

# Scientific Drivers for High-Resolution Non-Newtonian Subduction Modeling



Margarete A. Jadamec

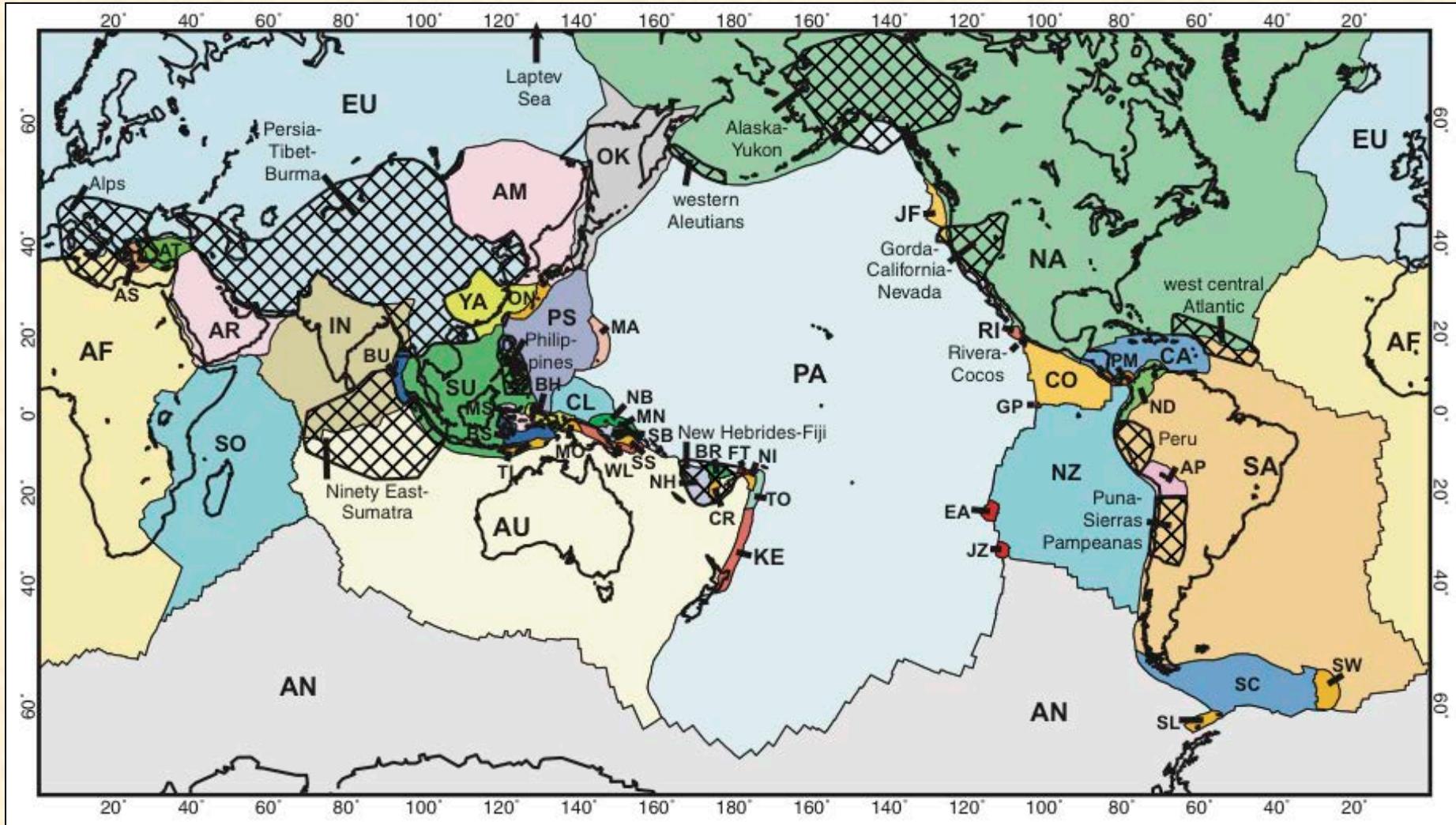
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Oliver Kreylos, Burak Yikilmaz, Karen Fischer  
Louis Moresi, Jerico Revote

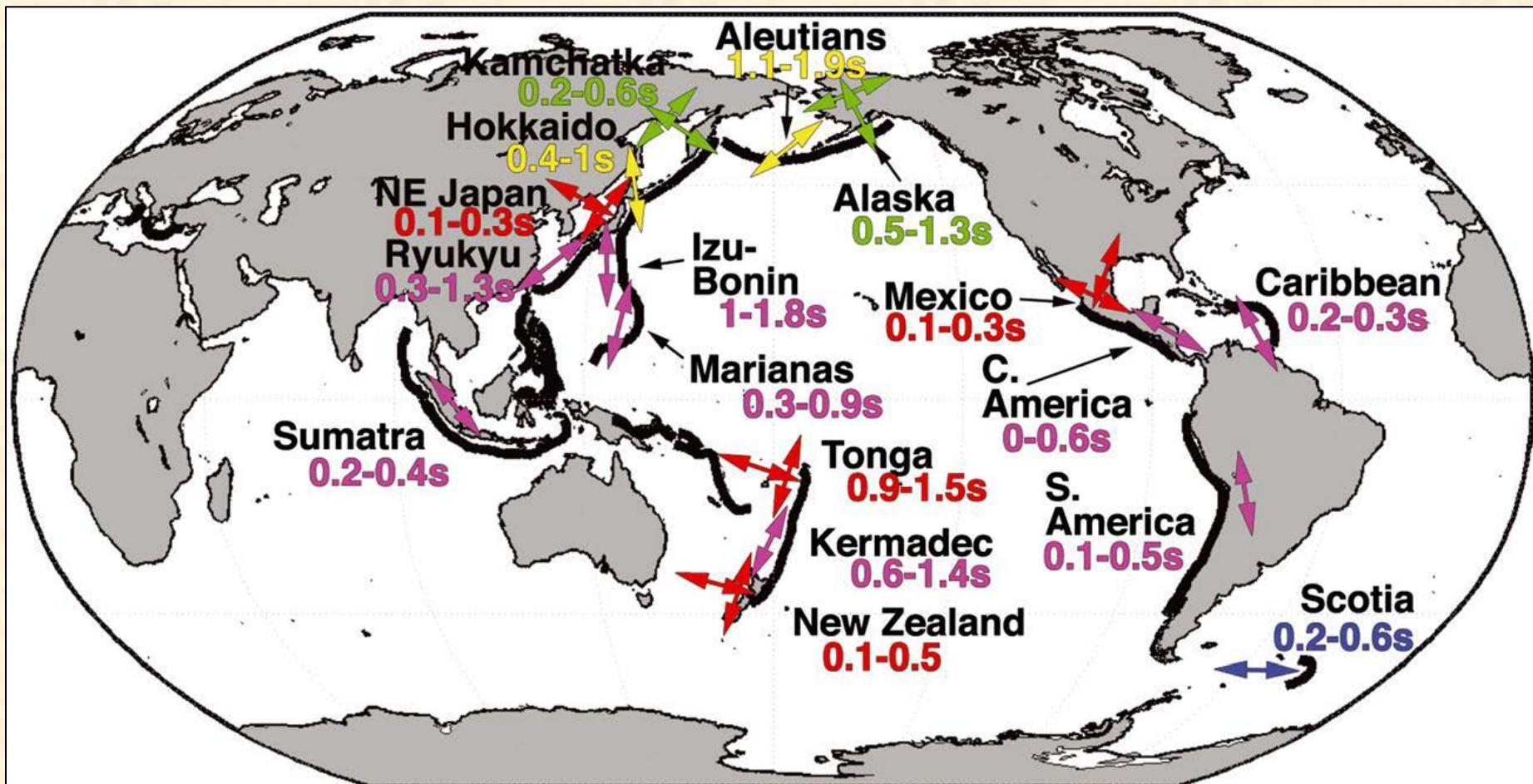
Resources: NSF, XSEDE, TACC, KeckCAVES

# Broad Zones of Lithosphere Deformation at Boundaries



Bird, G<sup>3</sup> 2003

# Broad Zones of Slab Driven Mantle Deformation

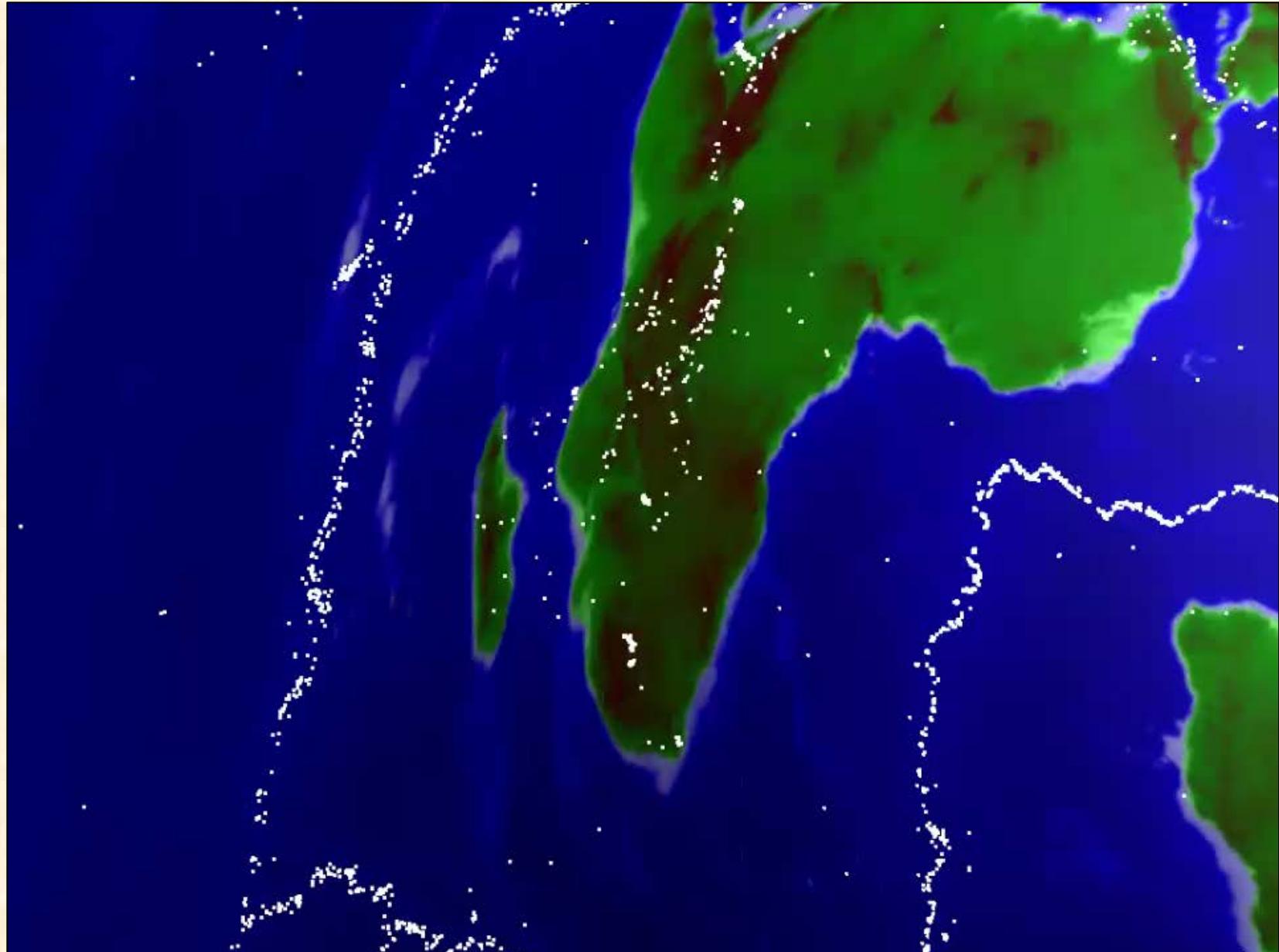


Summary of (Local S) Shear Wave Splitting in Mantle Wedge

Long and Wirth, JGR 2013

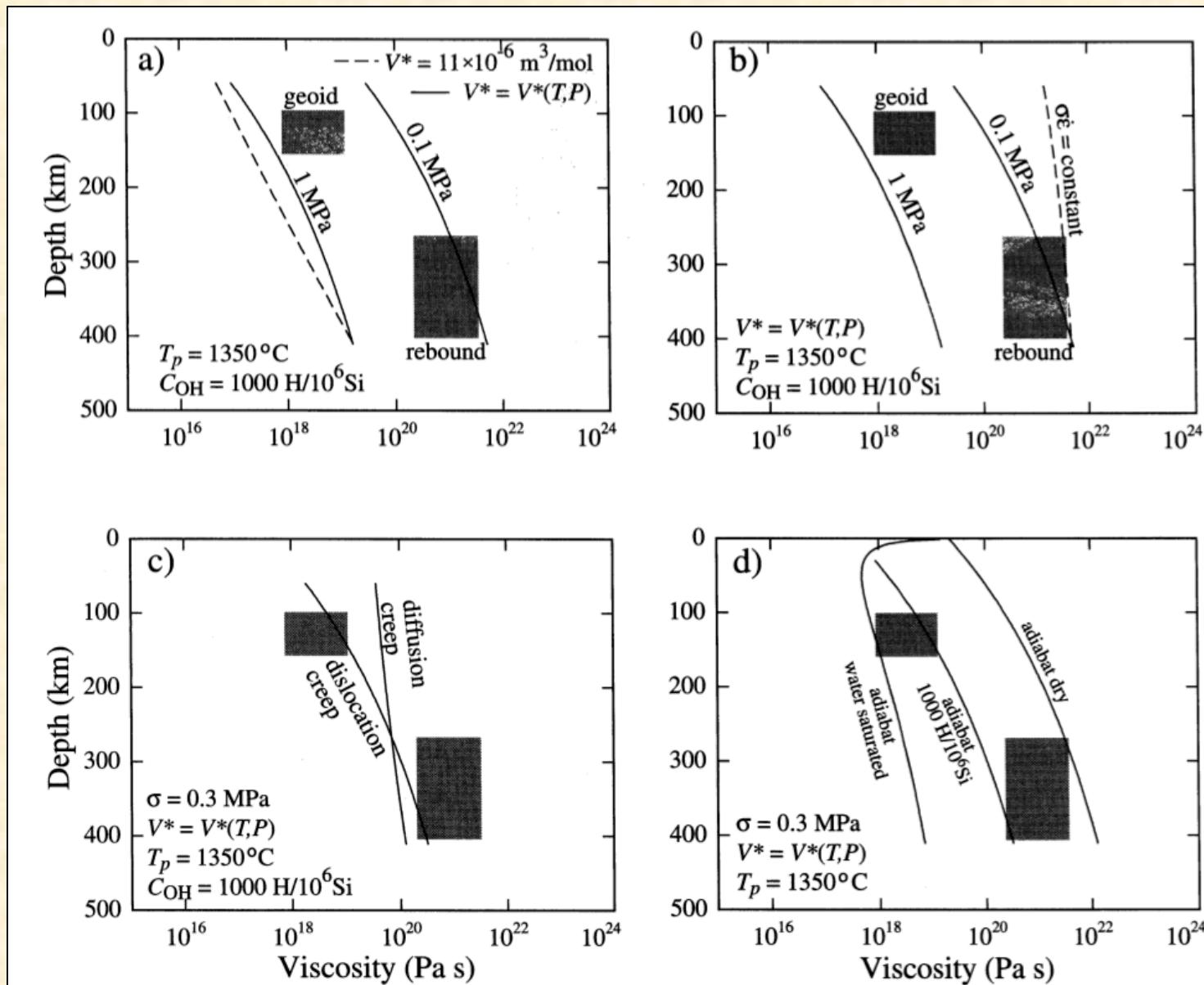
# Role of Slab Morphology in Driving Deformation

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Revote, Jadamec, and Moresi, 3DALIVE Demo, 2010 (Software from Kreylos et al., 2006)

# Role of Rheology in Modulating Plate Boundary Deformation



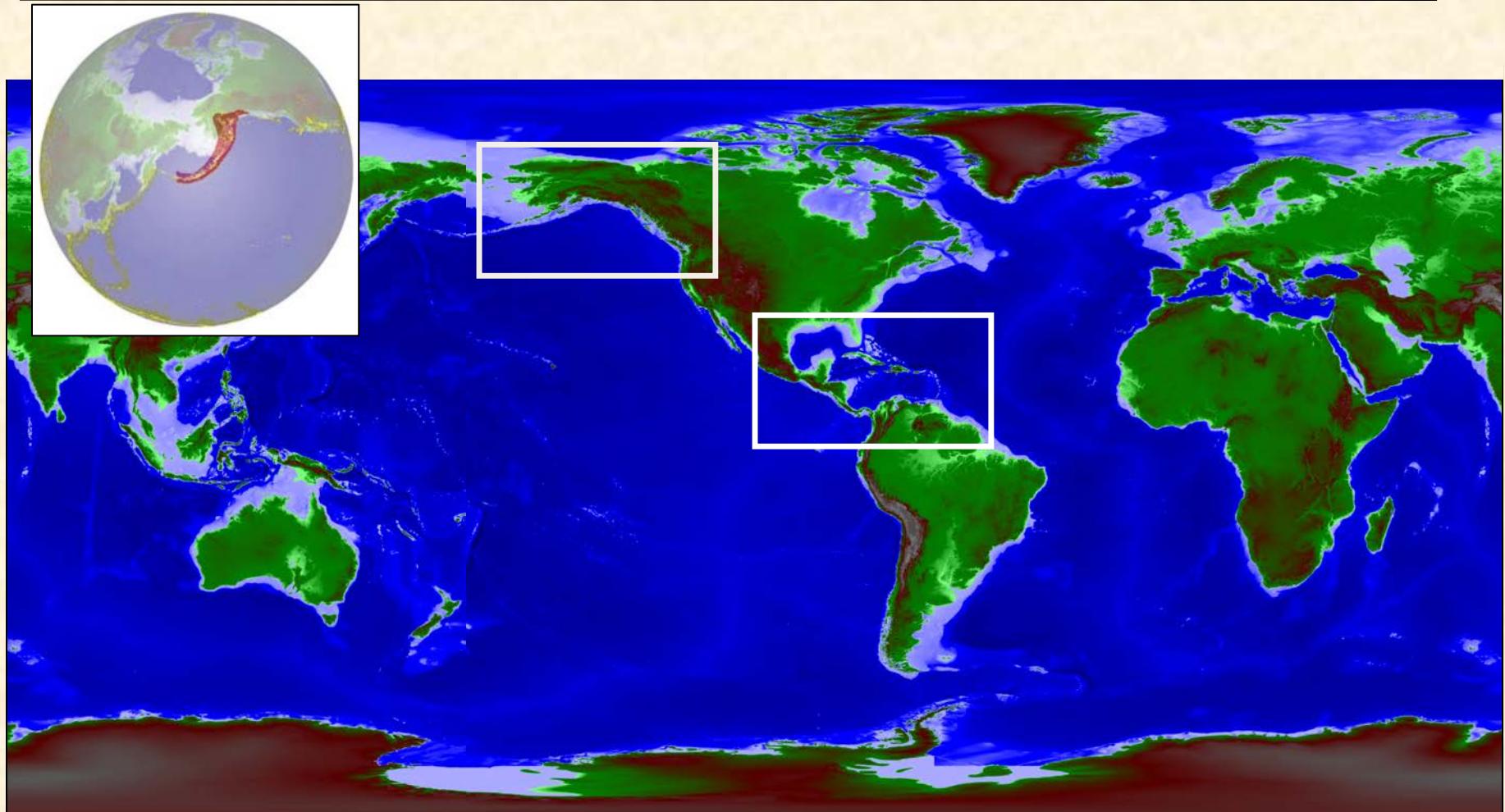
# Outline:

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- ① Intra-Continental Mountain Building
- ② Viscous (de)coupling of the Lithosphere to Mantle
  - Methods: High-resolution 3D Regional Modeling
  - Results: Predicted Plate Motion, Dynamic Topography
  - Results: Predicted Plate and Mantle Velocity
  - Conclusions & Looking Forward

# Regionally Based 3D Model to Elucidate Process

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# Regional Model Design: Constraints on Slab Geometry

## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →



## 3D Configuration

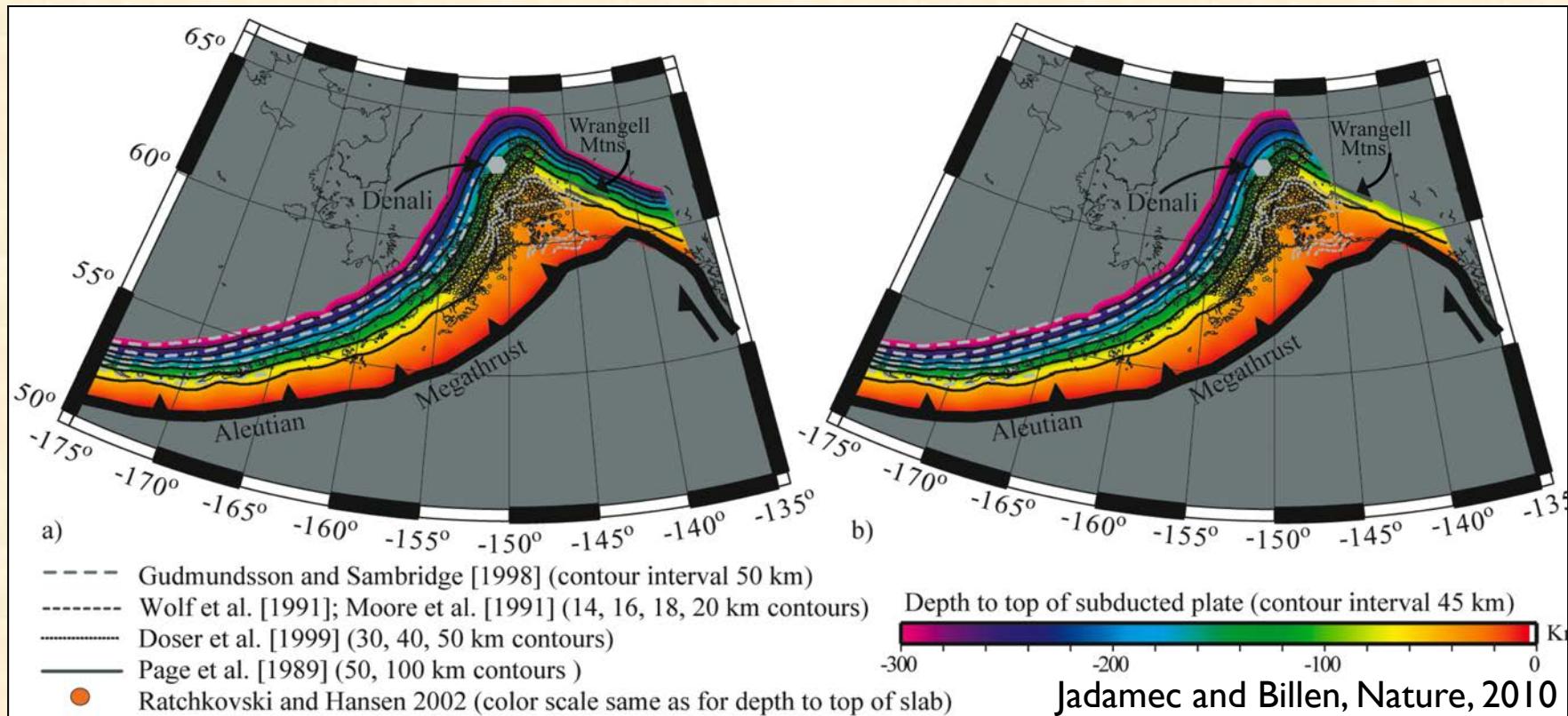
Mesh →  
Therm →  
Weak →



## Solution

$v, p$  →  
 $\sigma, \epsilon$  →  
 $\eta$  →

## Constraints on Slab Geometry



# Regional Model Design: Constraints on Plate Temperature

## Data Integration

Slab Shape  
Plate Ages  
Plt Bndy



## 3D Configuration

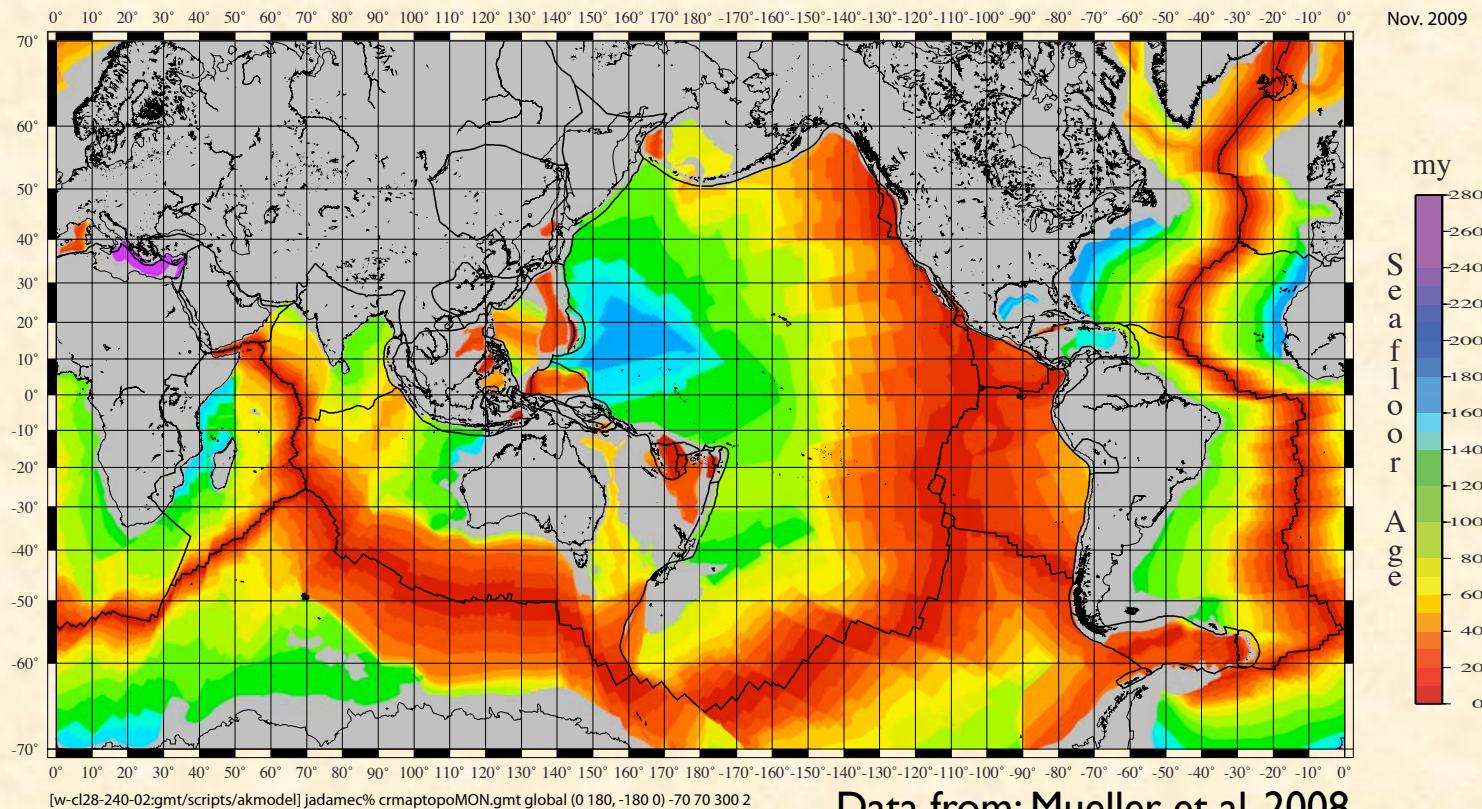
Mesh  
Therm  
Weak



## Solution

$v, p$   
 $\sigma, \epsilon$   
 $\eta$

## Constraints on Oceanic Plate Temperature



# Regional Model Design: Constraints on Plate Temperature

## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →



## 3D Configuration

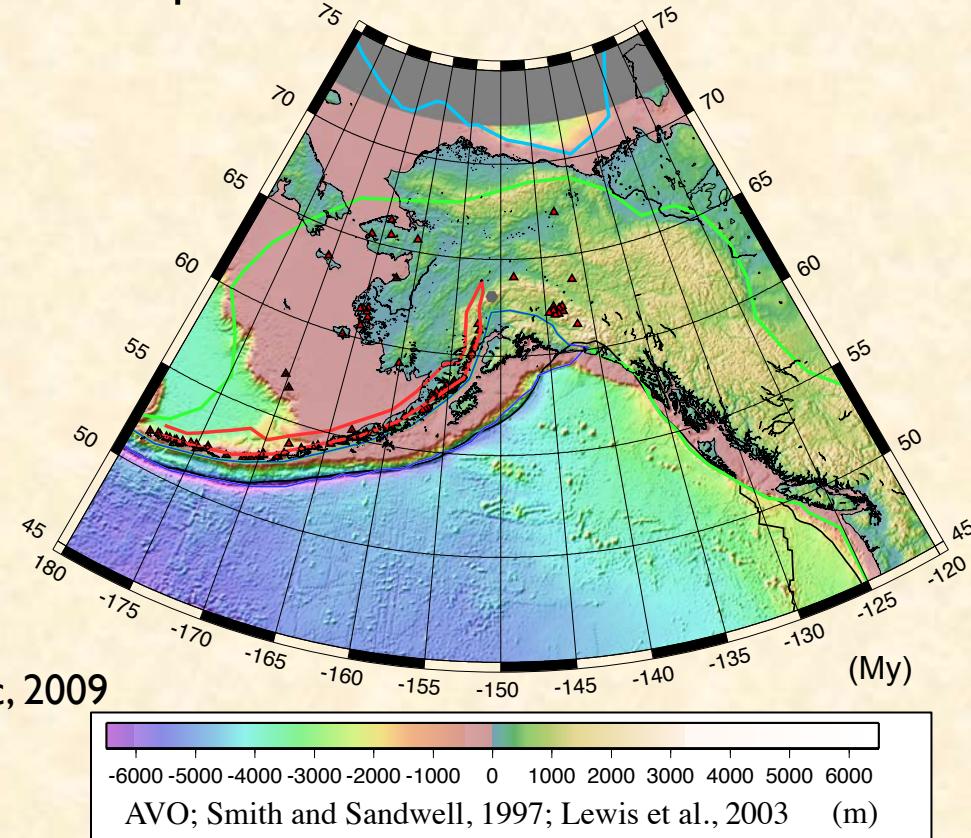
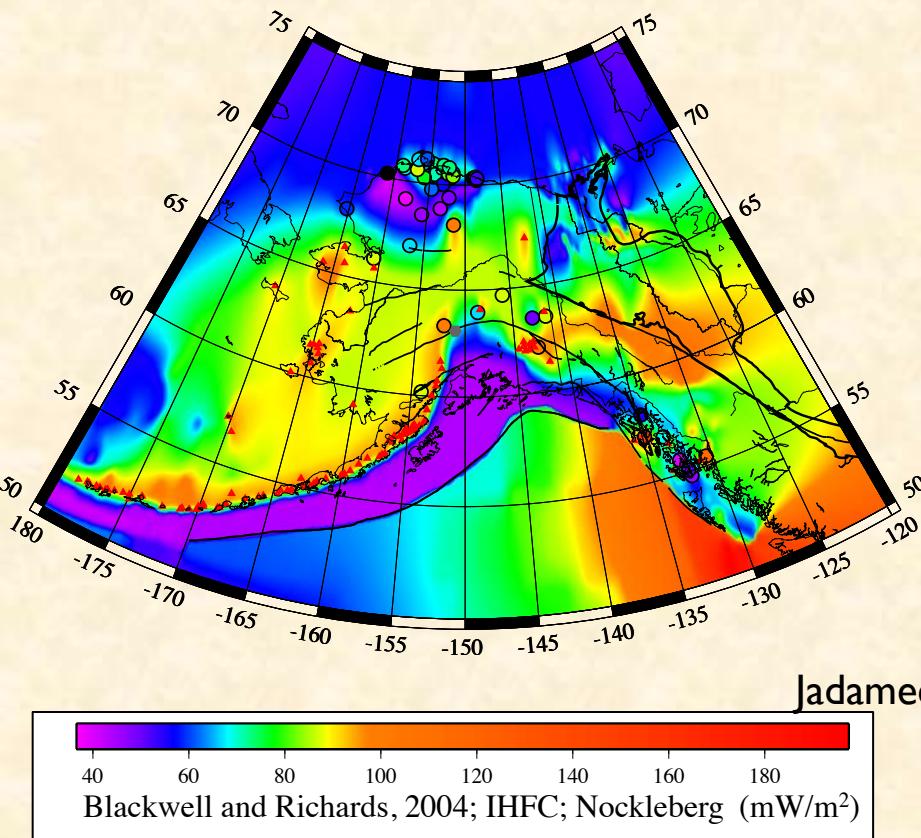
Mesh →  
Therm →  
Weak →



## Solution

$v, p$  →  
 $\sigma, \epsilon$  →  
 $\eta$  →

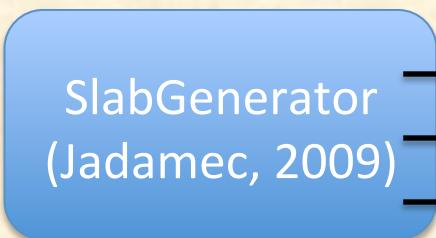
### Constraints on Continental Plate Temperature



# Regional Model Design: Constraints on Plate Thickness

## Data Integration

Slab Shape  
Plate Ages  
Plt Bndy



## 3D Configuration

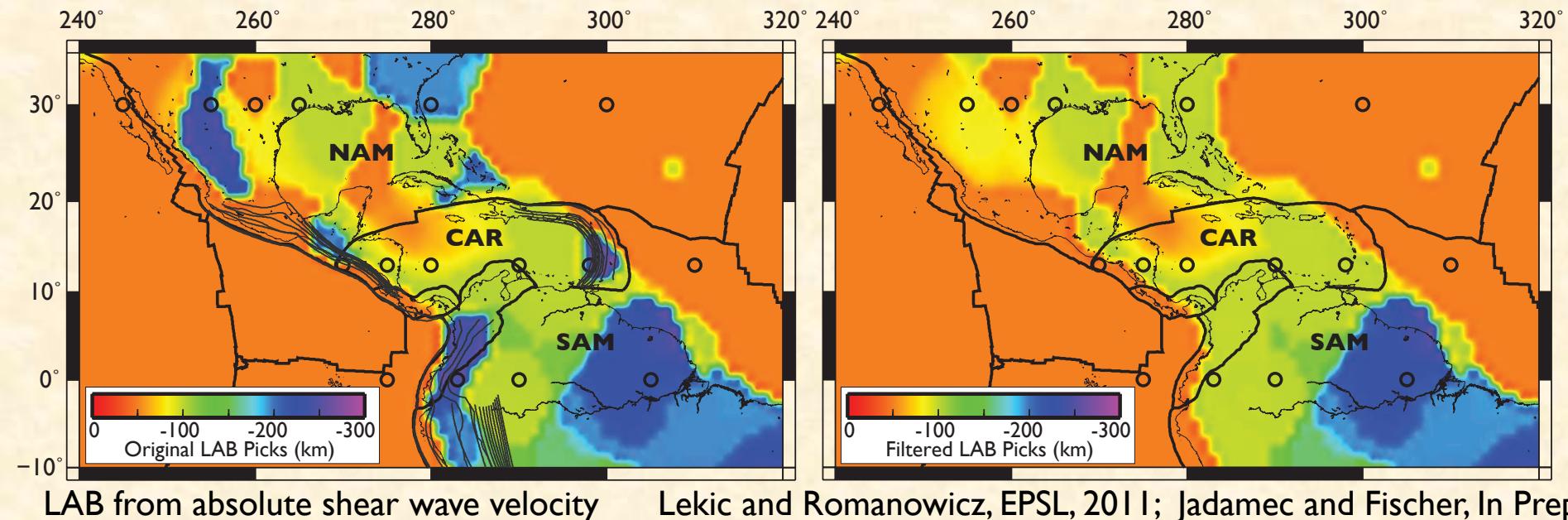
Mesh  
Therm  
Weak



## Solution

$v, p$   
 $\sigma, \epsilon$   
 $\eta$

Constraints on Upper Plate Thickness (Depth to LAB)



# Regional Model Design: Calculation of Initial Temperature

## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →

SlabGenerator  
(Jadamec, 2009)

## 3D Configuration

Mesh →  
Therm →  
Weak →

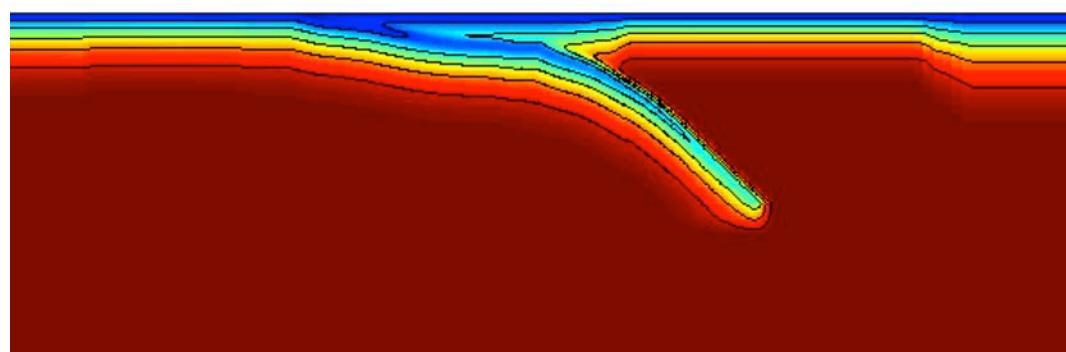
CitcomCU  
(Zhong, 2006)

## Solution

v, p →  
 $\sigma, \epsilon$  →  
 $\eta$  →

$$T = (T_m - T_s) \operatorname{erf} \left( \frac{d}{2\sqrt{\kappa t}} \right) + T_s$$

$$T = T_s + (T_m - T_s) \left[ \frac{y}{y_{Lo}} + \frac{2}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} \exp \left( -\frac{\kappa n^2 \pi^2 t}{y_{Lo}^2} \right) \sin \left( \frac{n \pi y}{y_{Lo}} \right) \right]$$



Jadamec and Billen, Nature, 2010; Jadamec et al., EPSL 2013

# Regional Model Design: Calculation of Initial Temperature

## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →



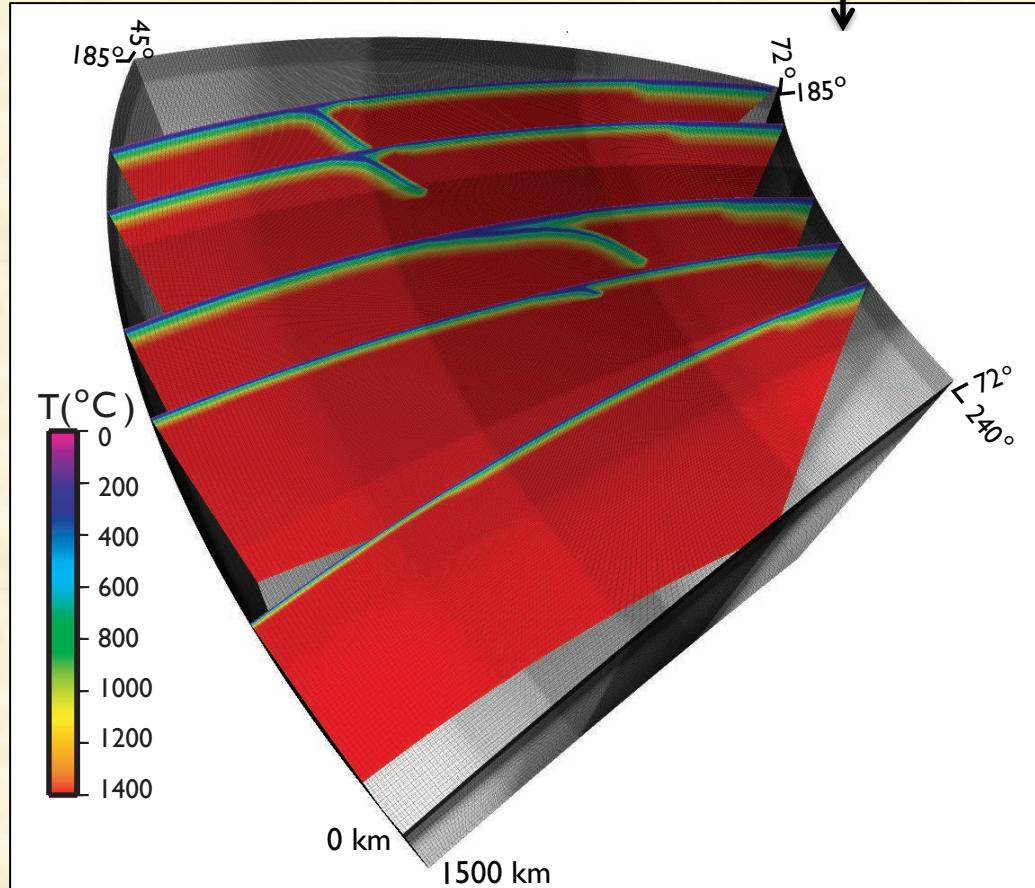
## 3D Configuration

Mesh →  
Therm →  
Weak →



## Solution

$v, p$  →  
 $\sigma, \epsilon$  →  
 $\eta$  →



### 3D Models:

55° × 27° × 1500 km  
El: 960 × 648 × 160  
Res: 2.35 – 20 km

50° × 35° × 1000 km  
El: 896 × 864 × 112  
Res: 2.75 – 25 km

69° × 38° × 1500 km  
El: 1536 × 1152 × 160  
Res: 2.75 – 25 km

Jadamec and Billen, Nature, 2010  
Jadamec and Billen, JGR, 2012  
Jadamec et al., EPSL, 2013  
Jadamec and Fisher, In Prep

# Regional Model Design: Calculation of Initial Temperature

## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →



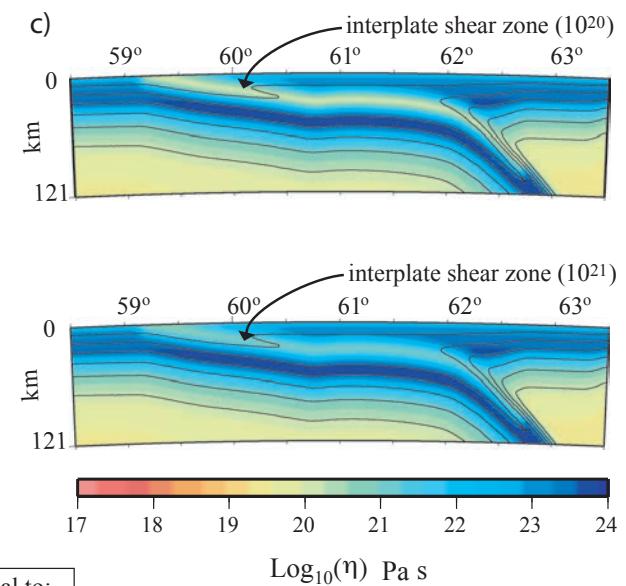
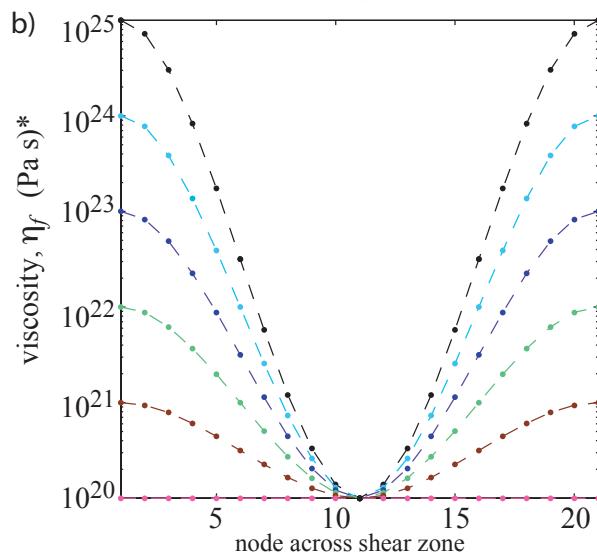
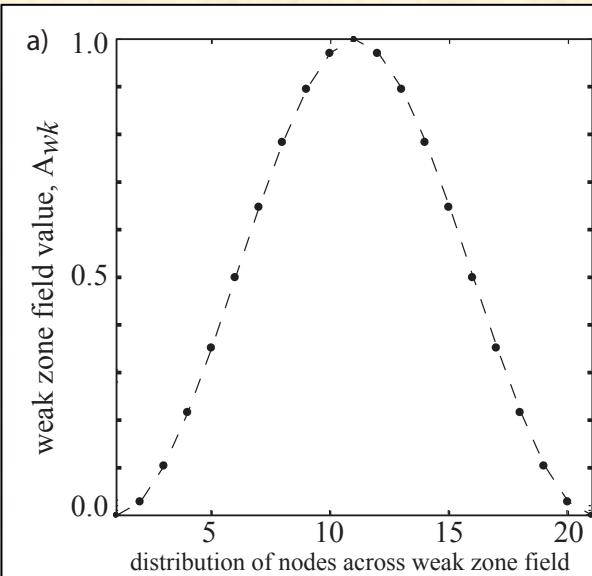
## 3D Configuration

Mesh →  
Therm →  
Weak →



## Solution

$v, p$  →  
 $\sigma, \epsilon$  →  
 $\eta$  →



# Regional Model: Viscous Flow Code CitcomCU

Solves conservation equations for incompressible, creeping flow

$$\nabla \cdot \mathbf{u} = 0$$

$$\nabla p - \nabla \cdot [\eta_{\text{eff}} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)] = \rho_o \alpha (T - T_o) g \delta_{rr}$$

(Moresi and Solomatov, Phys. Fluids, 1995; Moresi et al., PEPI, 1996; Zhong, JGR, 2006)

## Composite Rheology

The composite rheology,  $\eta_{\text{com}}$ , is defined by

$$\eta_{\text{com}} = \frac{\eta_{\text{df}} \eta_{\text{ds}}}{\eta_{\text{df}} + \eta_{\text{ds}}}$$

where the flow law for wet olivine\* is

$$\eta_{\text{df,ds}} = \left( \frac{d^p}{A C_{\text{OH}}^r} \right)^{\frac{1}{n}} \dot{\varepsilon}^{\frac{1-n}{n}} \exp \left[ \frac{E + PV}{nRT} \right]$$

Variable	Description	df	ds
A	pre-exponential factor	1.0	$9 \times 10^{-20}$
n	stress exponent	1	3.5
d	grain size, $\mu\text{m}$ (assuming A term is in $\mu\text{m}$ )	$10 \times 10^3$	—
p	grain size exponent	3	—
$C_{\text{OH}}$	OH concentration in H/ $10^6$ Si	1000	1000
r	exponent for $C_{\text{OH}}$ term	1	1.2
E	activation energy, kJ/mol	335	480
V	activation volume, $\text{m}^3/\text{mol}$	$4 \times 10^{-6}$	$11 \times 10^{-6}$

\*flow law and parameters for wet olivine (Hirth and Kohlstedt 2003)

and a depth-dependent yield stress is applied such that if

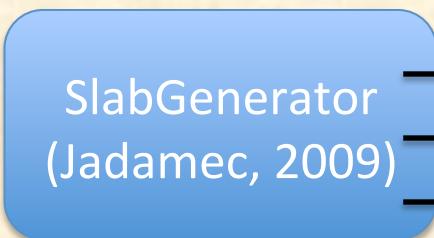
$$\sigma > \sigma_y, \eta_{\text{eff}} = \frac{\sigma_y}{\dot{\varepsilon}_{II}}, \text{ and if } \sigma < \sigma_y, \eta_{\text{eff}} = \eta_{\text{com}}$$

Hirth and Kohlstedt, Monograph, 2003; Billen and Hirth, G<sup>3</sup>, 2007; Jadamec and Billen, Nature, 2010

# Regional Model Tests: Effects on Model Runtime

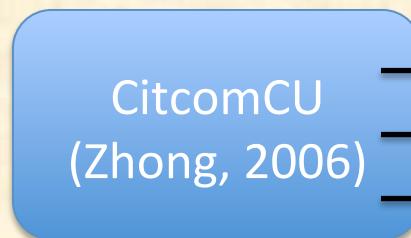
## Data Integration

Slab Shape →  
Plate Ages →  
Plt Bndy →



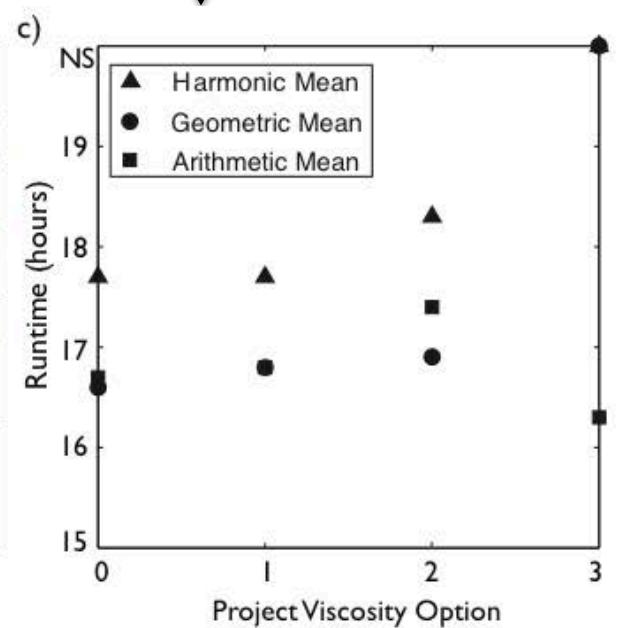
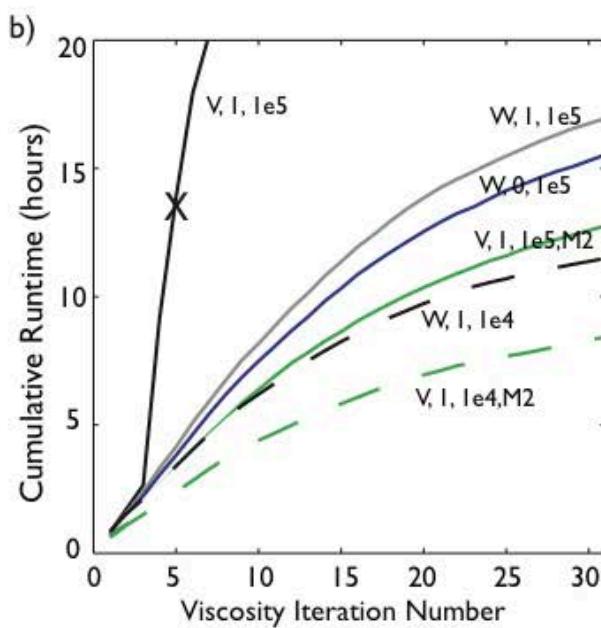
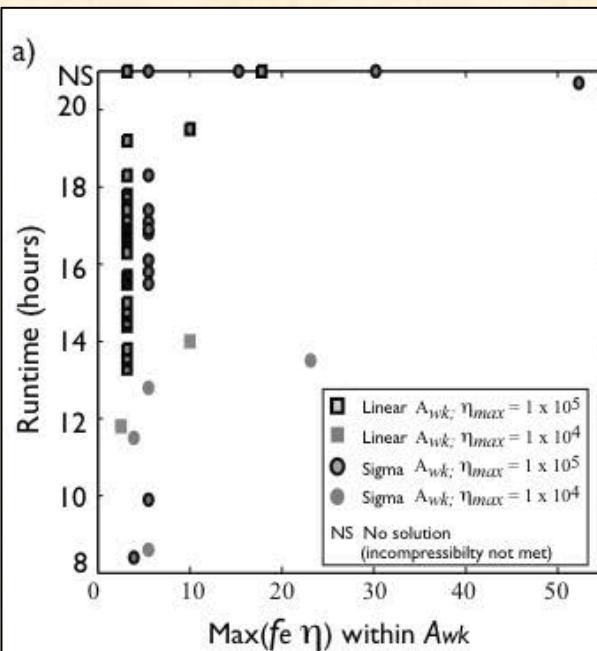
## 3D Configuration

Mesh →  
Therm →  
Weak →



## Solution

$v, p$  →  
 $\sigma, \epsilon$  →  
 $\eta$  →



# Methods: 3D Visualization of Temperature and Viscosity

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## Flat Slab Subduction, the Denali Fault, and Mountain Building in the Central Alaska Range

by Margarete Jadamec

in collaboration with Magali Billen and Sarah Roeske

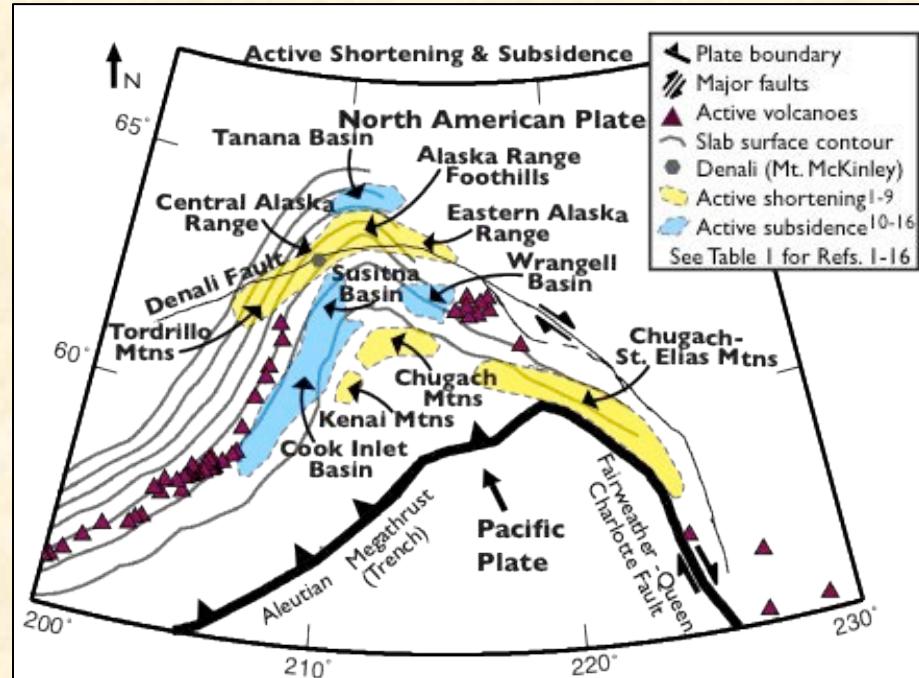
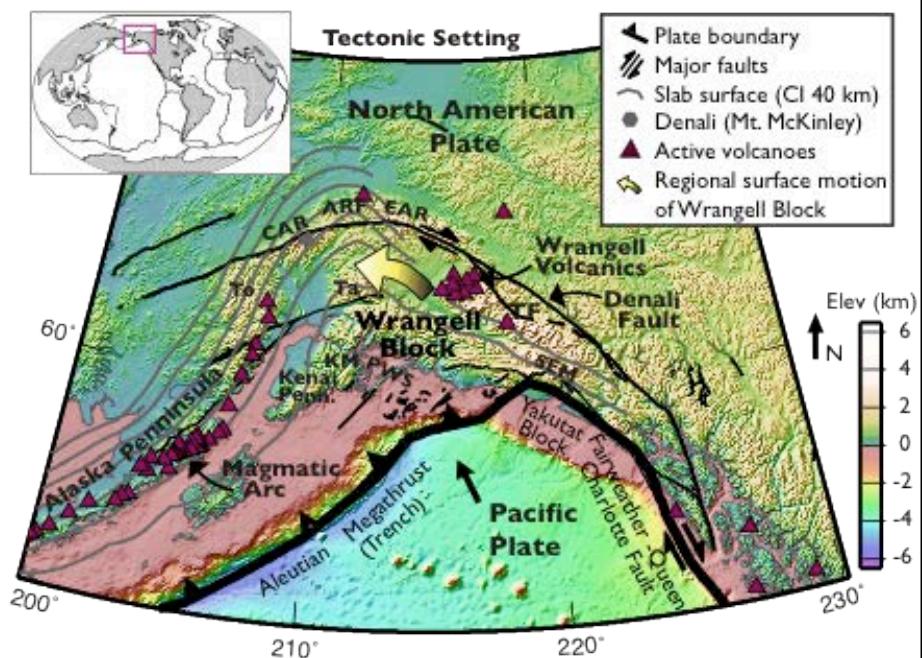
Filmed by Oliver Kreylos in the KeckCAVES

Edited by Margarete Jadamec

For additional Information See:

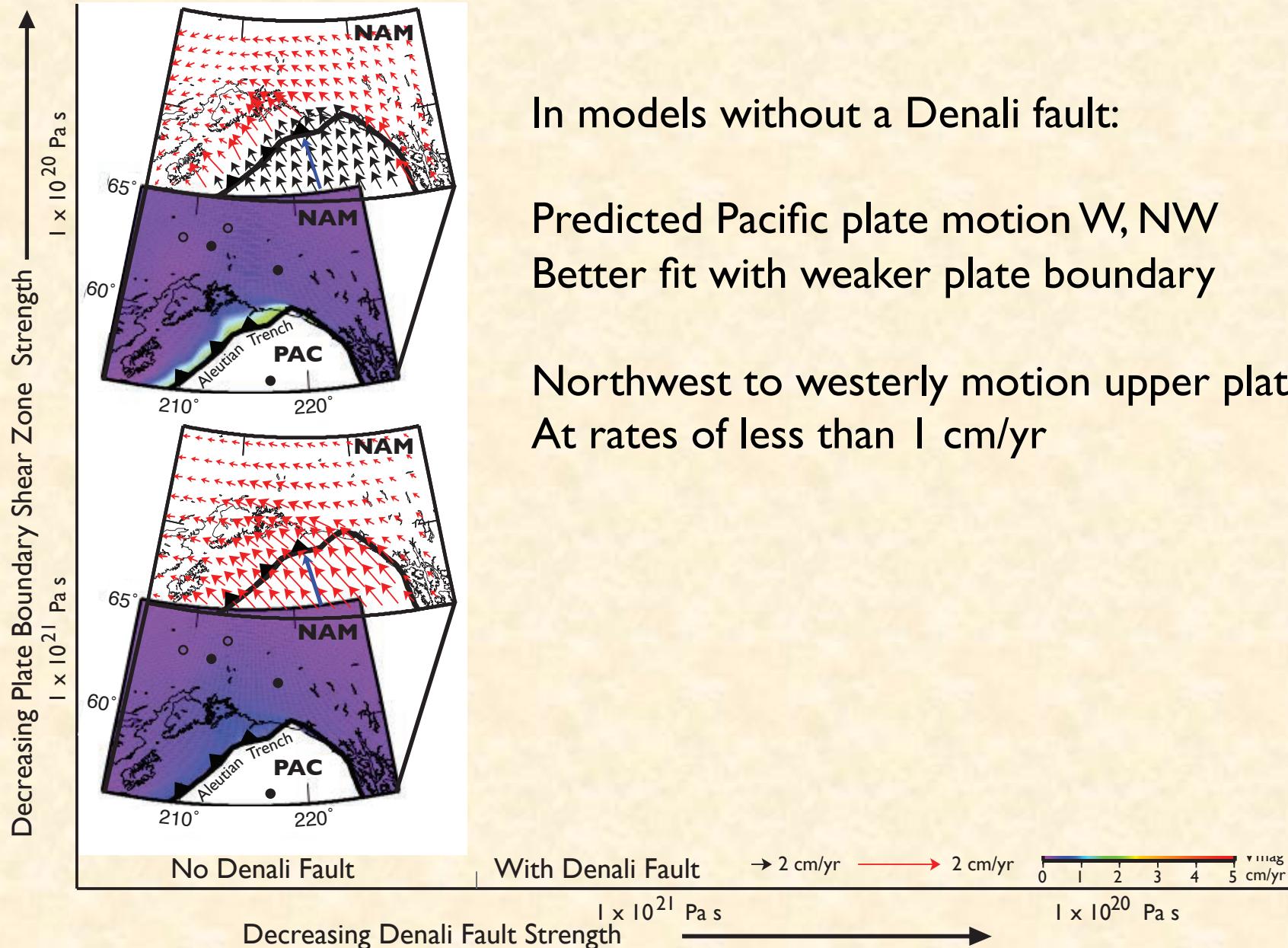
Jadamec, M. A., Billen, M. I., and Roeske, S. M., 2013, Three-dimensional numerical models of flat slab subduction and the Denali fault driving deformation in south-central Alaska. *Earth and Planetary Science Letters*, 376, p. 29-42, 2013. doi:10.1016/j.epsl.2013.06.009.

# Tectonic Setting in South Central Alaska

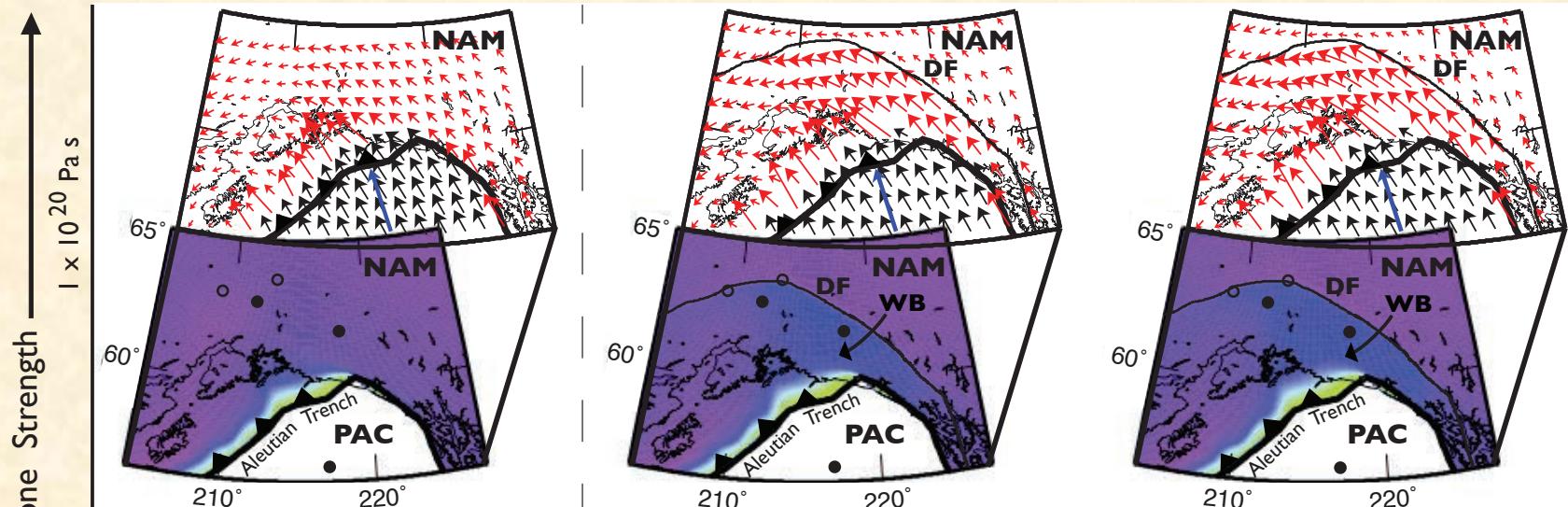


Jadamec et al., EPSL, 2013

# Newtonian Viscosity: Predicted Surface Velocity



# Newtonian Viscosity: Predicted Surface Velocity



With Denali fault :

Denali fault decouples part of Alaska (WB) from rest of NAM

Models with Denali fault - Sharp velocity gradient across DF

WB motion sub-parallel to motion of underlying flat slab and DF

Weaker Denali fault, faster Wrangell Block velocity

No Denali Fault

With Denali Fault

$\rightarrow 2 \text{ cm/yr}$

$\rightarrow 2 \text{ cm/yr}$

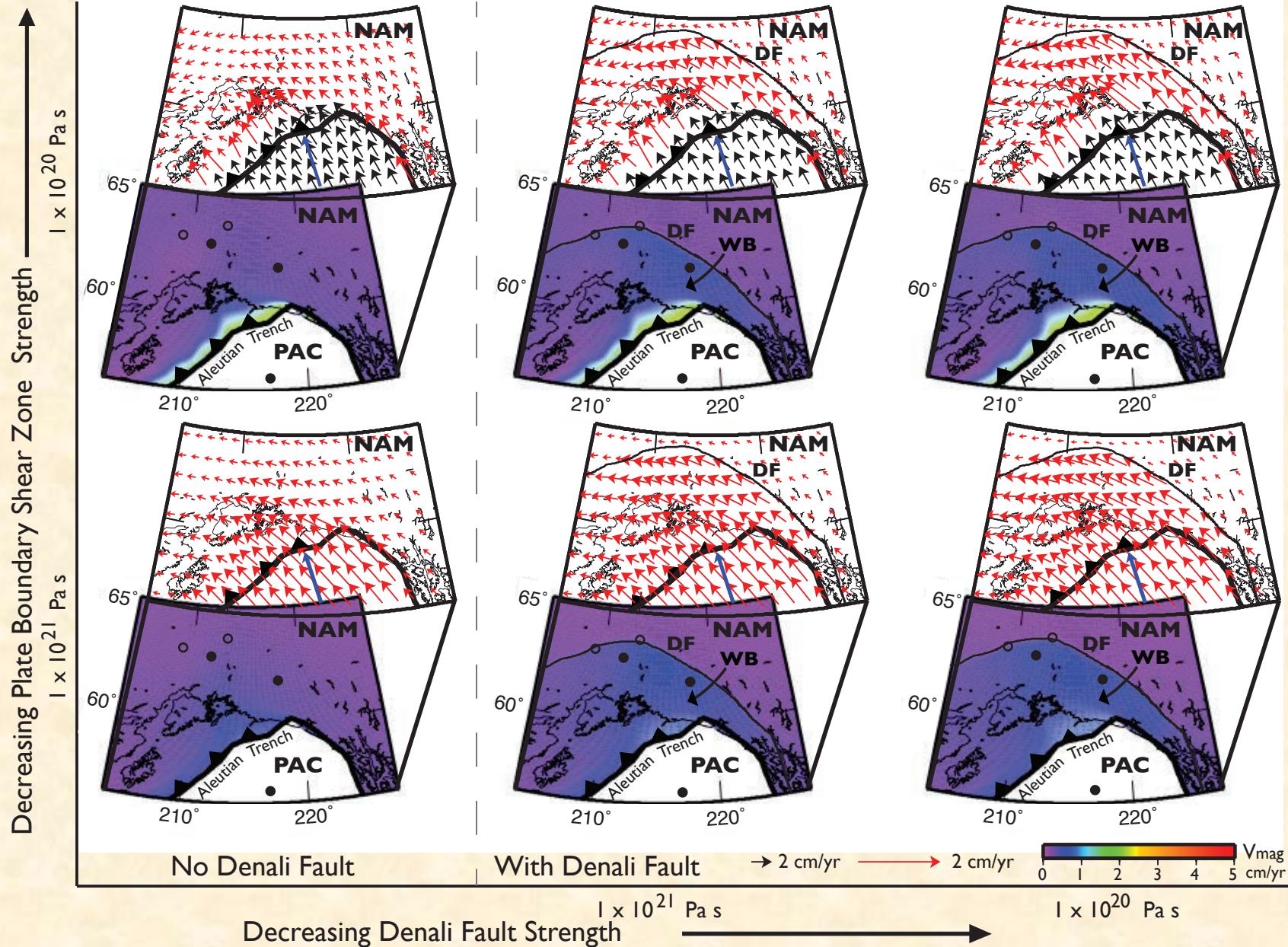
0 1 2 3 4 5  
cm/yr

Decreasing Denali Fault Strength

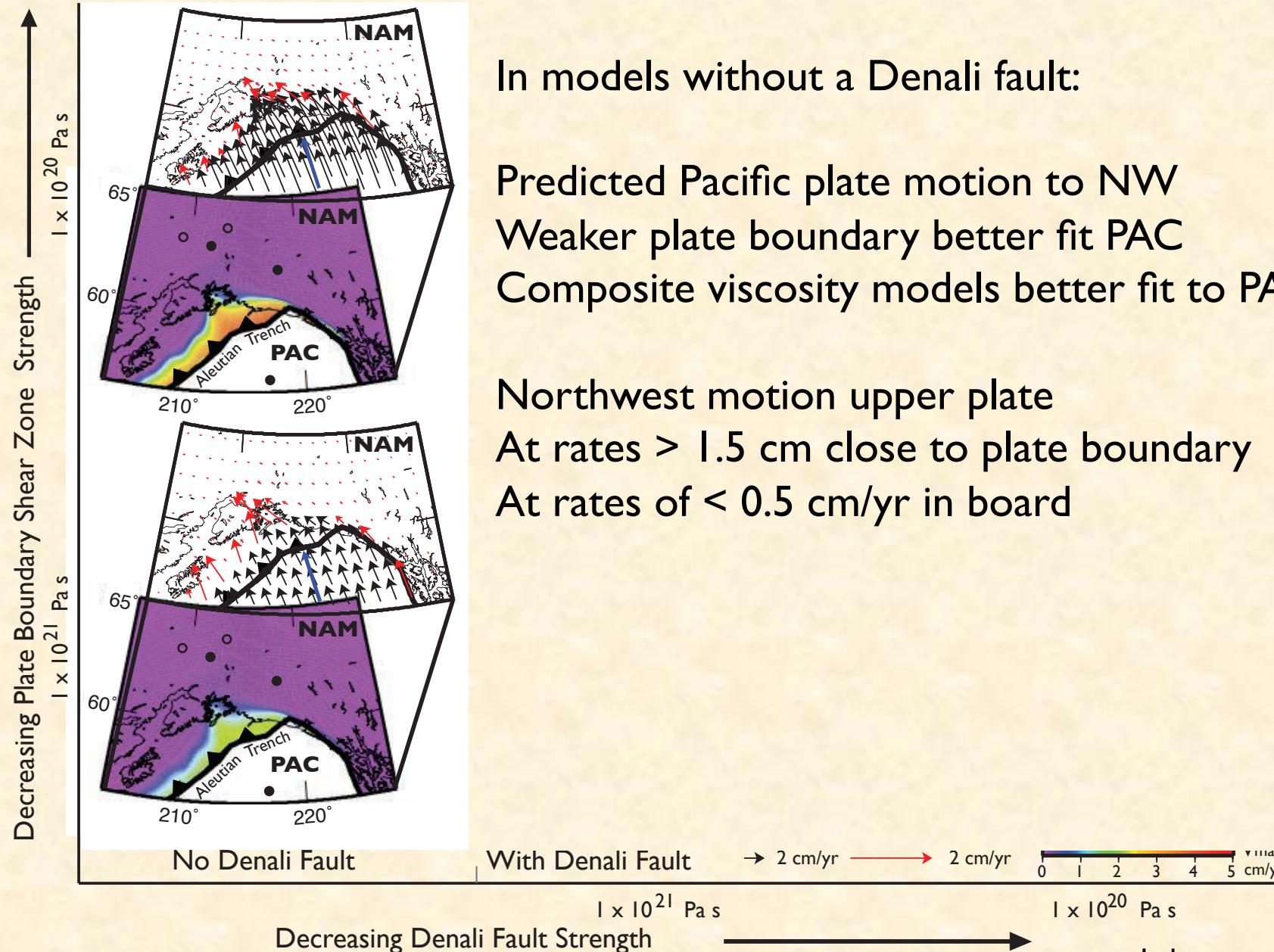
$1 \times 10^{21} \text{ Pa s}$

$1 \times 10^{20} \text{ Pa s}$

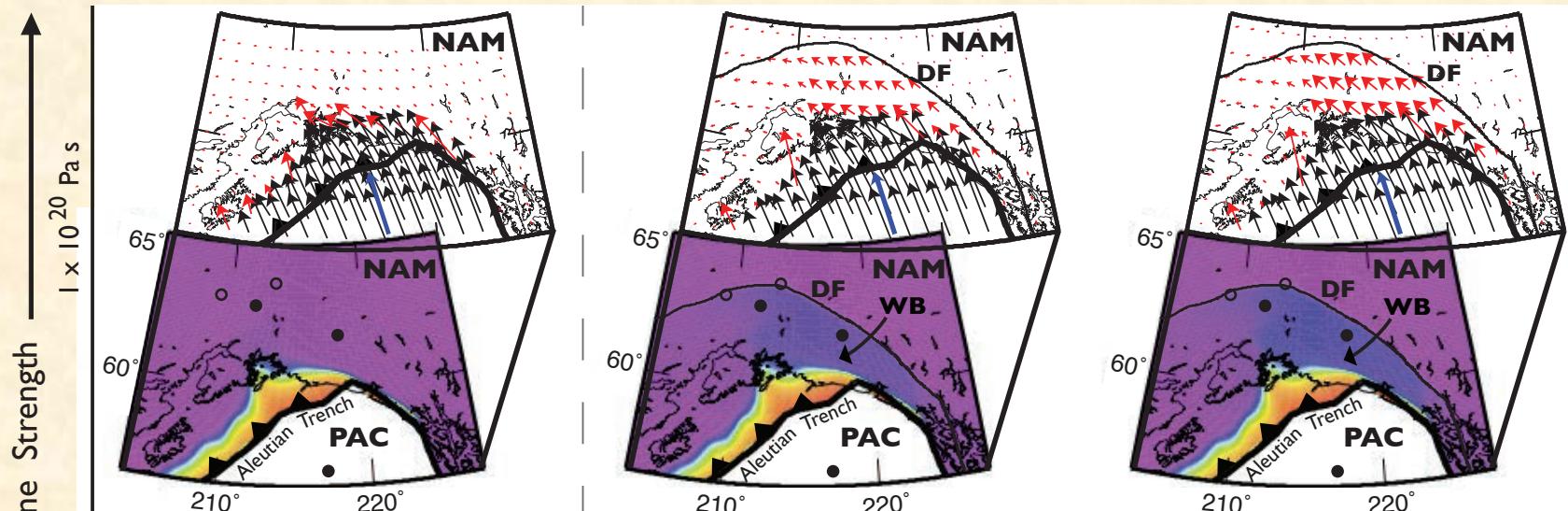
# Newtonian Viscosity: Predicted Surface Velocity



# Non-Newtonian Viscosity: Predicted Surface Velocity



# Non-Newtonian Viscosity: Predicted Surface Velocity



With Denali fault :

Denali fault decouples part of Alaska from rest of NAM

Models with Denali fault - Sharper velocity gradient across DF

Weaker Denali fault, faster Wrangell Block velocity

Motion sub-parallel to motion of underlying flat slab

Predicts convergence at northern bend in DF (AK Range)

No Denali Fault

With Denali Fault

$\rightarrow 2 \text{ cm/yr}$

$\rightarrow 2 \text{ cm/yr}$

0 1 2 3 4 5  
cm/yr

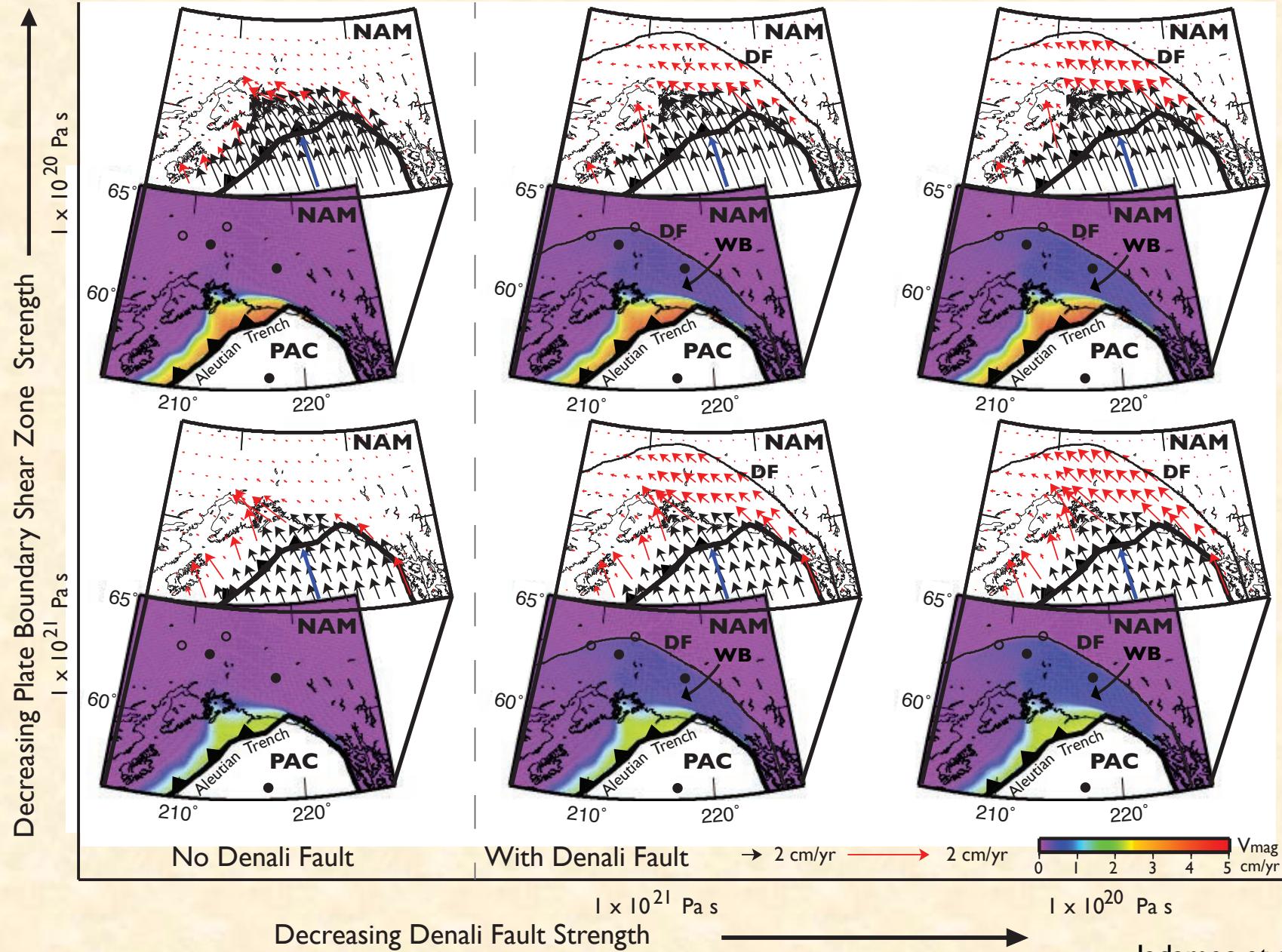
$1 \times 10^{21} \text{ Pa s}$

Decreasing Denali Fault Strength

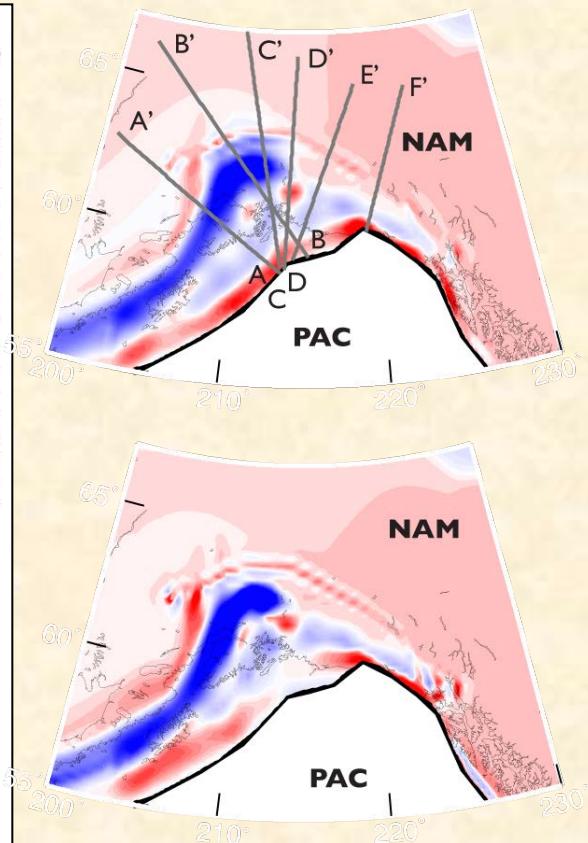
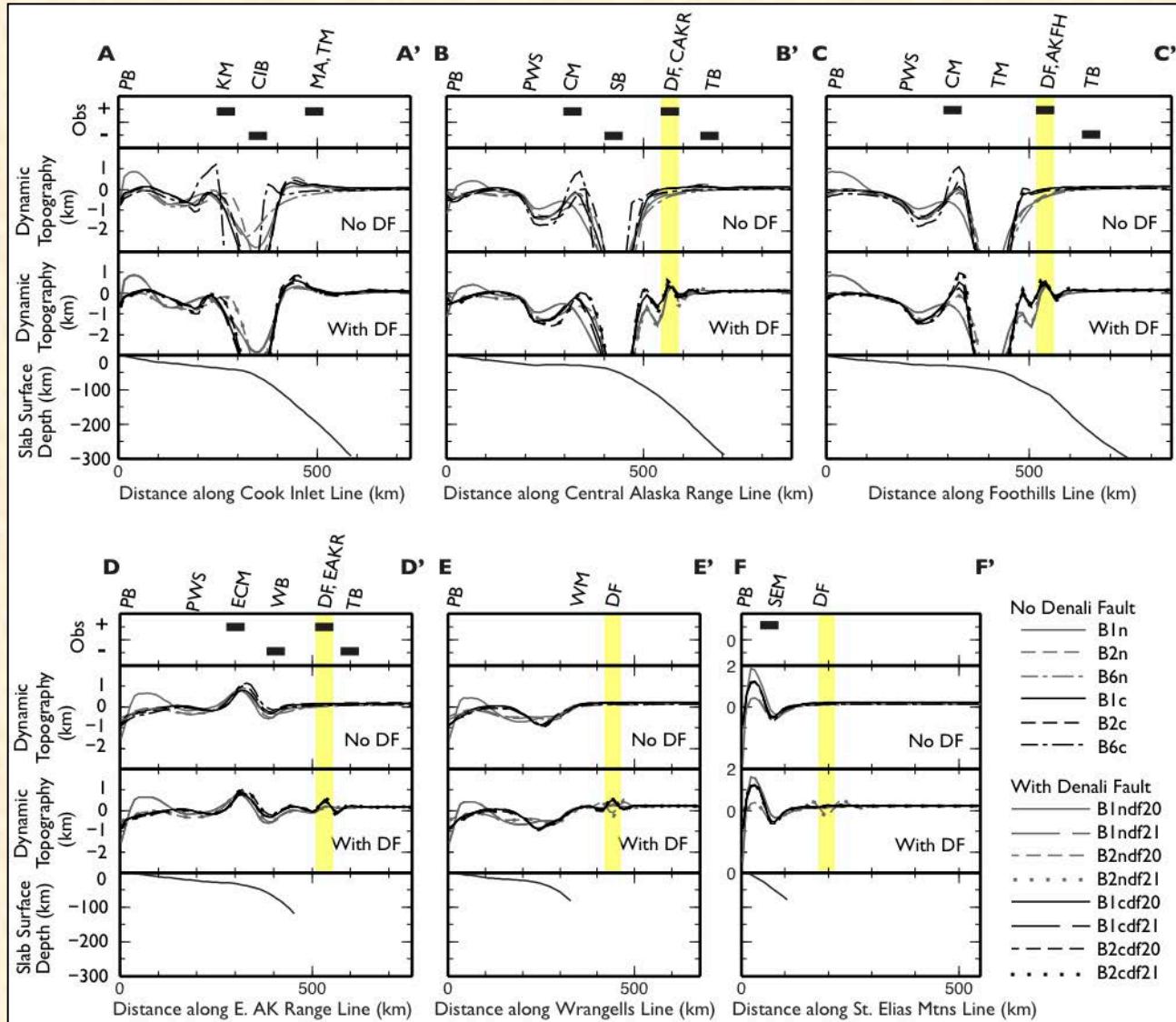
$1 \times 10^{20} \text{ Pa s}$

Jadamec et al., 2013

# Non-Newtonian Viscosity: Predicted Surface Velocity

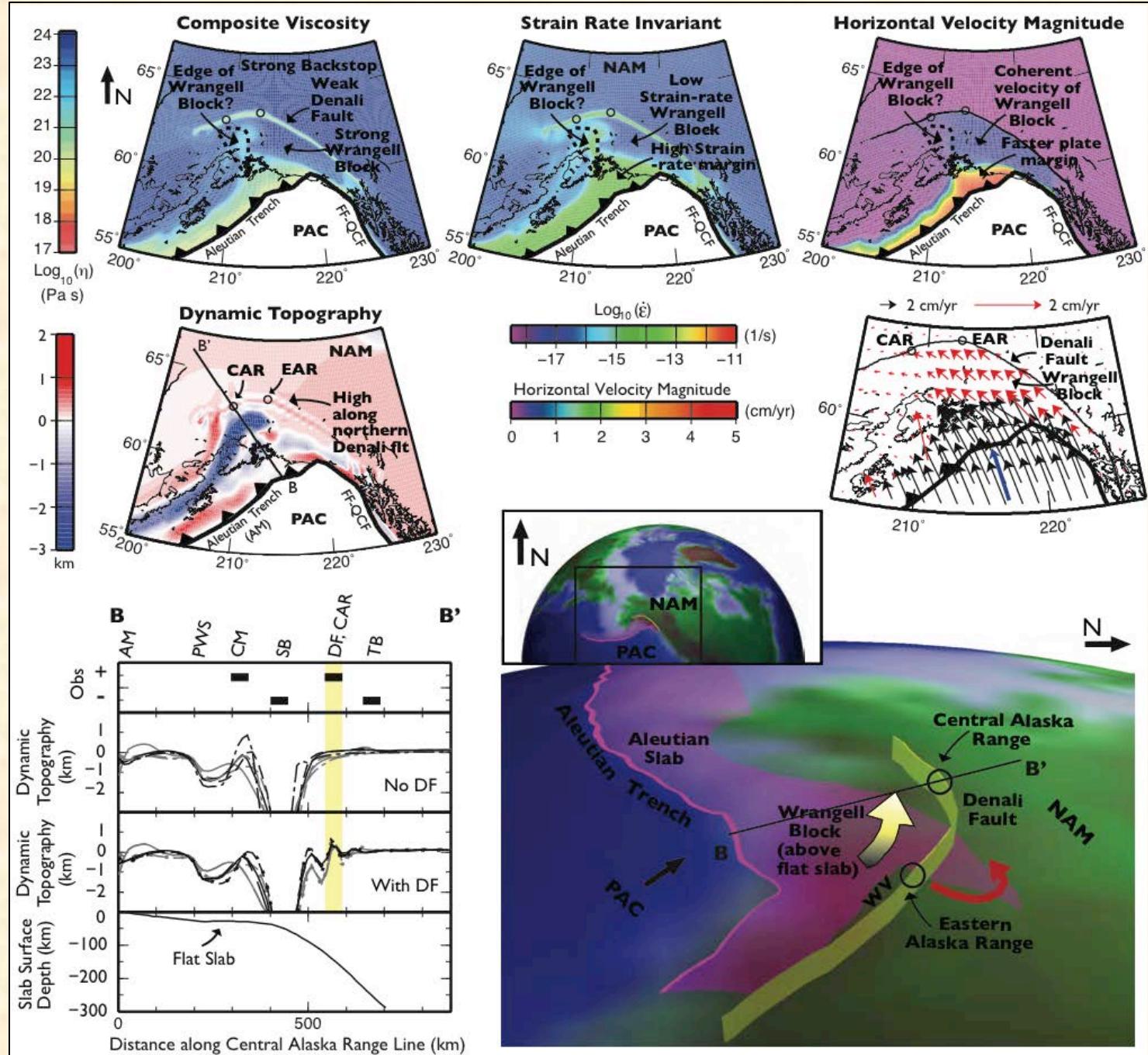


# Effect of Denali Fault on Uplift of the Central Alaska Range

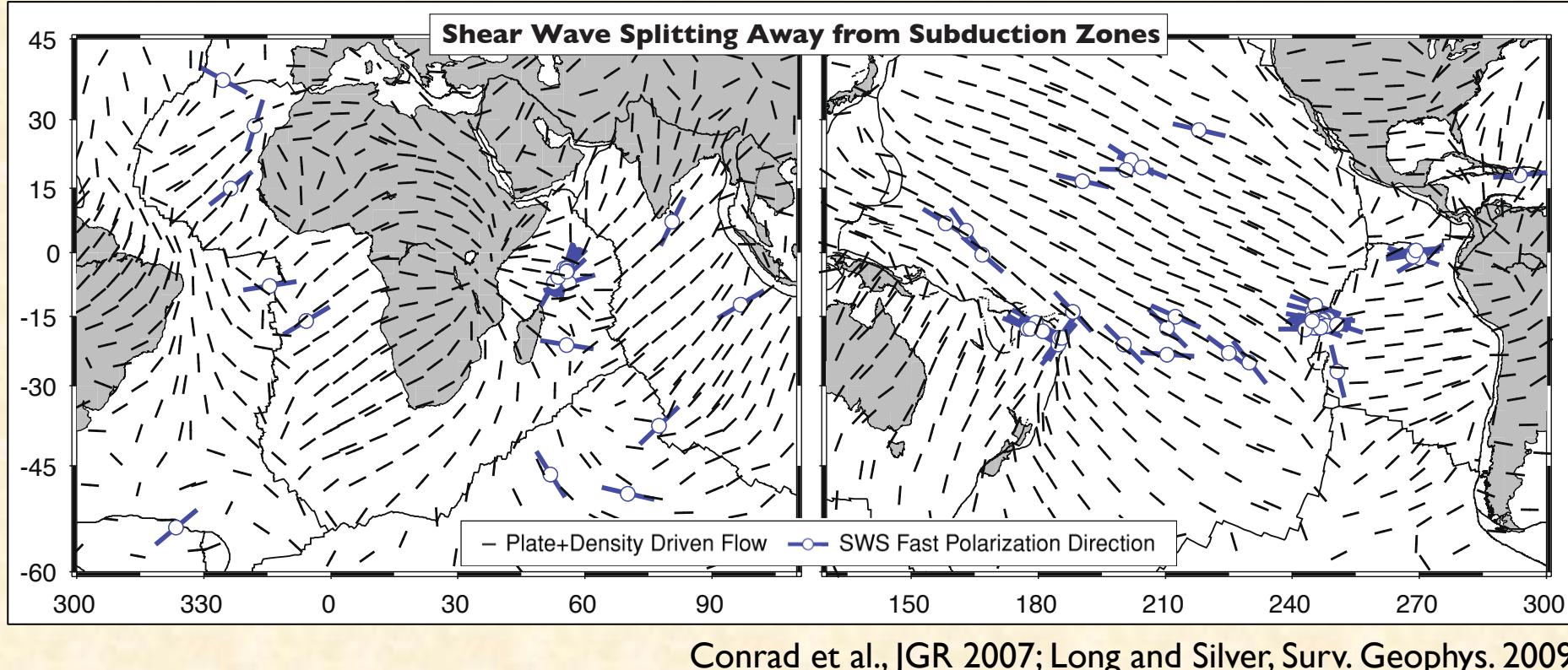


Denali fault  
localizes uplift  
in Alaska Range  
(greater in models with  
composite viscosity)

# Slab driving overriding plate deformation in South Central Alaska



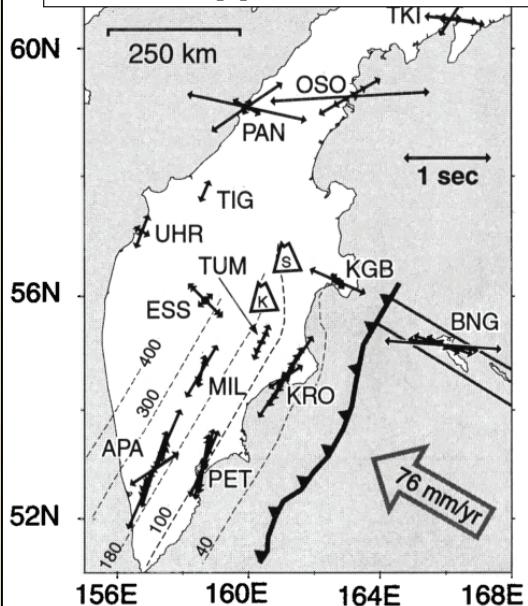
# What About the Mantle Underneath the Plates?



Away from subduction zones, the surface motion of oceanic plates is well correlated with the fast axis of seismic anisotropy implying **coupling** between the plates and mantle (assuming A type fabric in olivine)

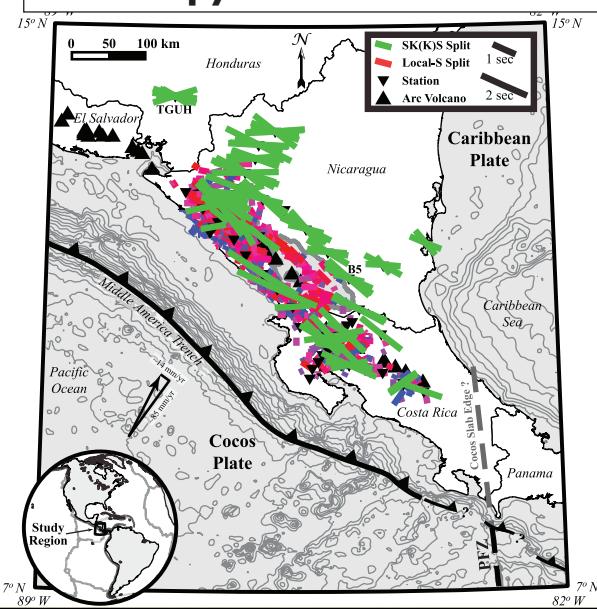
# Plate Mantle-(de)coupling & Is Complex Flow Common?

Anisotropy in Kamchatka



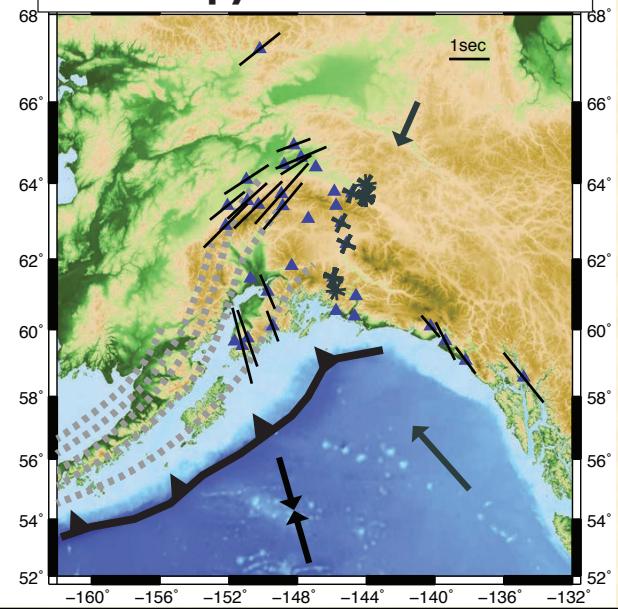
Peyton et al., GRL 2001

Anisotropy in Central America



Abt et al., JGR 2010

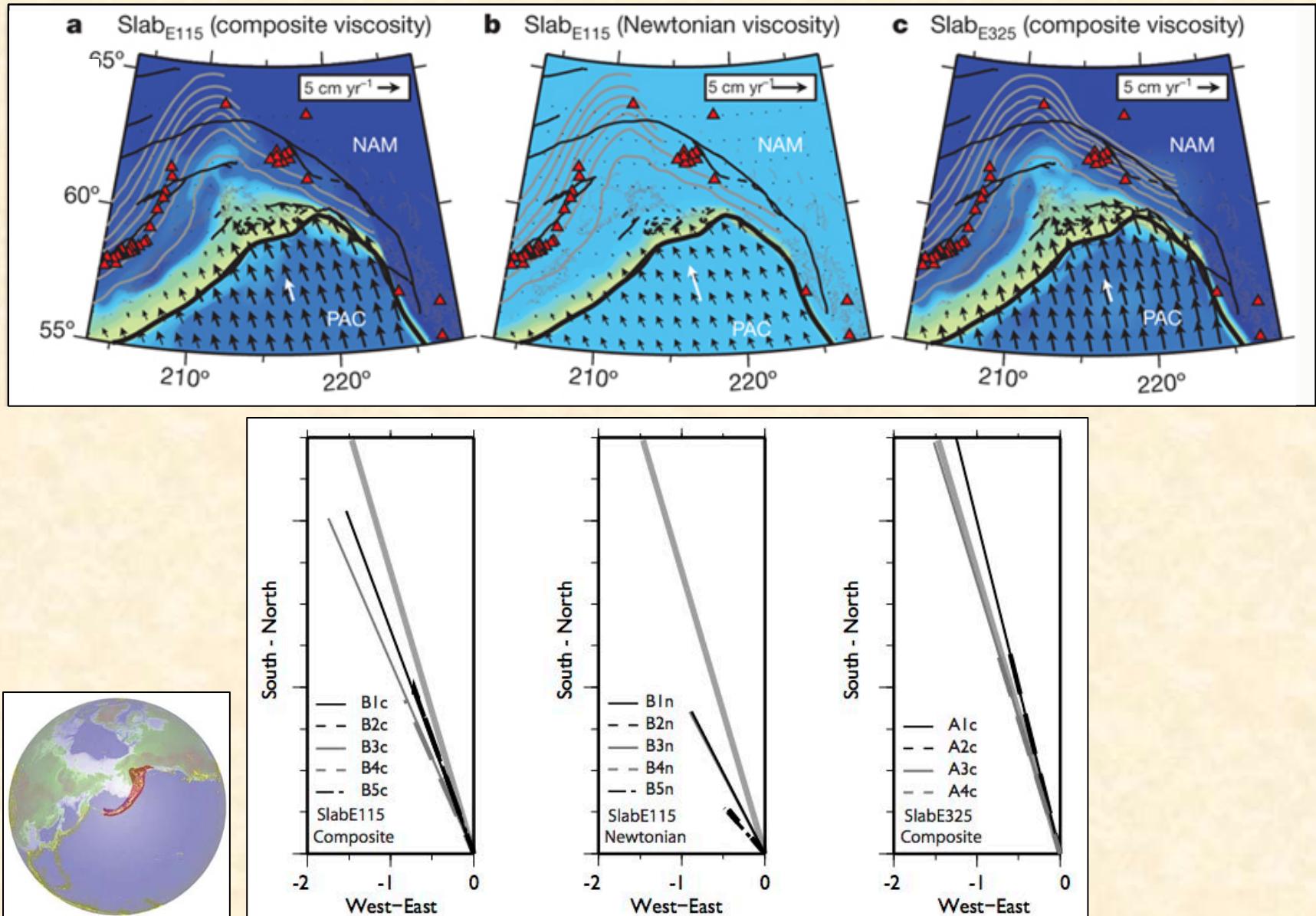
Anisotropy in Eastern Alaska



Hanna and Long, Tect. 2012

This is not the case at many subduction zones where the seismic fast axis is not aligned with surface plate motion, implying complex mantle flow in subduction zones and **decoupling** between the plates and mantle (assuming A type fabric in olivine)

# Results: Viscosity and Predicted Pacific Plate Motion



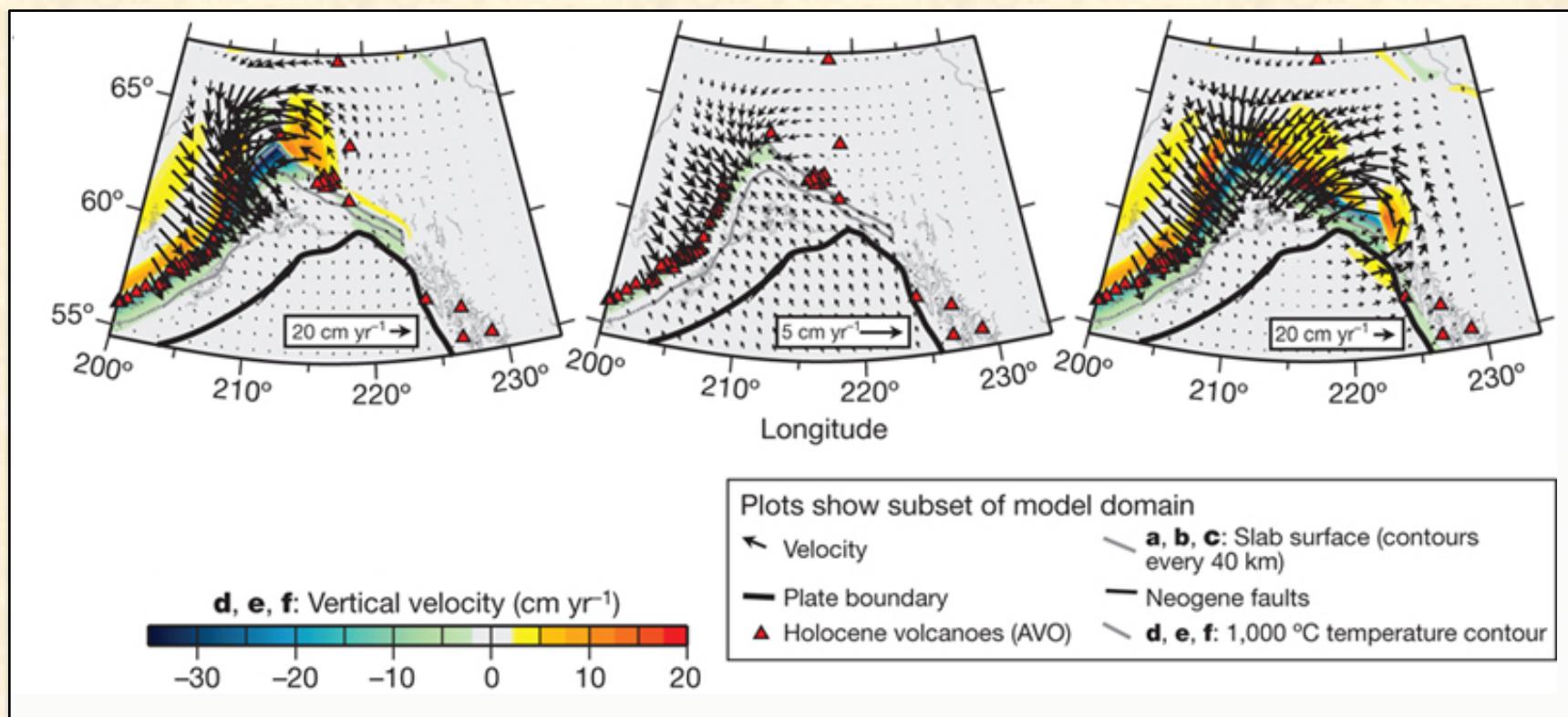
# Results: Predicted Mantle Velocity at 100 km Depth

Toroidal flow around slab edge

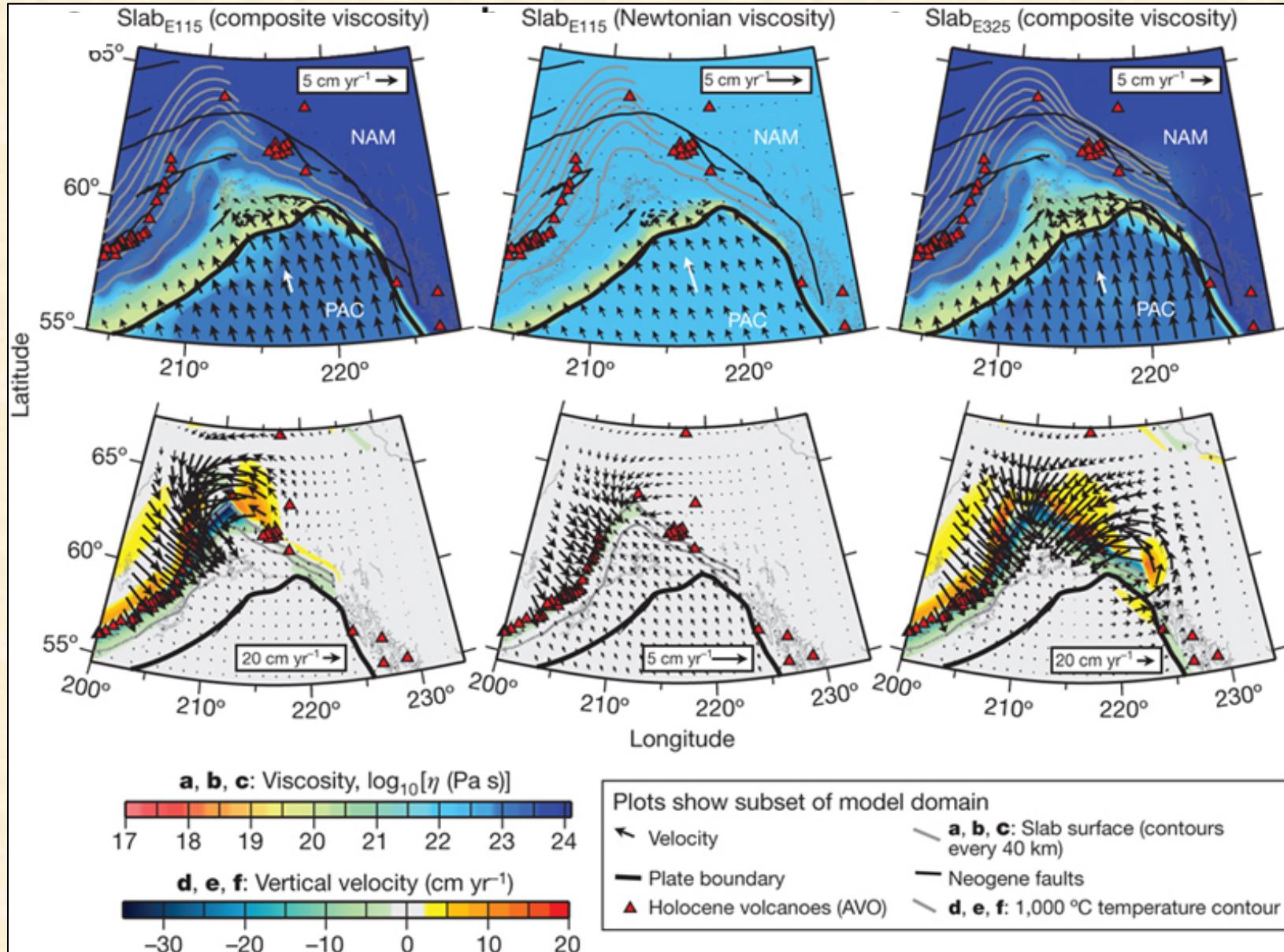
Upward component of flow associated with slab edge ( $> 5 \text{ cm/yr}$ )

Localized fast mantle flow velocity magnitudes ( $> 50 \text{ cm/yr}$ )

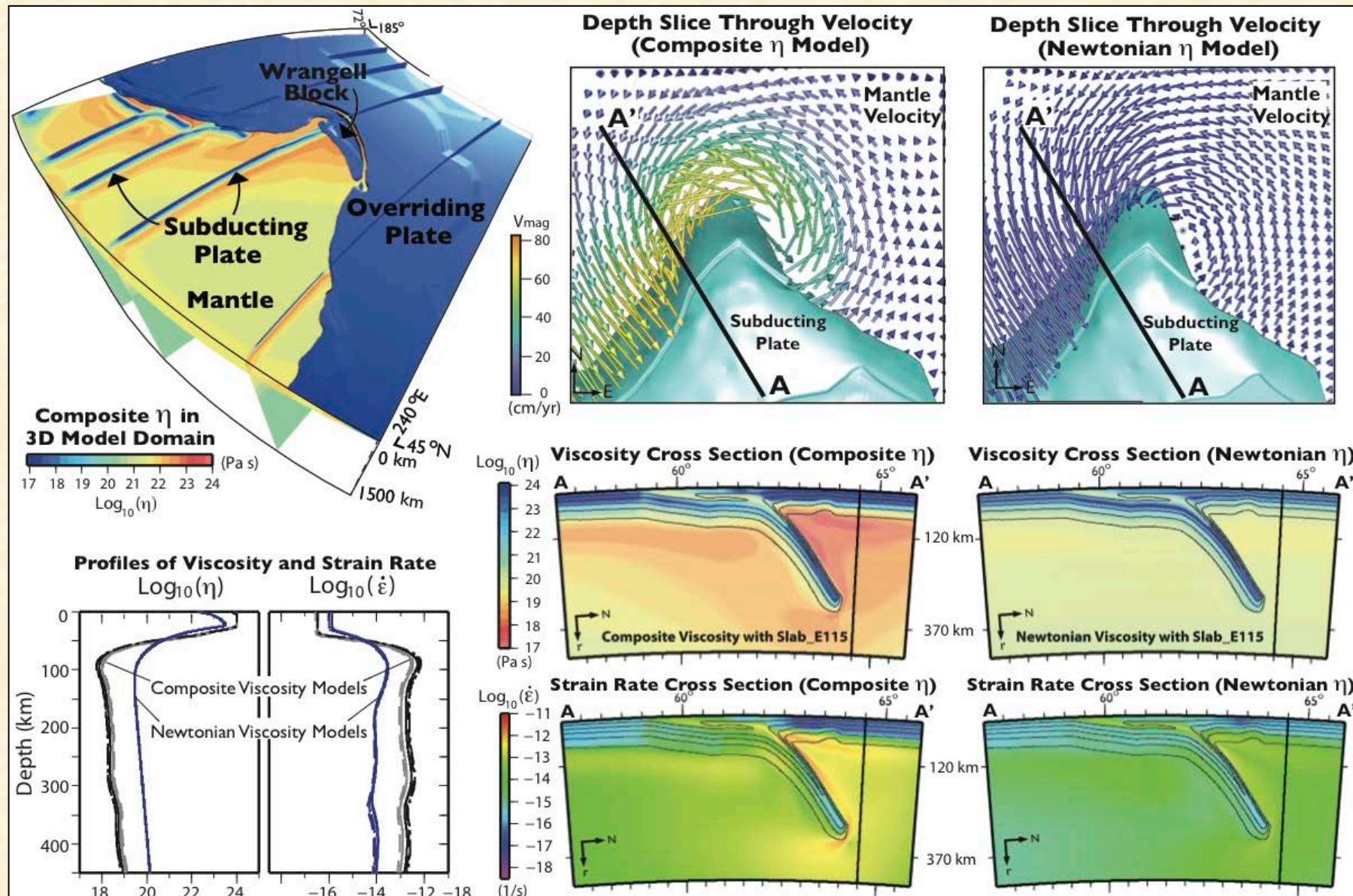
Location of toroidal flow shifts with position of slab edge



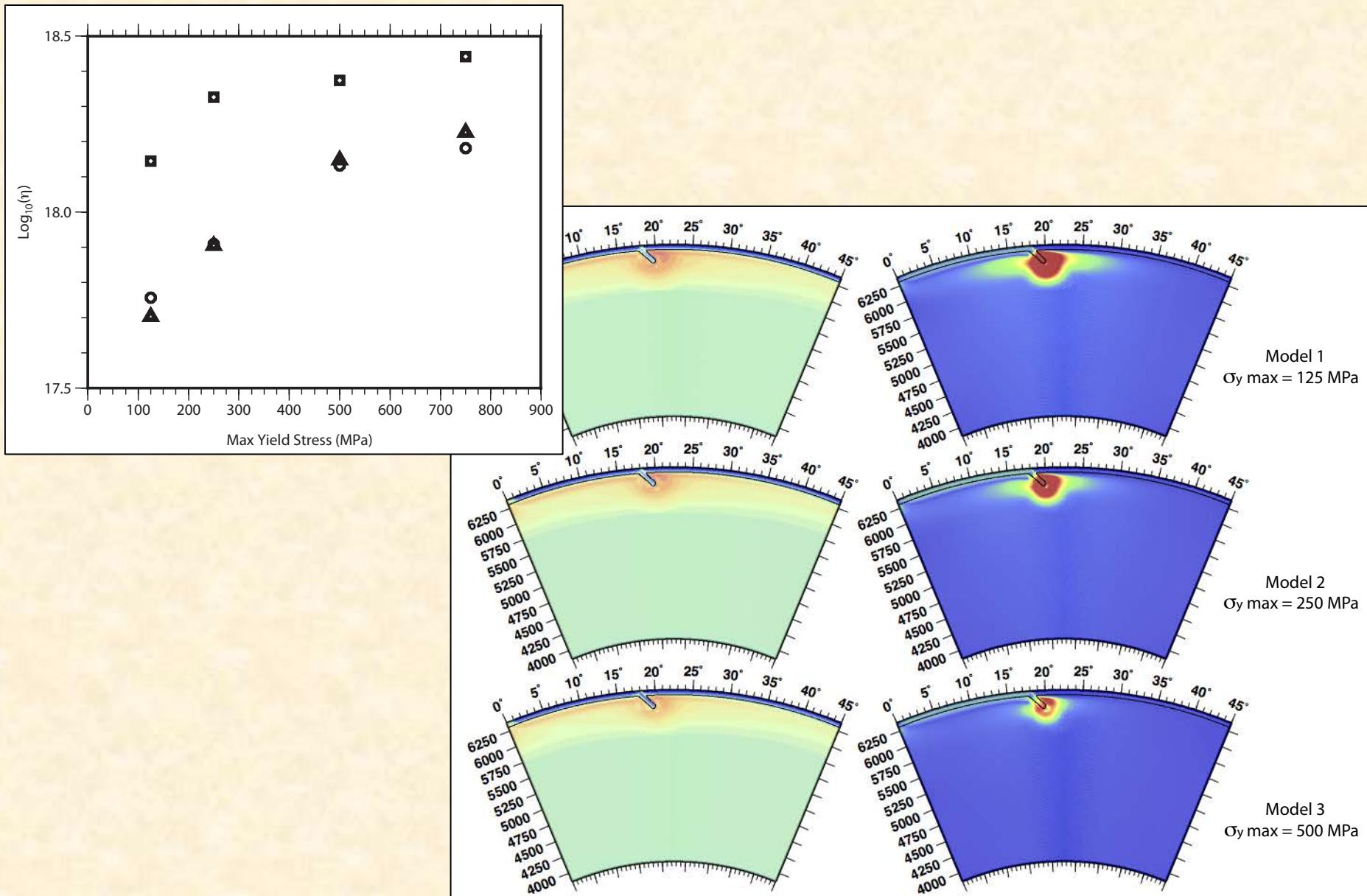
# Rapid Mantle Flow Not Inconsistent with Plate Motions



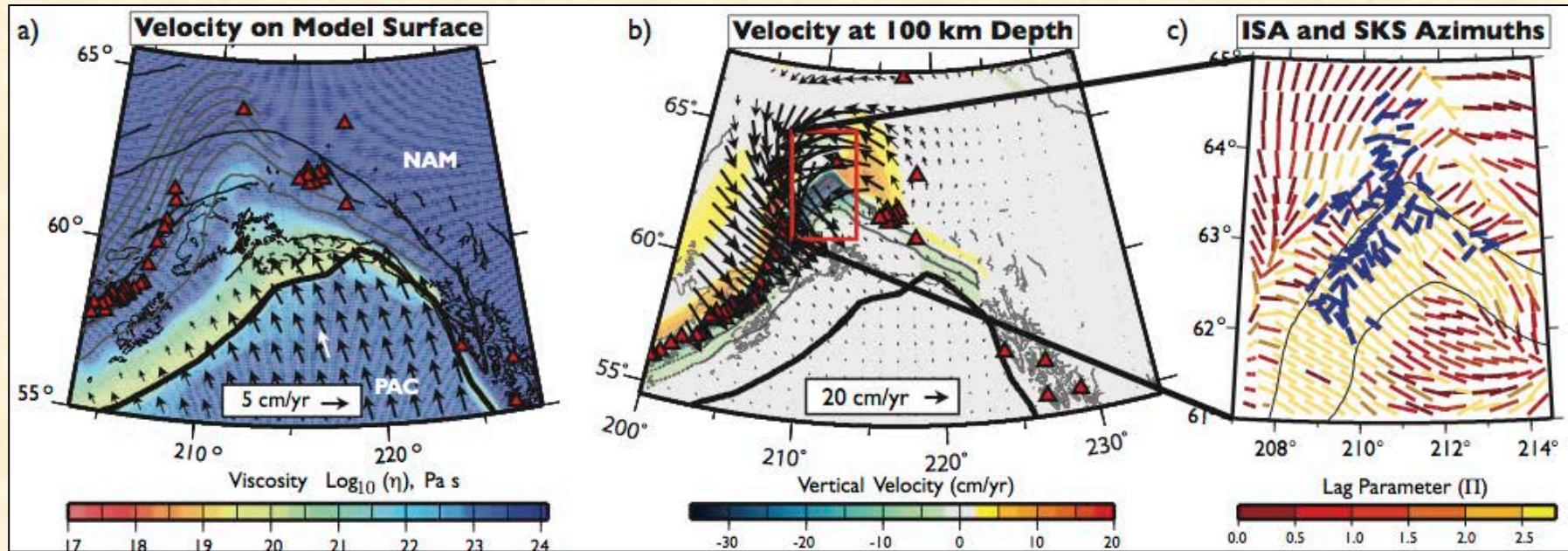
# Results: Rheology and 3D Flow Around Alaska Slab Edge



# Results: Decreased Viscosity as a Function of Slab Strength

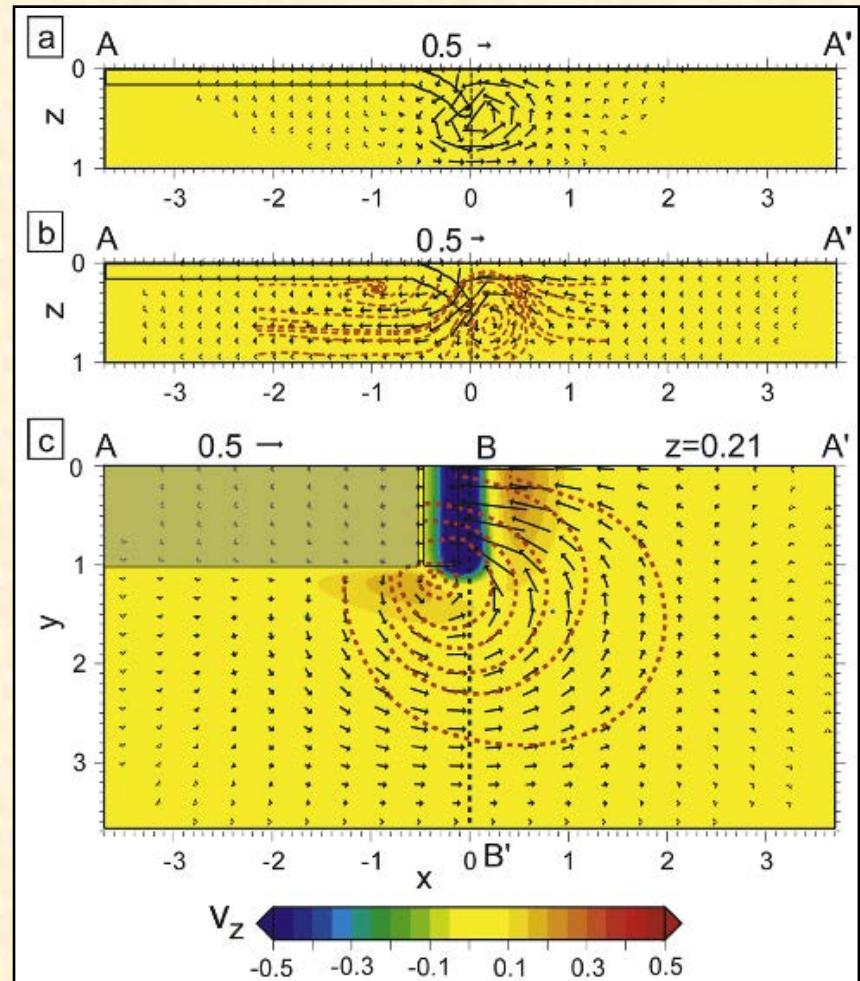


# Results: Differential Plate-Mantle Motion and SKS Splitting

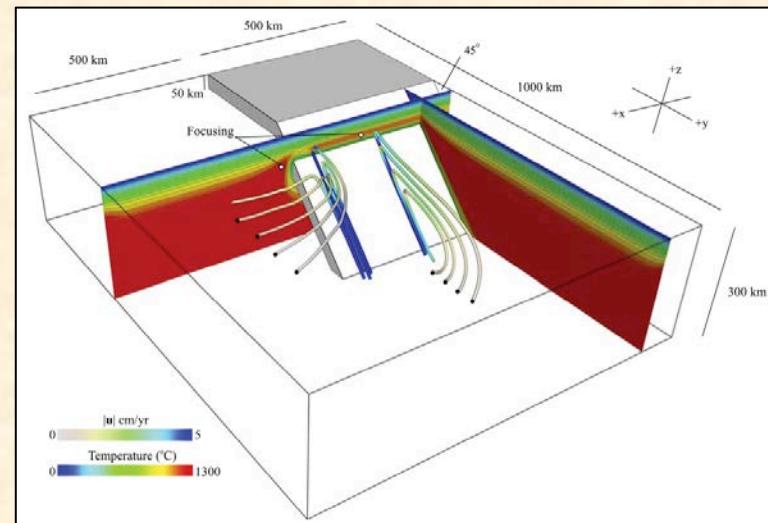


Jadamec and Billen, Nature 2010; Jadamec and Billen, JGR 2012; SKS from Christensen and Abers, 2010

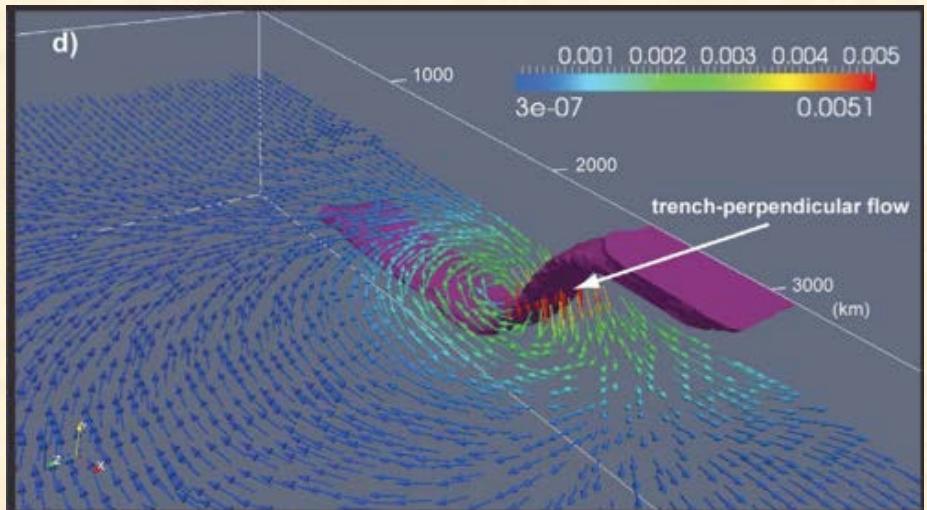
# A Lateral Gradient in Velocity Consistent with Previous Models



Piromallo et al., GRL 2006

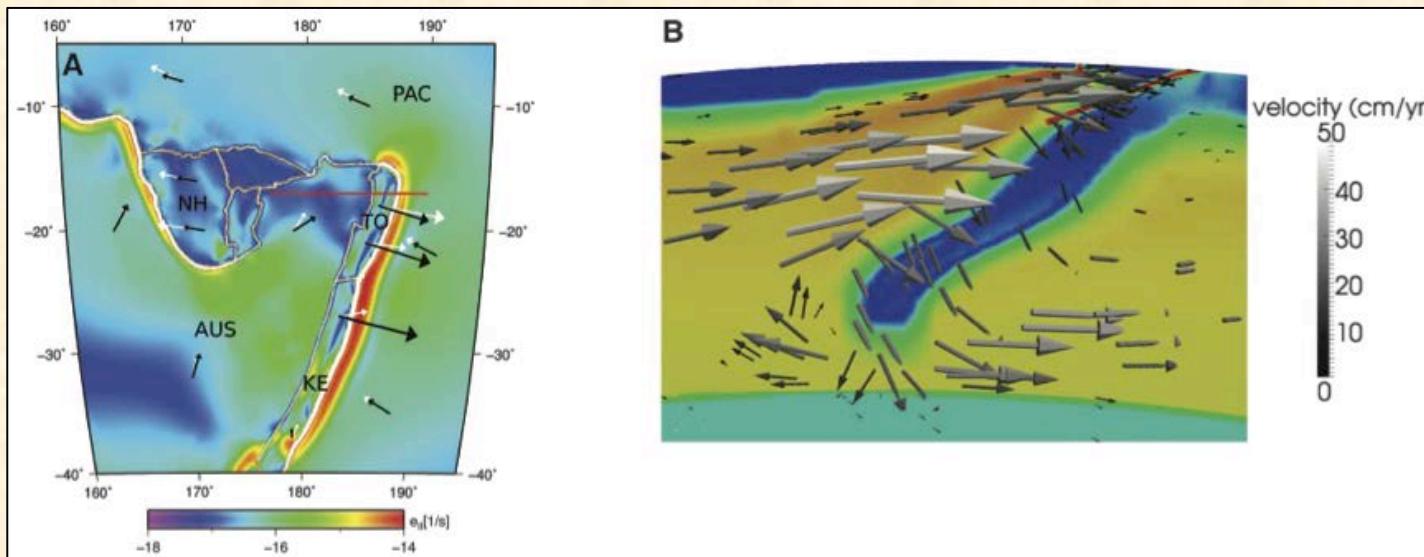


Kneller and van Keken, G<sup>3</sup> 2007

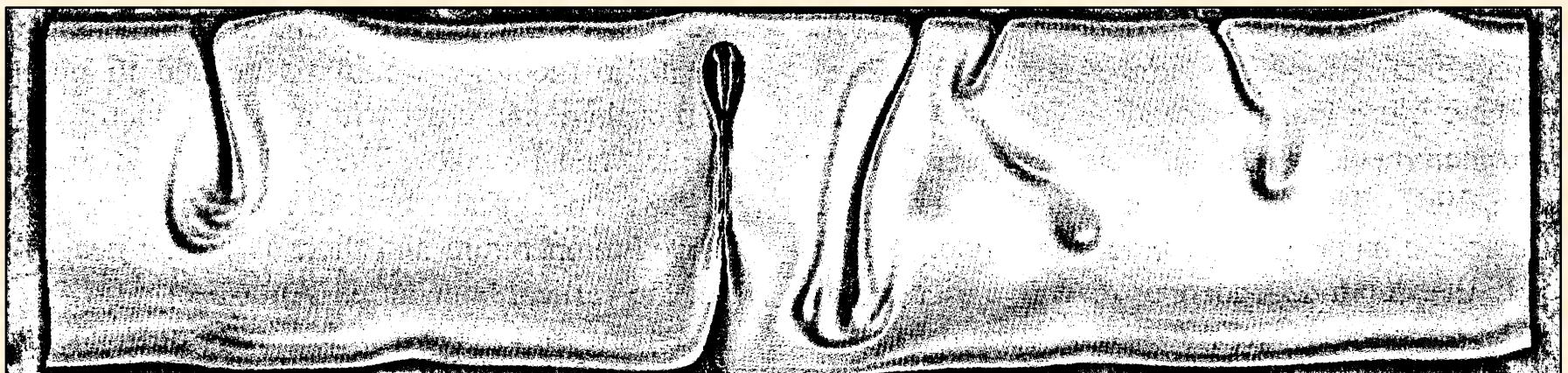


Faccenda and Capitanio, GRL, 2012

# Large Velocity Magnitudes in Global Models and Plume Studies

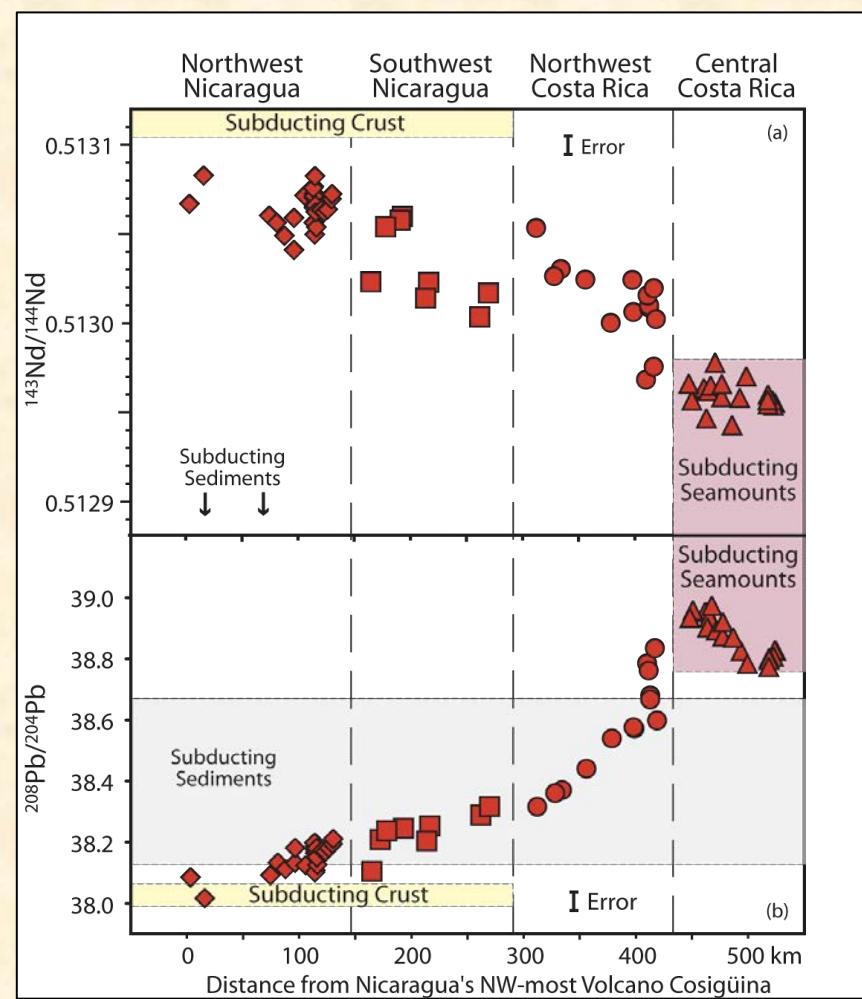
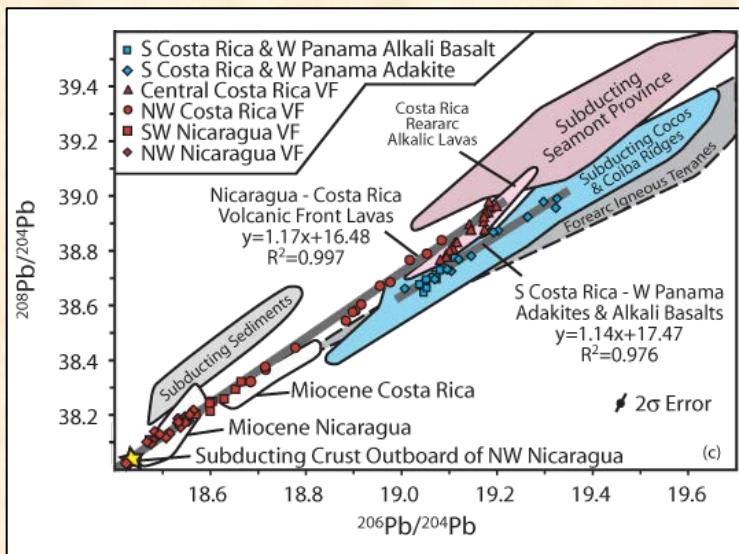
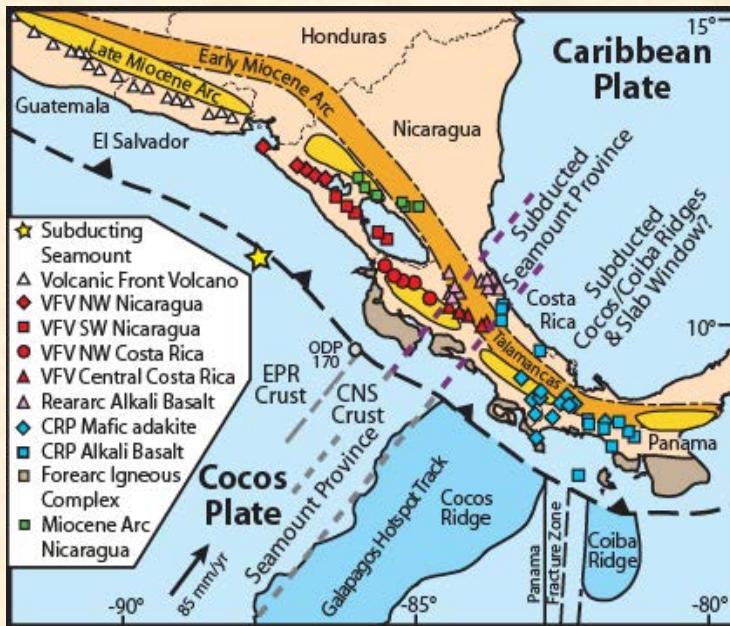


Stadler et al., Science, 2010



Larsen et al., Tectonophysics, 1999

# Independent Observational Constraints on Mantle Flow Rates

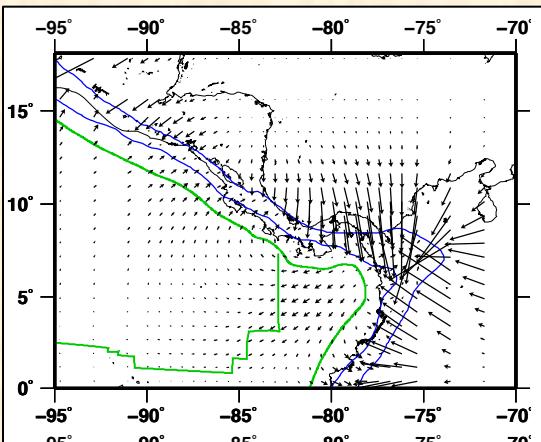


Hoernle et al., Nature, 2008

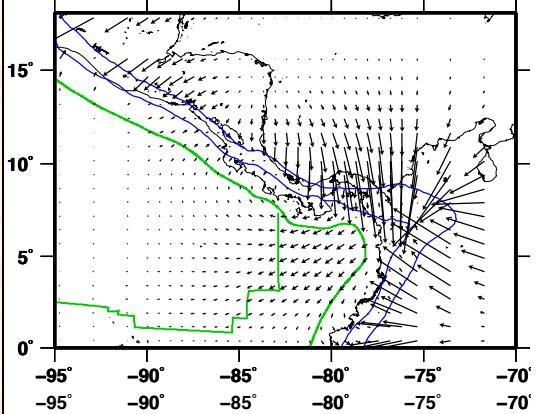
# Predicted Mantle Flow Field in Central America System

No Gap Model:

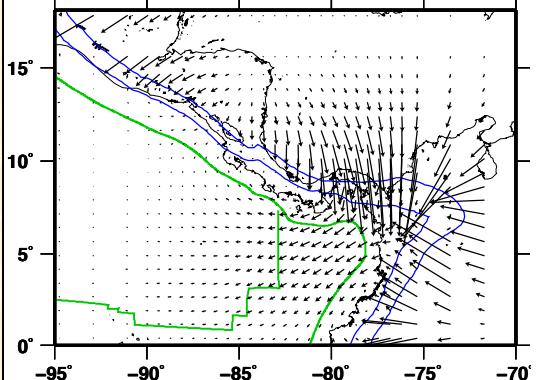
100 km depth



120 km depth

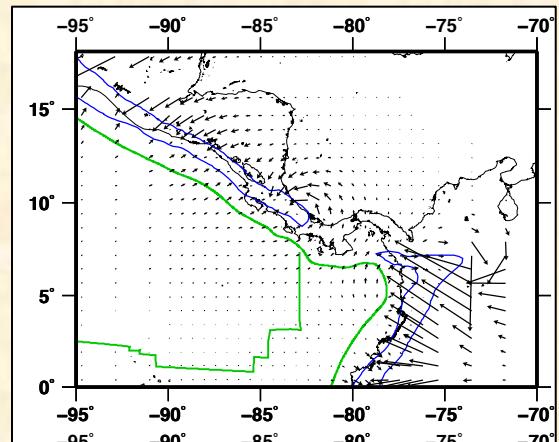


140 km depth

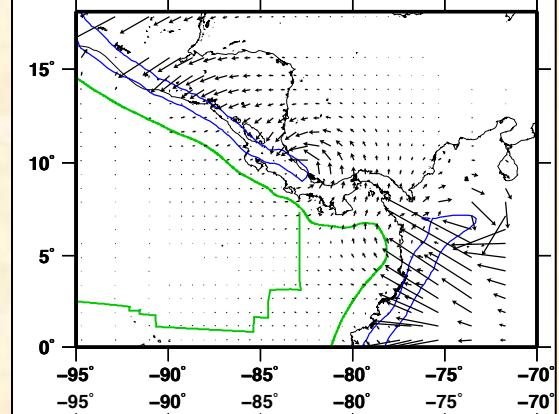


Gap Model:

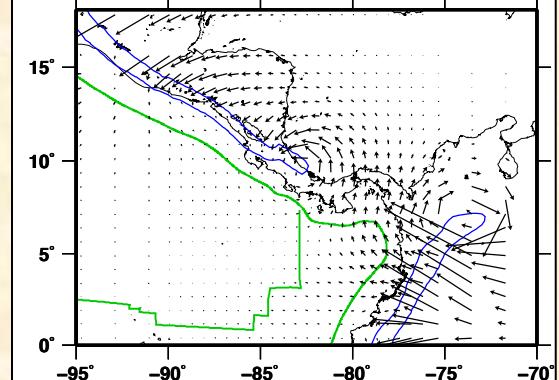
100 km depth



120 km depth

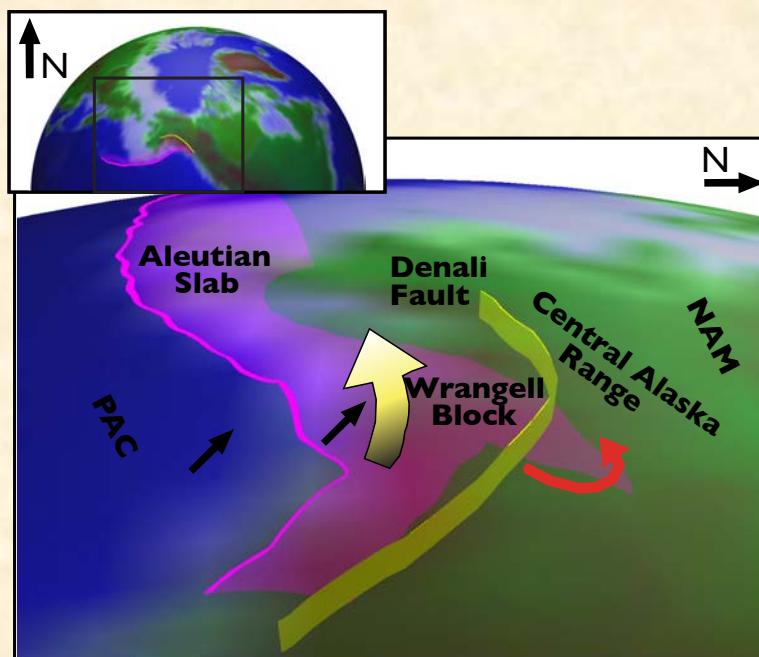


140 km depth



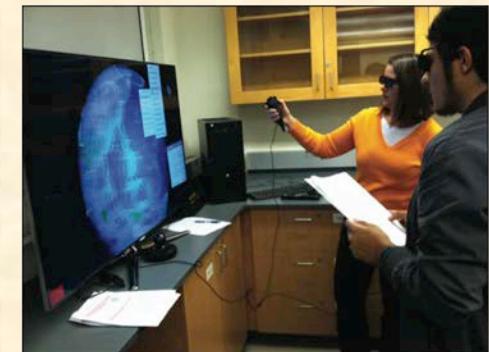
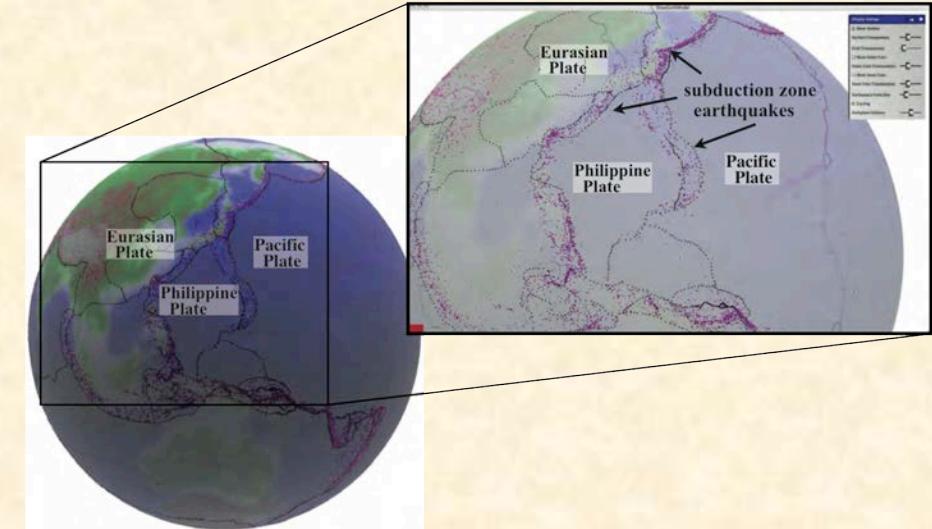
# Conclusions & Looking forward

- 3D framework – slab driving deformation in lithosphere and mantle
- Power law (stress-dependent viscosity) decouples mantle from plates in subduction zones, leading to mantle flow rates over 10X plate motions, questions fixing slab velocity to plate motions
- Incorporation of geophysical complexity and large viscosity variations have high computational costs



- Software and Hardware to render spatial complexities and Gigabytes of data
- Incorporation of disparate data sets, uncertainty quantification
- Data storage, archiving, libraries, code repositories, version control

# Conclusions & Looking forward



Interactive Scientific Data Visualization:  
Upper Left: KeckCAVES (UC Davis)  
Lower Left: 3DALIVE (Monash)  
Upper Right: In-Office (Brown)

# Thank You

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