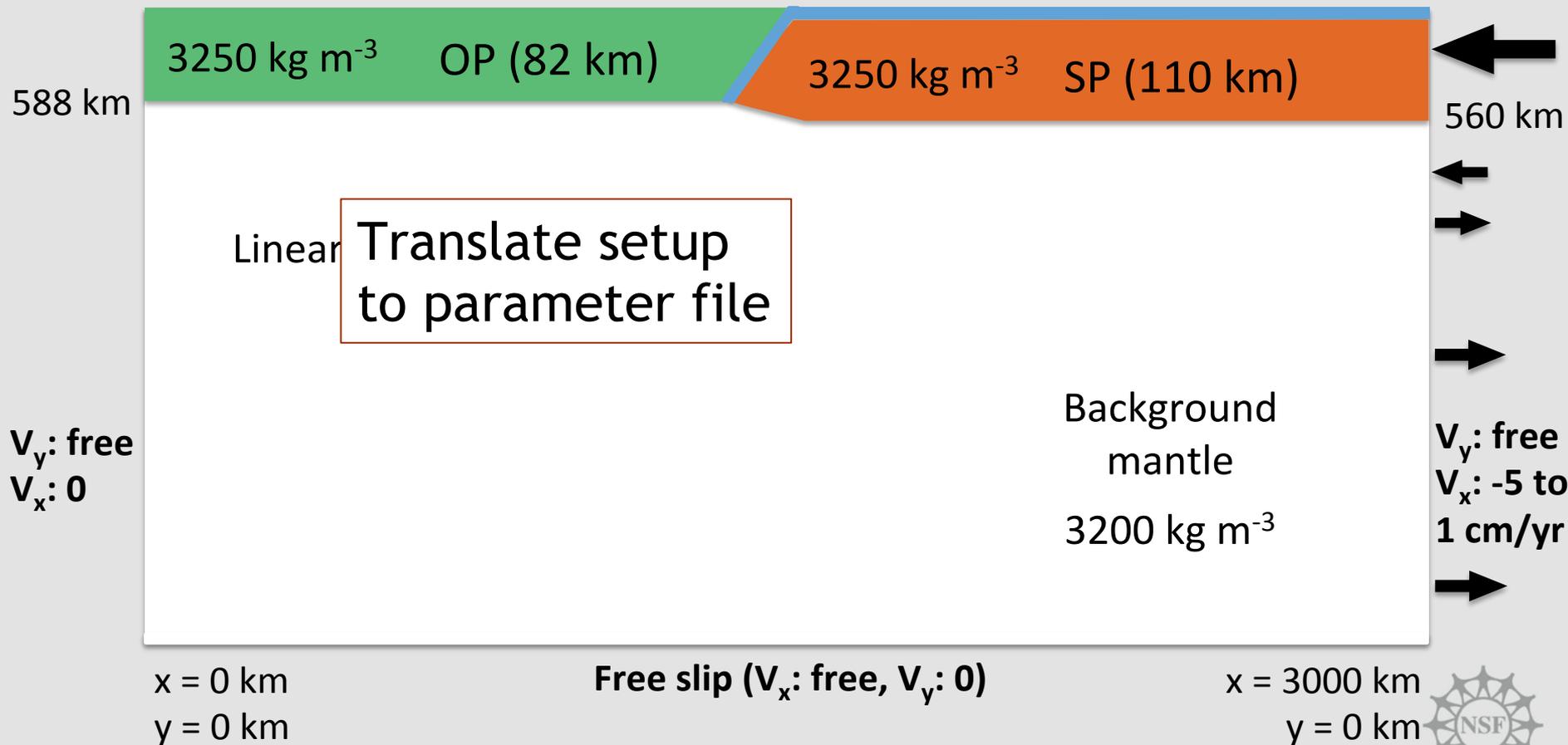
Velocity Boundary Conditions

$y = 670 \text{ km}$ Free slip ($V_y = 0, V_x = \text{free}$)



Velocity Boundary Conditions

$y = 670 \text{ km}$ Free slip ($V_y = 0, V_x = \text{free}$)



Parameter file: Global parameters

Open `prescribed_subduction.prm` with `vi` or your editor of choice

```
$vi Case1.prm
```

which is an adapted version of the actual Quinquis benchmark.

```
set Dimension = 2
set Start time = 0
set End time = 15e6 [years]
set CFL number = 0.01
set Use years in output instead of seconds = true
set Output directory = \
prescribed_subduction/
set Adiabatic surface temperature = 0
```

Temperature plays no role in this setup.

Parameter file: Solver settings

```
set Nonlinear solver scheme = single Advection,  
                             single Stokes  
subsection Solver parameters  
  subsection Stokes solver parameters  
    set Linear solver tolerance           = 1e-6  
    set Number of cheap Stokes solver steps = 200  
  end  
end
```

Linear viscosities,
so no need for an
iterative solver scheme

Cheap Stokes preconditioner



```
subsection Discretization
  set Composition polynomial degree           = 2
  set Temperature polynomial degree          = 1
  set Stokes velocity polynomial degree      = 2
  set Use locally conservative discretization = false
set Use discontinuous composition discretization = true

subsection Stabilization parameters
  set Use limiter for discontinuous composition solution
= true
  set Global composition maximum             = 1, 1, 1, 1, 100
  set Global composition minimum             = 0, 0, 0, 0, 0
  set Stabilization method                   = entropy viscosity
end
end
```

Discontinuous Galerkin for compositional fields → explain

Stabilization of advection



Parameter file: Geometry

```
subsection Geometry model  
  set Model name = box
```

```
  subsection Box  
    set X extent      = 3000e3  
    set Y extent      = 670e3  
    set X repetitions = 4
```

2D box of 3000x670 km

Divide the coarse grid to get better aspect ratio of mesh cells

```
  end  
end
```



Parameter file: Composition

```
subsection Compositional fields
  set Number of fields      = 3
  set Names of fields      = OP, ML_SP, crust_SP
end
```

Sublithospheric mantle is background

```
subsection Initial composition model
  set List of model names  = function
  subsection Function
    set Function constants = Ax=1451200.0, Az=670000.0, ...
    set Function expression = \
if(z>=Cz&z>=((Az-Cz)/(Ax-Cx)*(x-Cx)+Cz),1,0); \
if((x>=Ex&z>=Ez&z<Gz)| \
  (x<Ex&z<=((Bz-Dz)/(Bx-Dx)*(x-Dx)+Dz)
  &z<Gz&z>=((Ez-Dz)/(Ex-Dx)*(x-Dx)+Dz)),1,0); \
if(z>=Cz&z>((Bz-Dz)/(Bx-Dx)*(x-Dx)+Dz)&
  z<((Az-Cz)/(Ax-Cx)*(x-Cx)+Cz)| \
  z>=Gz&z<=((Bz-Dz)/(Bx-Dx)*(x-Dx)+Dz),1,0)
  set Variable names      = x,z
end
end
```



Parameter file: Composition

```
subsection Boundary composition model
  set Fixed composition boundary indicators = right
  set List of model names                = initial composition
end
```

Prescribed inflow on the right,
so fix the composition that comes in



Parameter file: Temperature

```
subsection Initial temperature model
  set List of model names = function
  subsection Function
    set Function expression = 0
  end
end
subsection Boundary temperature model
  set Fixed temperature boundary indicators = bottom, top,
                                             right

  set List of model names = box
  subsection Box
    set Bottom temperature = 0
    set Left temperature   = 0
    set Right temperature  = 0
    set Top temperature    = 0
  end
end
```

Temperature plays no role,
but we should set boundary conditions for inflow boundaries.

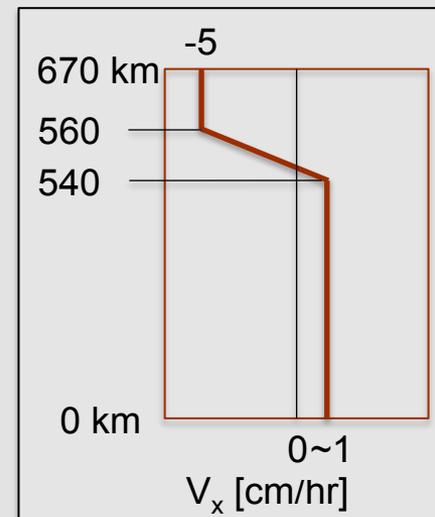


Parameter file: Velocity BC

```
subsection Boundary velocity model
  set Tangential velocity boundary indicators = left, bottom, top
  set Prescribed velocity boundary indicators = right x:function

subsection Function
  set Function constants = cm=100.
  set Function expression = if(z<540000.0, (600.0/550.0)/cm, \
    if(z>560000.0, -5.0/cm, \
      ((((-600.0/550.0)-5.0)/-20.0)*
        ((z/1000.0)-560.0)+5.0)*
        (-1.0/cm))); \
    0
  set Variable names = x,z
end
end
```

Prescribe the plate inflow (horizontal component only) and a gradual transition to a compensating outflow of mantle material.



Parameter file: Material parameters

```
subsection Material model  
  set Model name = multicomponent
```

```
  subsection Multicomponent  
    set Reference temperature      = 0.0  
    set Viscosity averaging scheme = maximum composition  
    # Fields: background, OP, ML SP, crust SP  
    set Viscosities                = 1e20, 1e23, 1e23, 1e20  
    set Densities                  = 3200, 3250, 3250, 3250  
    set Thermal conductivities     = 1  
  end
```

Take the max composition to compute viscosity to counteract diffusion.

Only density and viscosity vary between all compositions.

```
end
```

```
subsection Formulation  
  set Formulation = Boussinesq approximation  
end
```



Parameter file: Mesh refinement

```
subsection Mesh refinement
  set Initial adaptive refinement           = 2
  set Initial global refinement           = 4
  set Minimum refinement level           = 2
  set Normalize individual refinement criteria = true
  set Refinement criteria merge operation = plus
  set Coarsening fraction                 = 0.10
  set Refinement fraction                 = 0.9
  set Strategy                           = minimum refinement
                                          function, viscosity, composition
  set Time steps between mesh refinement = 10

subsection Minimum refinement function
  set Coordinate system = cartesian
  set Variable names = x,z,t
  set Function constants = vel=150e3, L=100e3, crust=10e3
  set Function expression = if(x>=1350e3&670e3-z<crust,6,
                              if(670e3-z<L,5,if(670e3-z<vel,4,1)))
end
end
```

Limit coarsening to level 2

Static and dynamic
strategies

Make sure the crustal layer is
always well resolved.



Parameter file: Postprocessing

```
subsection Postprocess
  set List of postprocessors = visualization,
                             velocity statistics
                             Track the RMS velocity

  subsection Visualization
    set List of output variables = density, viscosity,
                                  strain rate,
                                  error indicator

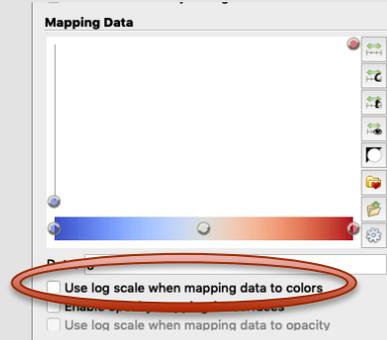
    set Time between graphical output = 5e5
  end
end

Output graphics every 0.5 My
(since set Use years in output
instead of seconds = true)
```

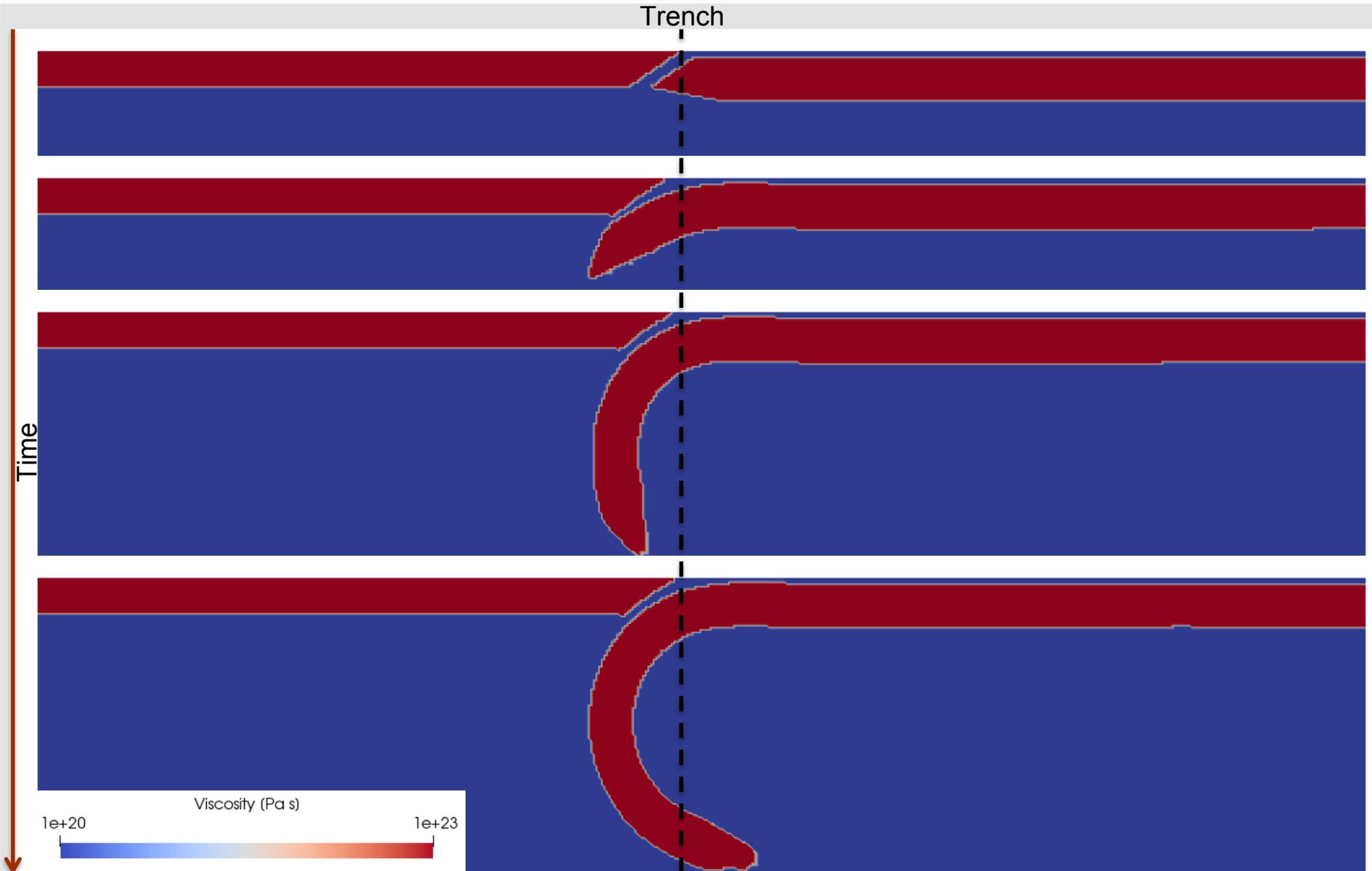


Visualizing the results

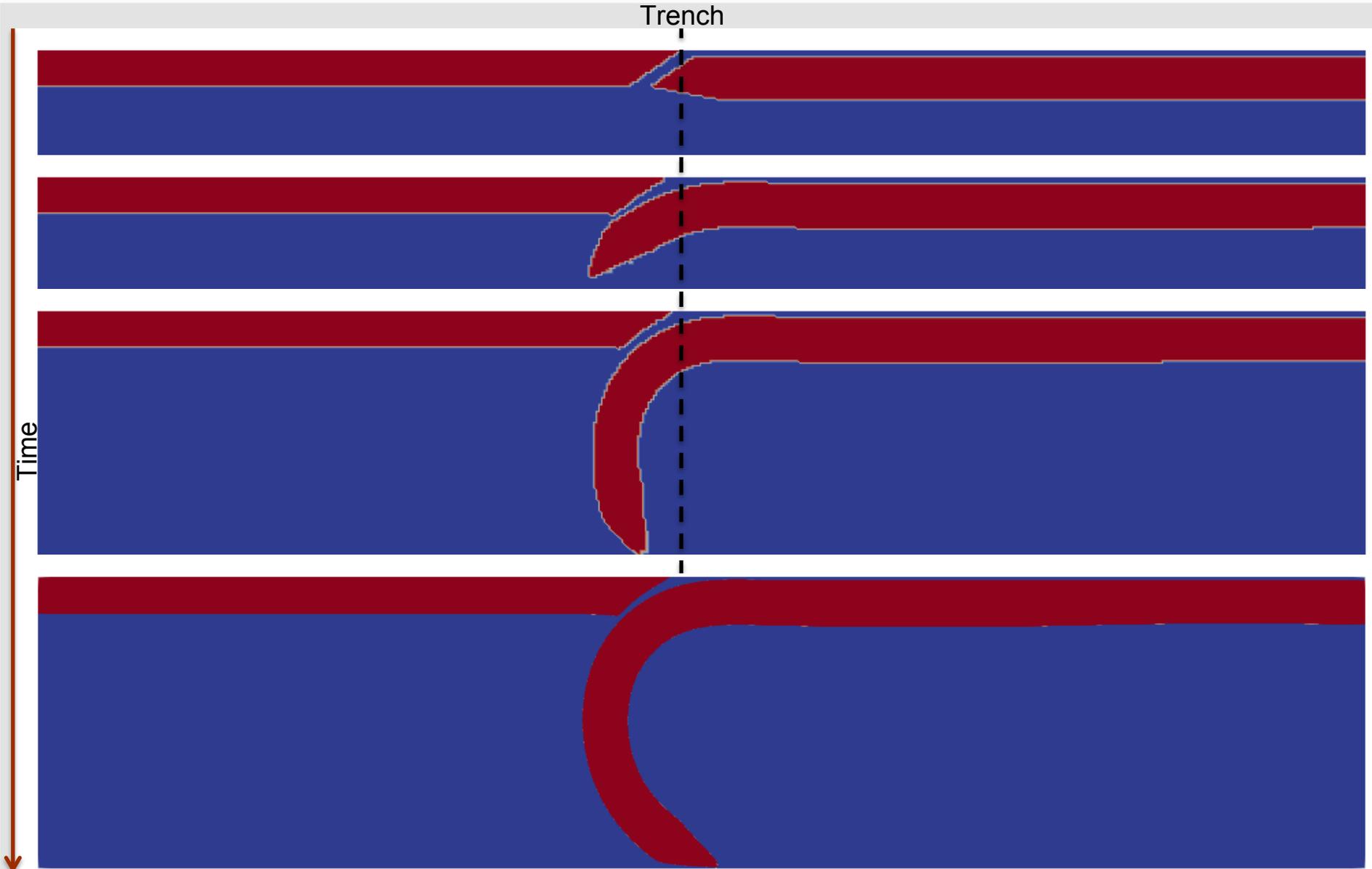
1. Start ParaView by typing `paraview &` in the terminal
2. Load the solution.pvd file
3. Display the viscosity and set the colorbar to log scale:
 1. Click *Edit color map* 
 2. Select log scale
3. Press play!
4. What does the slab do? E.g. advance, retreat, slide along the 660...
5. Look at the strain rate, where is it highest?
6. Does the mesh refinement follow the slab?
7. Add velocity vectors:
 1. Click *Glyphs* 
 2. Set *Active Attributes* → *Vectors* to **velocity**
 3. Set *Scaling* → *Scale mode* to **vector** and press the reset button 
 4. How would the boundary conditions affect the flow field?



Visualizing the results



Visualizing the results



Plotting the statistics

1. In the terminal, go to the directory with the statistics file:

```
$ cd prescribed_subduction/
```

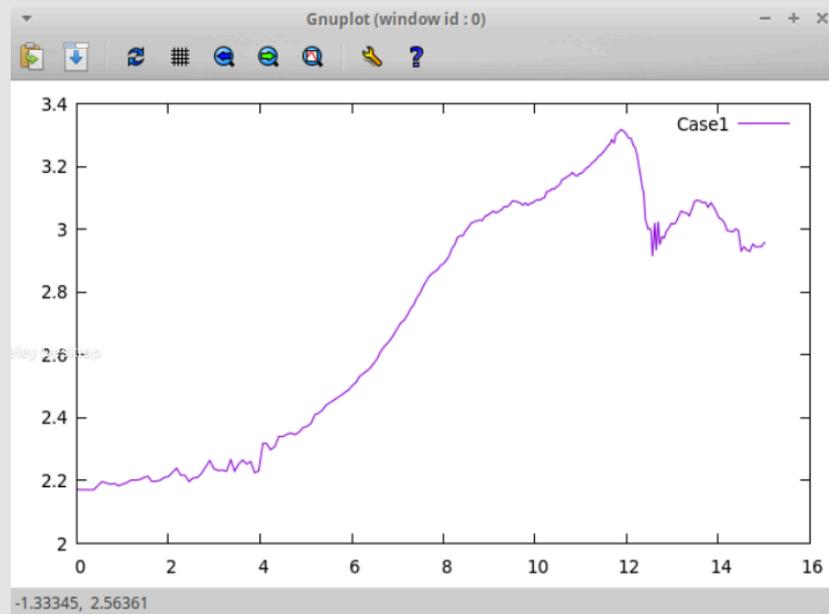
2. Start gnuplot:

```
$ gnuplot
```

3. Plot the root-mean-square velocity [cm/yr] over time [My]:

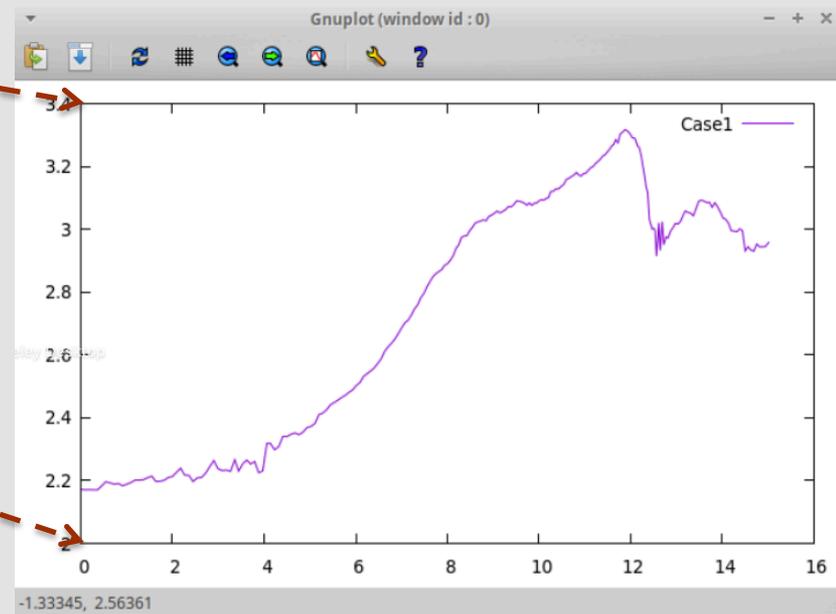
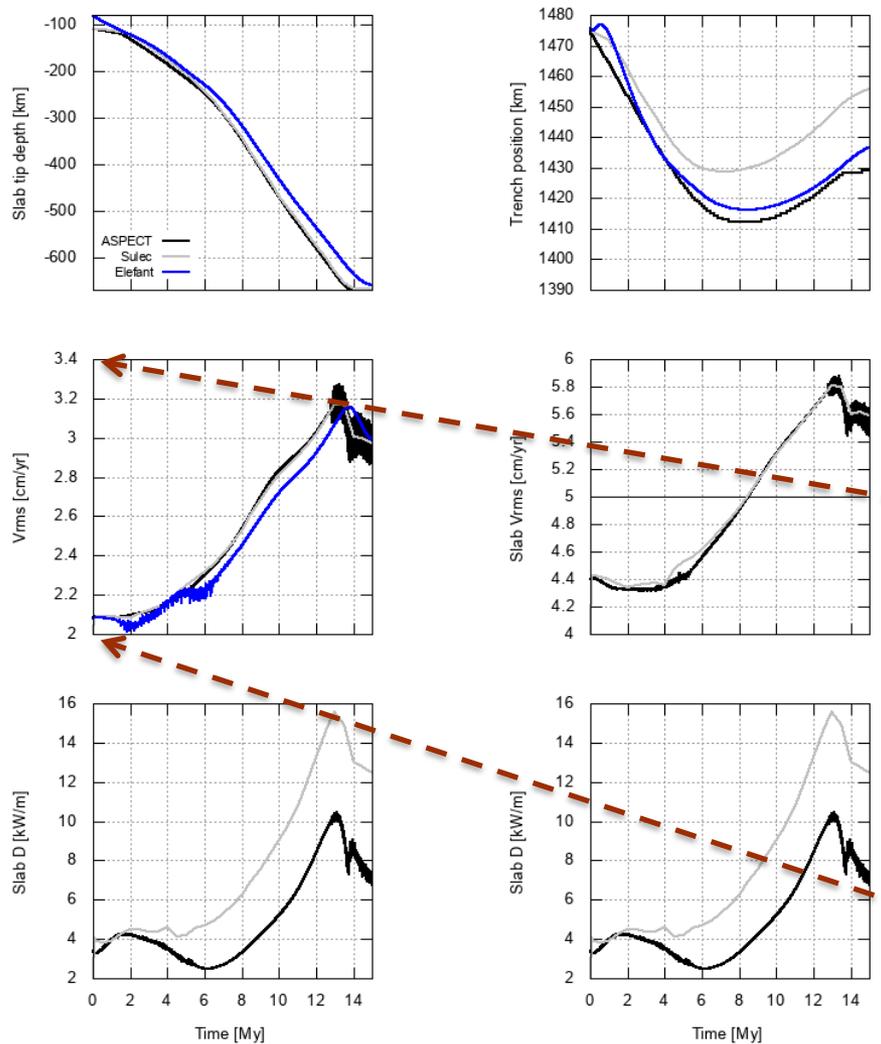
```
$ plot 'statistics' u ($2/1e6):($16*100) w l
```

4. Can you correlate the trends in the velocity with what you see in ParaView?



Comparing to other codes

High resolution results:



- ✓ Grid resolution
- ✓ Temperature advection and dependency (Case 2)
- ✓ Additional layering of the lithosphere
- ✓ Visco-plastic rheology (Case 3&4)
- ✓ Phase changes
- ✓ Free surface
- ✓ Self-consistent subduction
- ✓ 3D



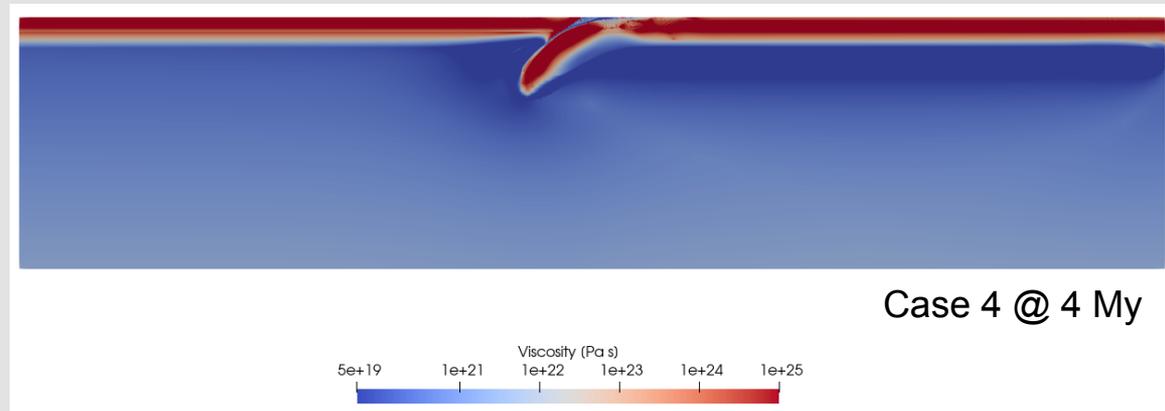
- ✓ Grid resolution
- ✓ Temperature advection and dependency (Case 2)
- ✓ Additional layering of the lithosphere
- ✓ Visco-plastic rheology (Case 3&4)
- ✓ Phase changes
- ✓ Free surface
- ✓ Self-consistent subduction
- ✓ 3D

*~70 publications with ASPECT:
<https://aspect.geodynamics.org/publications.html>*



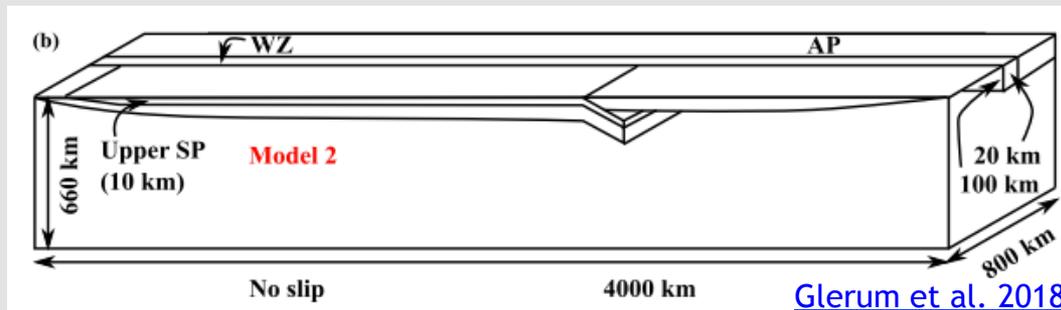
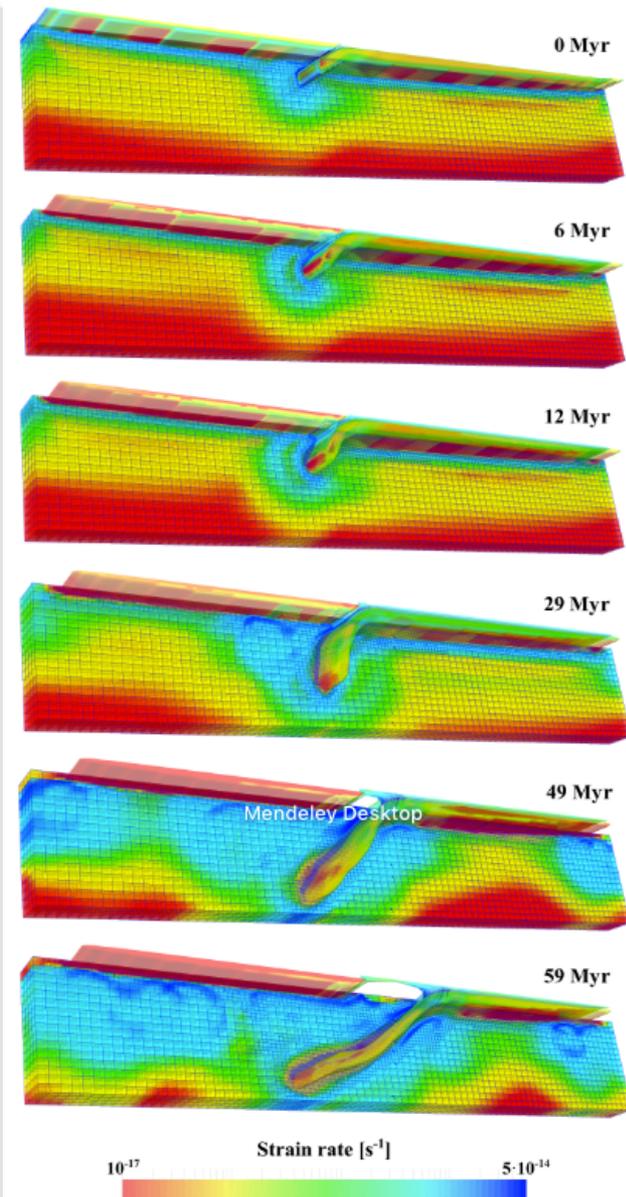
Model Extension

- ✓ Grid resolution
- ✓ Temperature advection and dependency (Case 2)
- ✓ Additional layering of the lithosphere
- ✓ Visco-plastic rheology (Case 3&4)



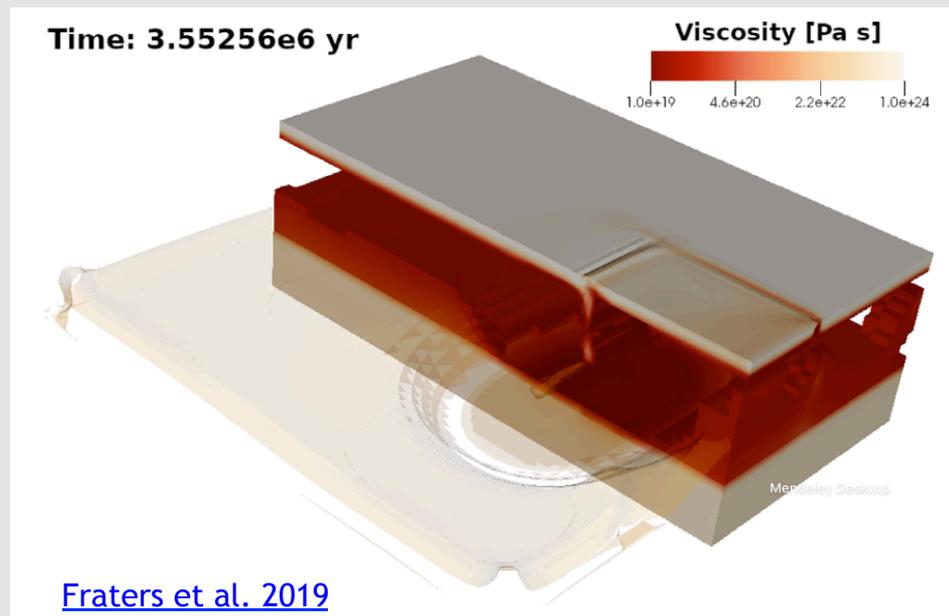
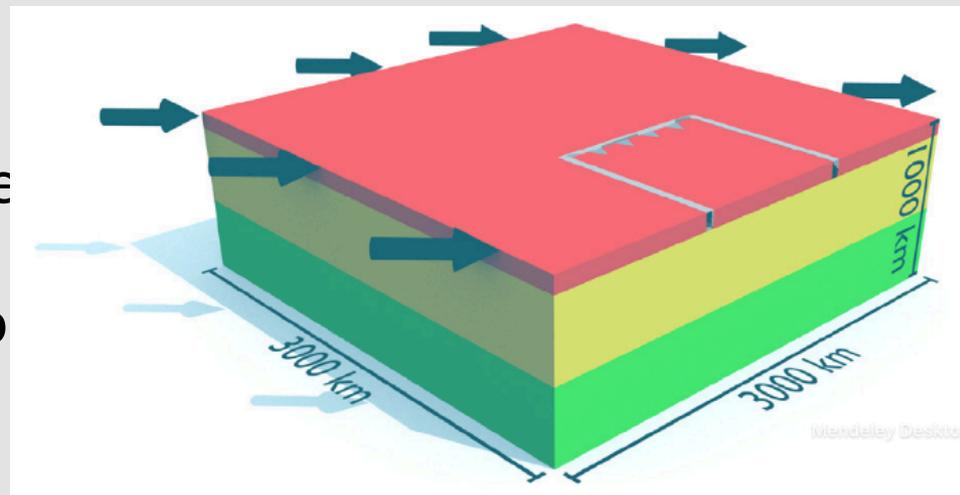
Model Extension

- ✓ Grid resolution
- ✓ Temperature advection and dependency
- ✓ Additional layering of the lithosphere
- ✓ Visco-plastic rheology
- ✓ Self-consistent subduction
- ✓ 3D



Model Extension

- ✓ Grid resolution
- ✓ Temperature advection and dependence
- ✓ Additional layering of the lithosphere
- ✓ Visco-plastic rheology
- ✓ Oblique subduction
- ✓ 3D



✓ Temperature advection and dependency (Case 2)

Try to add an initial temperature field consisting of:

1. A linear increase in the lithosphere from 293 K at the surface to 1600 K at the LAB.
2. A smaller increase (0.4 K/km) in the sublithospheric mantle.

Use the Function expression in line 90.



✓ Temperature advection and dependency (Case 2)

Try to add an initial temperature field, for example:

```
subsection Function
  set Function constants = Ts=473.25, Tm=1573.25, \
                        yl_OP=84e3, yl_SP=110e3, \
                        Dy=670e3
  set Function expression = if(x<1500e3, \
                              if(Dy-y<yl_OP, \
                                  Ts+(Tm-Ts)*((Dy-y)/yl_OP), \
                                  Tm+(Dy-yl_OP-y)/1000.*0.25), \
                              if(Dy-y<yl_SP, \
                                  Ts+(Tm-Ts)*((Dy-y)/yl_SP), \
                                  Tm+(Dy-yl_SP-y)/1000.*0.25)) \
  set Variable names = x, y, t
end
```



✓ Temperature advection and dependency (Case 2)

Try to add an initial temperature field, for example:

```
subsection Function
  set Function constants = Ts=473.25, Tm=1573.25, \
                        yl_OP=84e3, yl_SP=110e3, \
                        Dy=670e3
  set Function expression = if(x<1500e3, \
                              if(Dy-y<yl_OP, \
                                  Ts+(Tm-Ts)*((Dy-y)/yl_OP), \
                                  Tm+(Dy-yl_OP-y)/1000.*0.25), \
                              if(Dy-y<yl_SP, \
                                  Ts+(Tm-Ts)*((Dy-y)/yl_SP), \
                                  Tm+(Dy-yl_SP-y)/1000.*0.25)) \
  set Variable names = x, y, t
end
```

