



Volkswagen**Stiftung**

CIG/QUEST/IRIS Joint Workshop on
Seismic Imaging of Structure and Source
July 14-17, 2013, Fairbanks, Alaska

Rapid CAD and tetrahedral mesh generation for dynamic rupture problems



**Christian Pelties,
Cameron Smith,
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Alice Gabriel**



SeisSol - Project overview



Coordination, Host, Physics,
Numerics, Algorithm, Pre- and
Postprocessing, Application,
User support



Consulting, Scaling,
BlueGene/Q adaption



Automated CAD generation



Meshing, CAD generation



Technical development, HPC,
Optimization, Visualization, Design



Visualization, parallel I/O



Caltech



Barcelona
Supercomputing
Center

Centro Nacional de Supercomputación



...and others ...

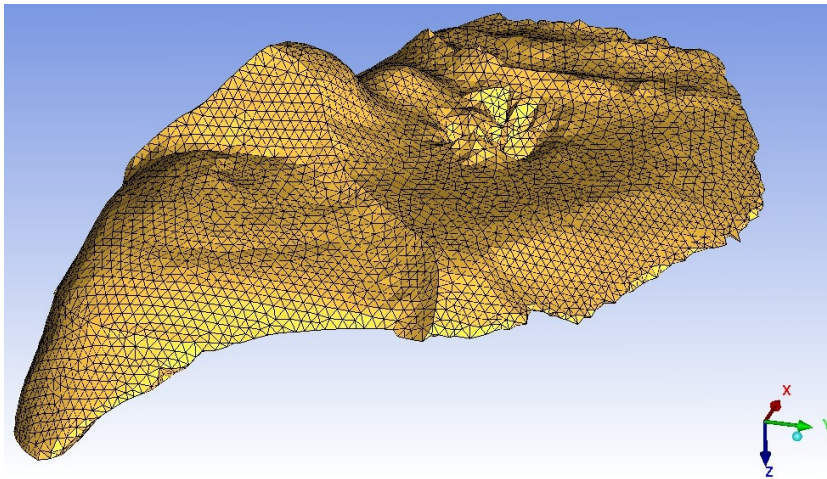
Support, Guidance,
Experience sharing, Consulting, ...

Goal

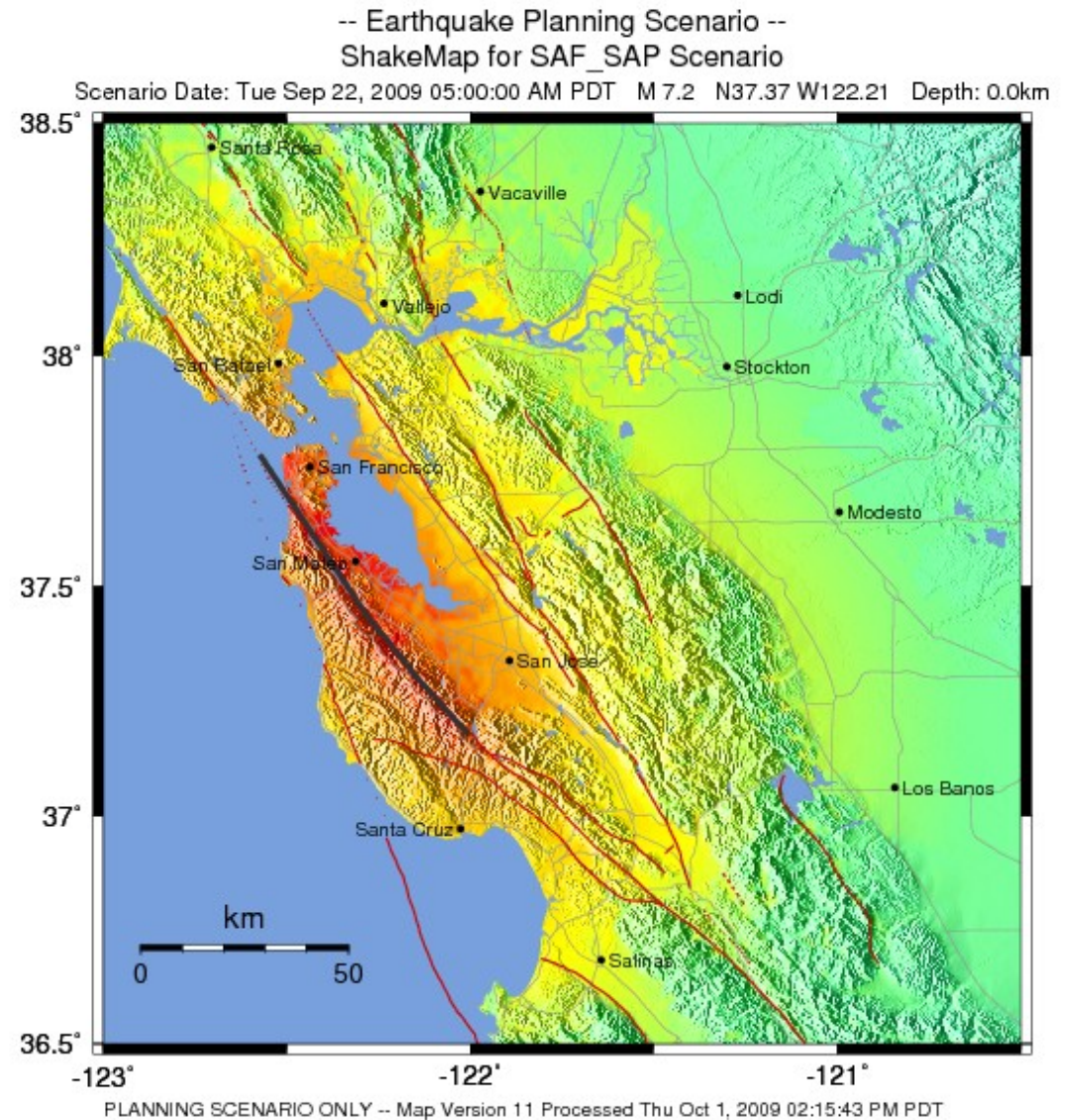
Complete seismic wave propagation package including solutions for

- dynamic rupture simulations
- exploration industry
- **Seismology**

with complex geometry and heterogeneous medium.



Käser, Martin, Christian Pelties, E. Cristobal Castro, Hugues Djikpesse, and Michael Prange (2010), **Wave Field Modeling in Exploration Seismology Using the Discontinuous Galerkin Finite Element Method on HPC-infrastructure**, *The Leading Edge*

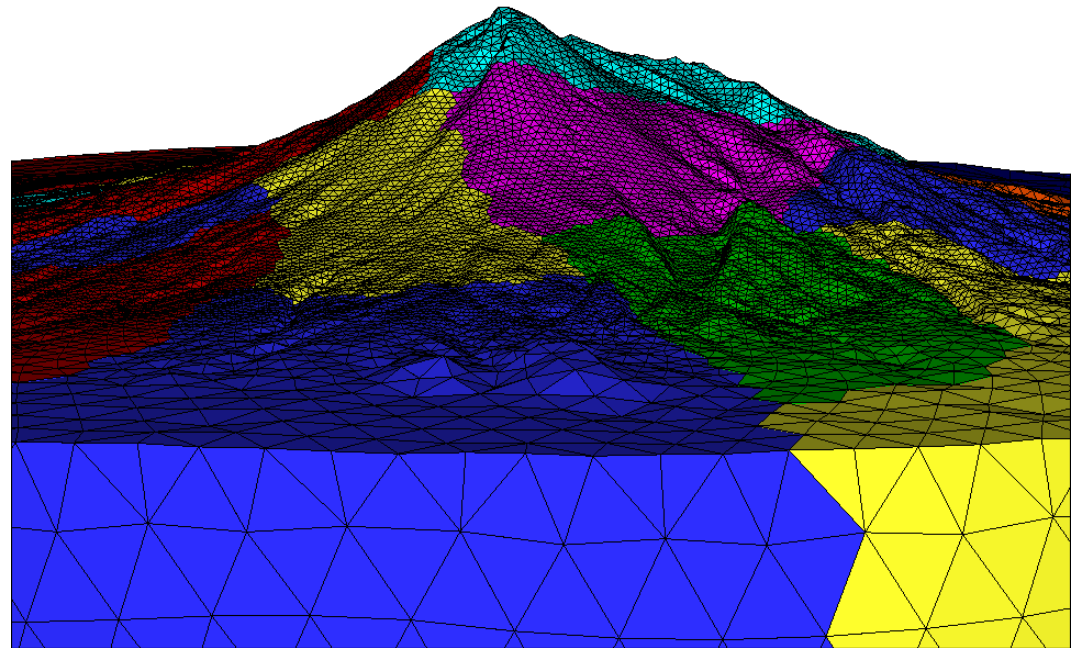
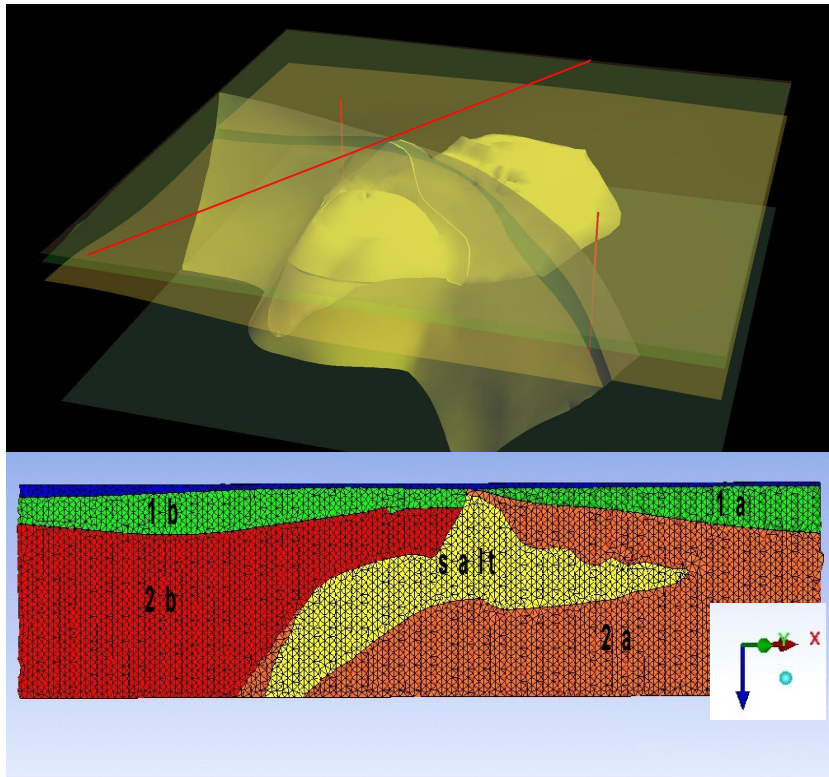


Warmer colors
= higher intensity

Requirements for solver

What do we need for this?

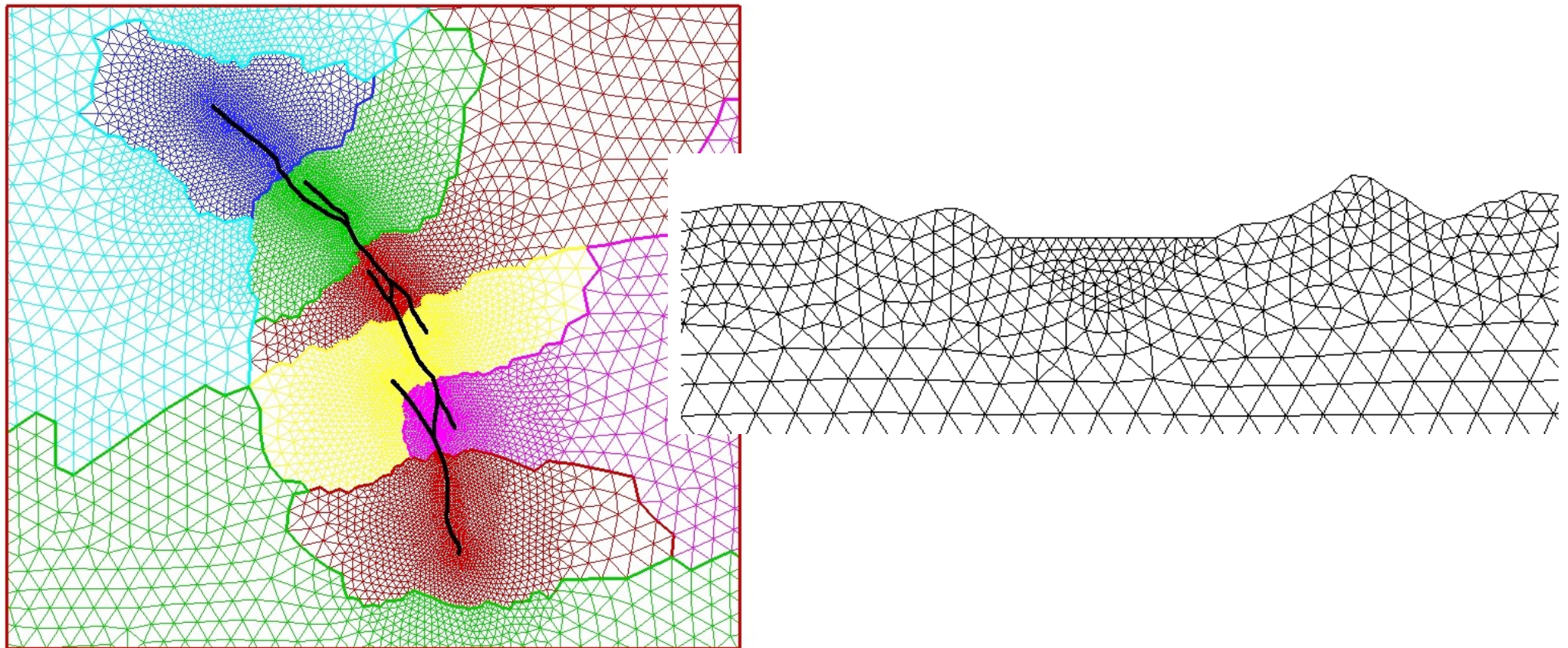
- Accurate numerical methods for reliable results (num. errors, boundary-, initial conditions)
- Proper geometry representation (topography, material interfaces)
- Use of acoustic, elastic, viscoelastic, and anisotropic material to approximate realistic geological subsurface properties
- Scalability on HPC architecture to tackle big problems with high frequency



(Merapi model)

Advantages of the ADER-DG Method

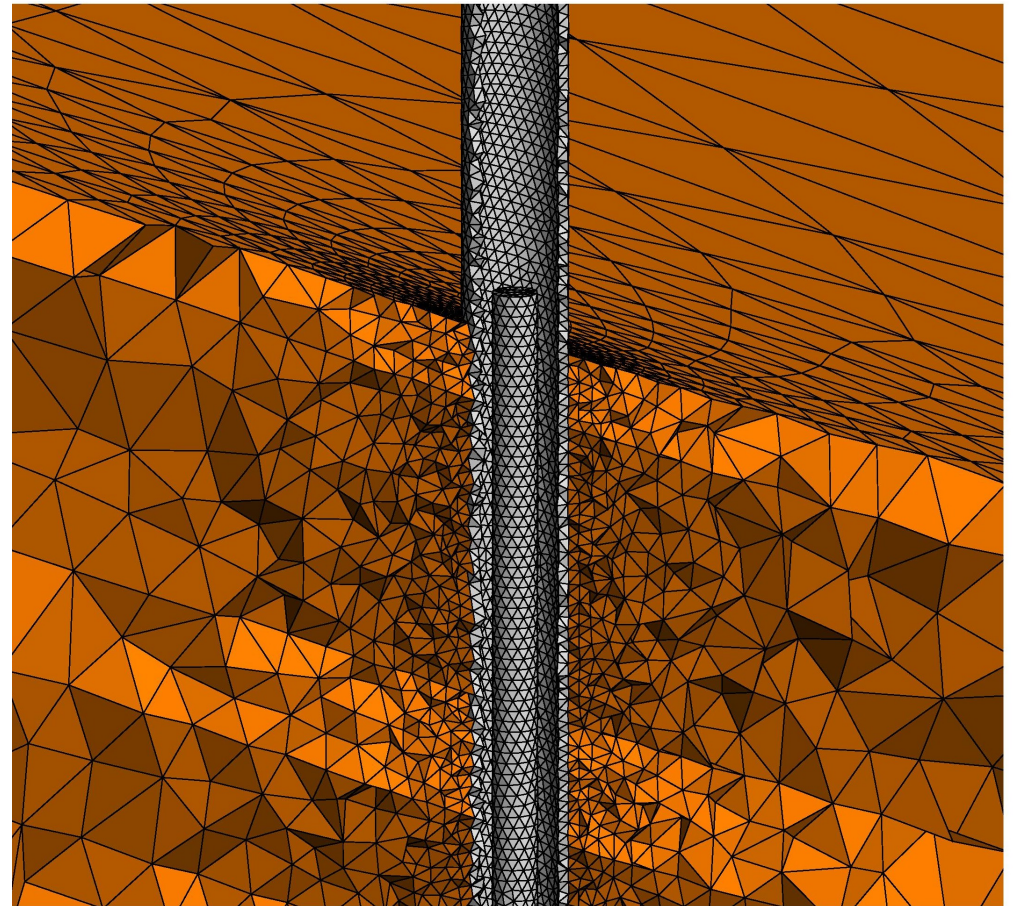
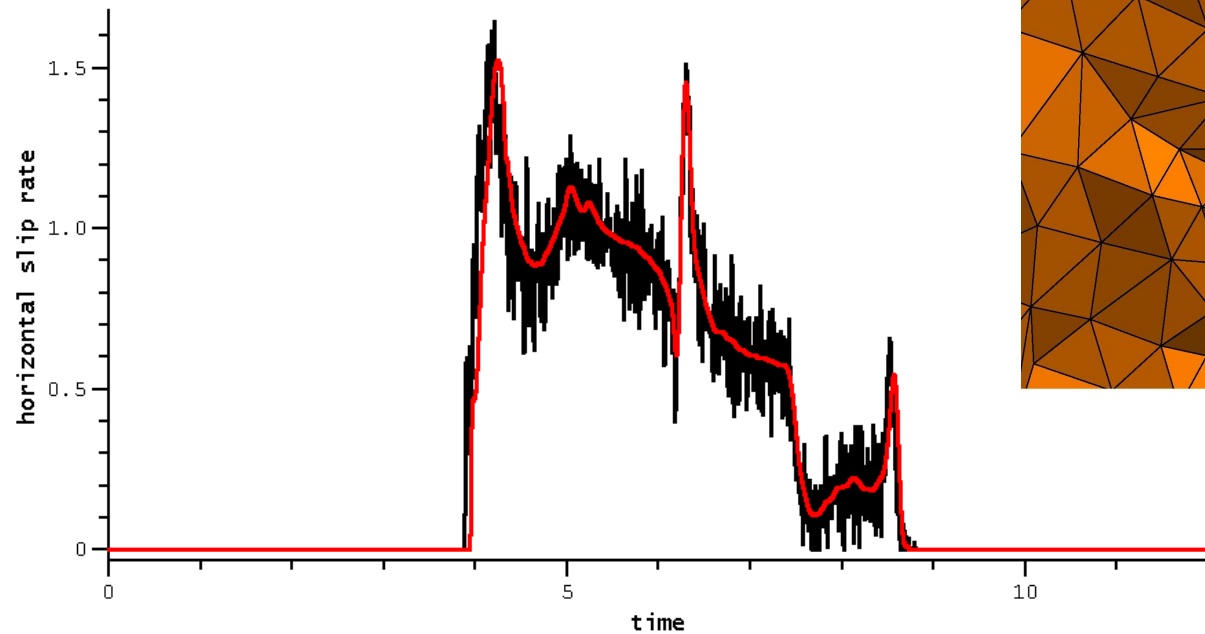
- Enables use of unstructured meshes – low velocity basins, curved or kinked faults, branching, surface rupture, fault interaction
- Mesh coarsening – adjustment of resolution
- High-order accurate simulation of the wave propagation including heterogeneous media and topography



Advantages of the ADER-DG Method

- ADER high-order time integration with local time stepping
- High-accurate results of the rupture process: Oscillation free dynamic rupture

SEM vs ADER-DG



Mathematical Model

Elastic Wave Equation as a Linear Hyperbolic System:

Vector-matrix notation:

$$\frac{\partial Q_p}{\partial t} + A_{pq} \frac{\partial Q_q}{\partial x} + B_{pq} \frac{\partial Q_q}{\partial y} + C_{pq} \frac{\partial Q_q}{\partial z} = S_p$$

Velocity-stress formulation:

$$\text{3D: } Q = (\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy}, \sigma_{yz}, \sigma_{xz}, u, v, w)^T$$

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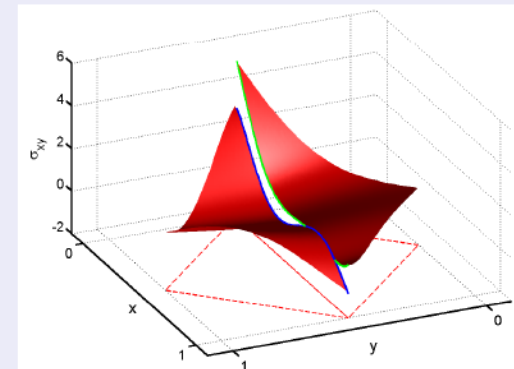
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$$3D: \quad Q = (\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy}, \sigma_{yz}, \sigma_{xz}, u, v, w)^T$$

Numerical Approximation of the solution

$$\left(Q_h^{(m)} \right)_p (\xi, \eta, \zeta, t) = \hat{Q}_{pl}^{(m)}(t) \Phi_l(\xi, \eta, \zeta)$$

- Φ_l are orthogonal basis functions
- the mass matrix is diagonal



Discontinuous Galerkin Approach – Flux computation

Flux computation

Exact Riemann solver is used to compute the state at the interfaces by upwinding:

$$\begin{aligned} F_p^h &= \frac{1}{2} T_{pq} \left(A_{qr}^{(m)} + \left| A_{qr}^{(m)} \right| \right) (T_{rs})^{-1} \hat{Q}_{sl}^{(m)} \Phi_l^{(m)} \\ &+ \frac{1}{2} T_{pq} \left(A_{qr}^{(m)} - \left| A_{qr}^{(m)} \right| \right) (T_{rs})^{-1} \hat{Q}_{sl}^{(m_j)} \Phi_l^{(m_j)} \end{aligned}$$

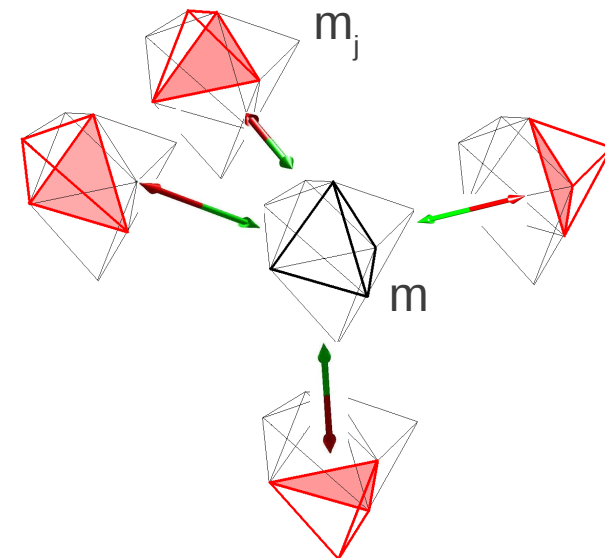
Computation of the line integrals:

- Pre-computed analytically
- Gauss-Legendre integration

➡ Opens up new possibilities:
non-conforming meshes, dynamic rupture source type

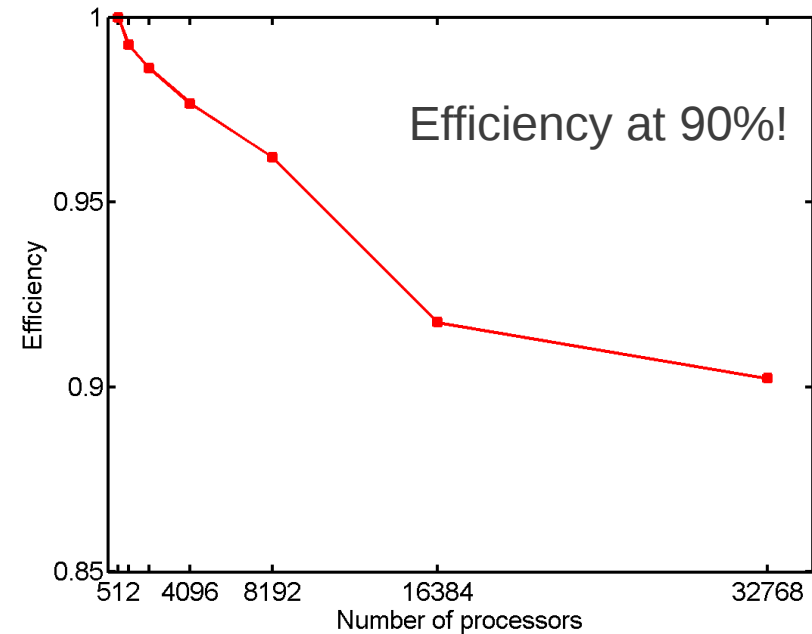
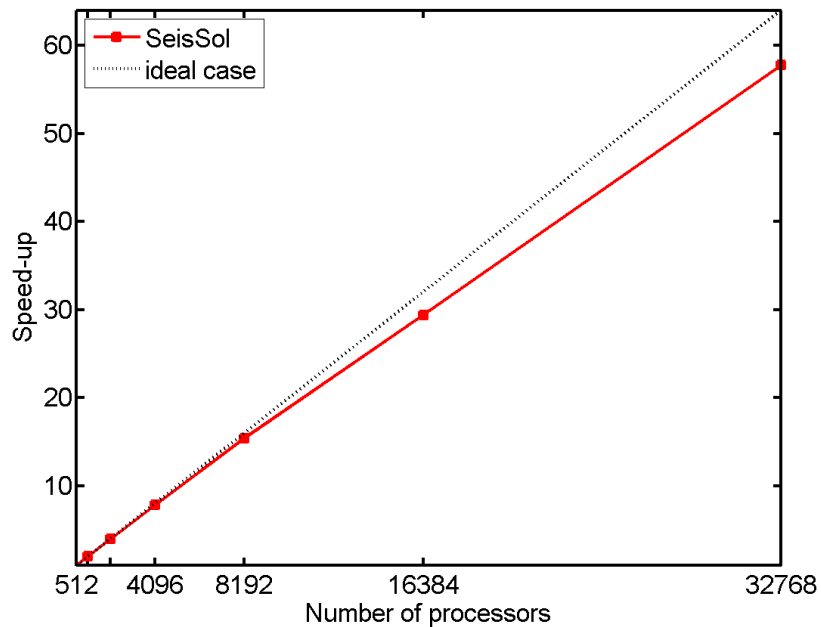
Locality of the computations:

only directly neighboring elements are required to exchange data, which leads to small communication times for parallel calculations



Suitability for large scale HPC infrastructure

Efficiency on the BlueGene/P machine Shaheen at KAUST



- 7,7 Mio. Elements
- Order of accuracy in space and time: O5
- Pure MPI parallelization – code is openMP hybrid now
- Metis partitioning

<http://glaros.dtc.umn.edu/gkhome/metis/metis/overview>

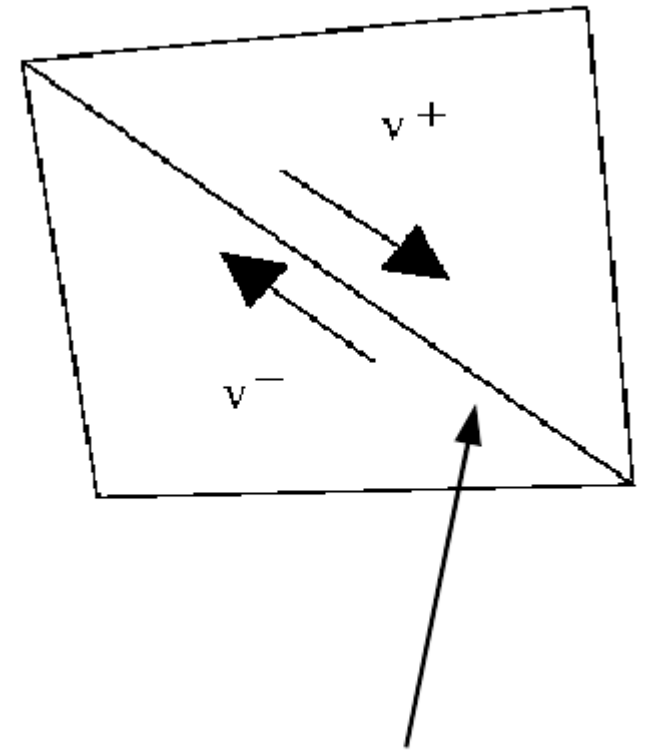
Dynamic Earthquake rupture

Incorporate source process

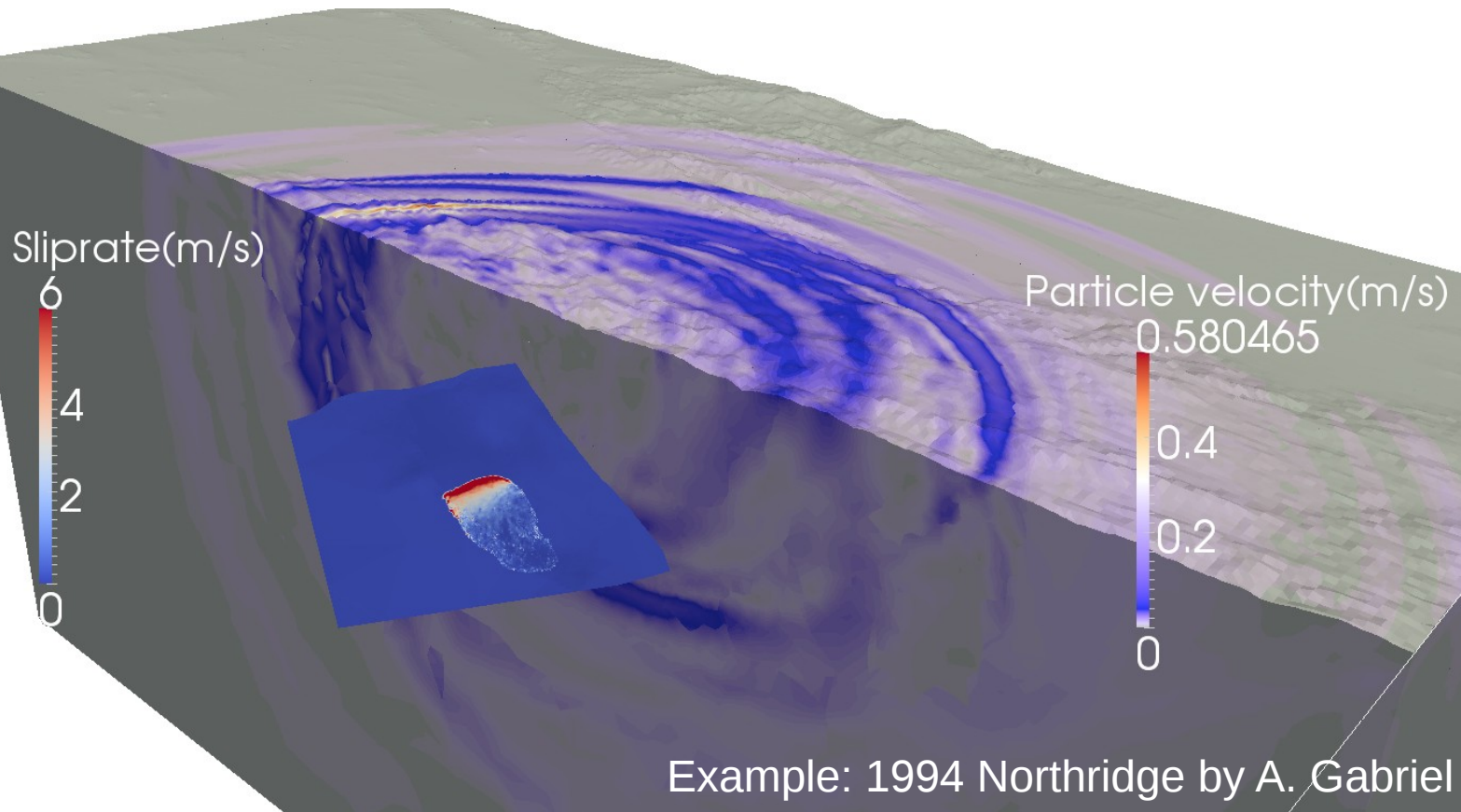
- To understand earthquake faulting
- Support physics-based ground motion prediction

Treat dynamic rupture as an interior time-dependent 'boundary condition' using the flux term!

- Impose new traction following the failure criterion
- Impose fault parallel velocities in opposite directions



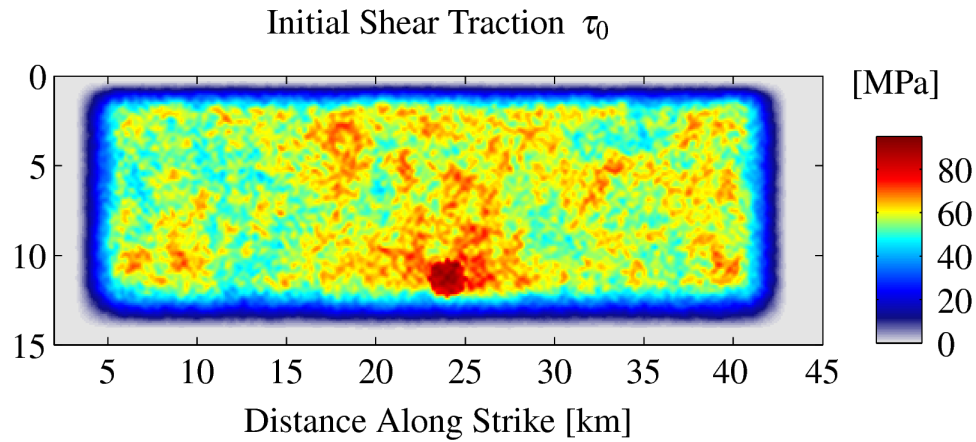
fault between two elements



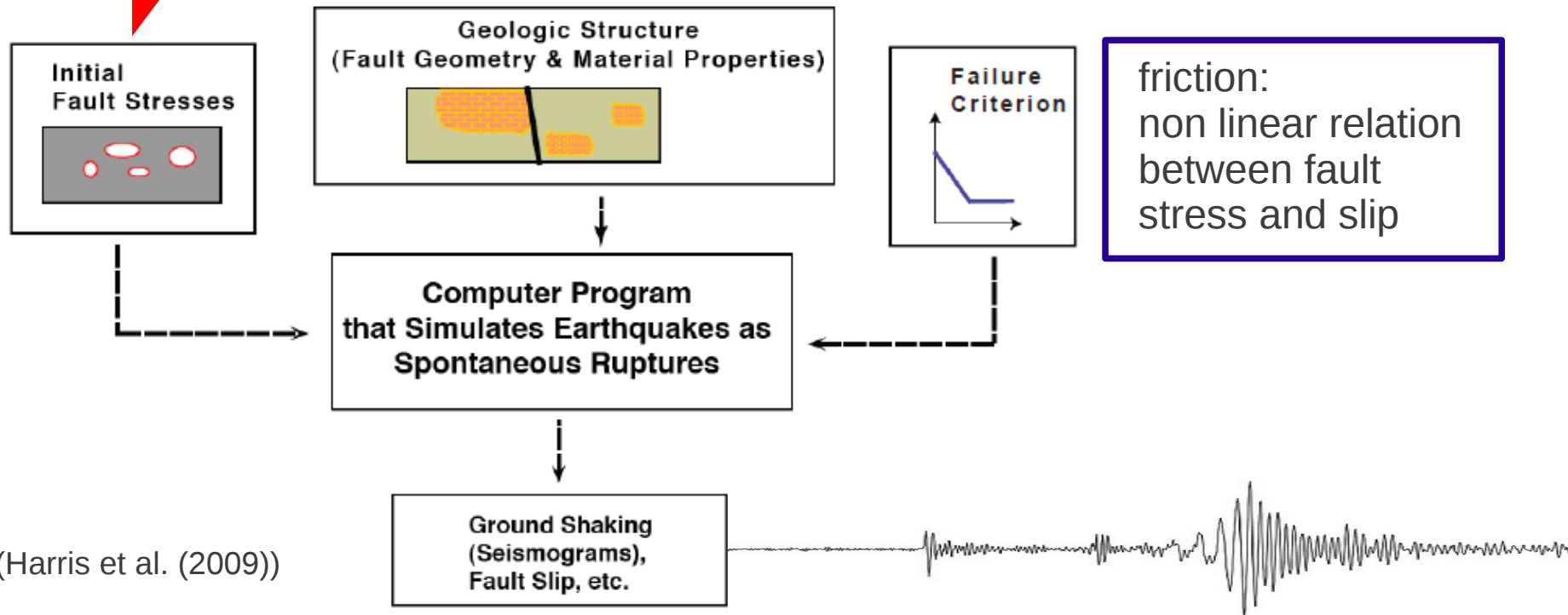
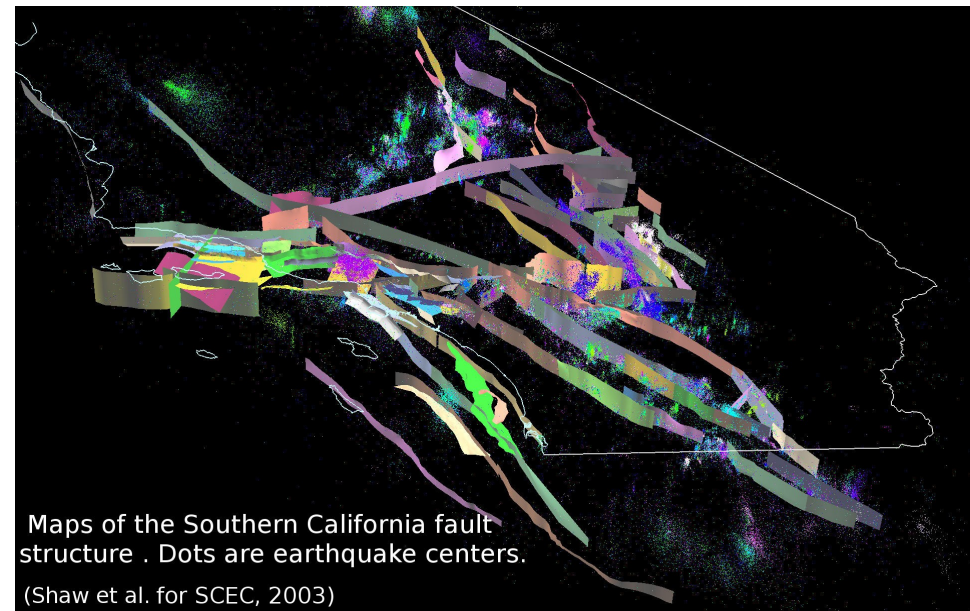
Example: 1994 Northridge by A. Gabriel

Ingredients

Distance Down Dip [km]



(Brietzke et al. (2009))



Failure criterion:

Coulomb friction model

$$|\sigma_{xy}| \leq \mu_f \sigma$$

traction fault strength

$$(|\sigma_{xy}| - \mu_f \sigma) \Delta v = 0$$

σ_{xy} traction

μ_f friction coefficient

σ normal stress

Δv slip rate

Failure criterion:

Coulomb friction model

$$|\sigma_{xy}| \leq \mu_f \sigma$$

traction fault strength

$$(|\sigma_{xy}| - \mu_f \sigma) \Delta v = 0$$

σ_{xy} traction

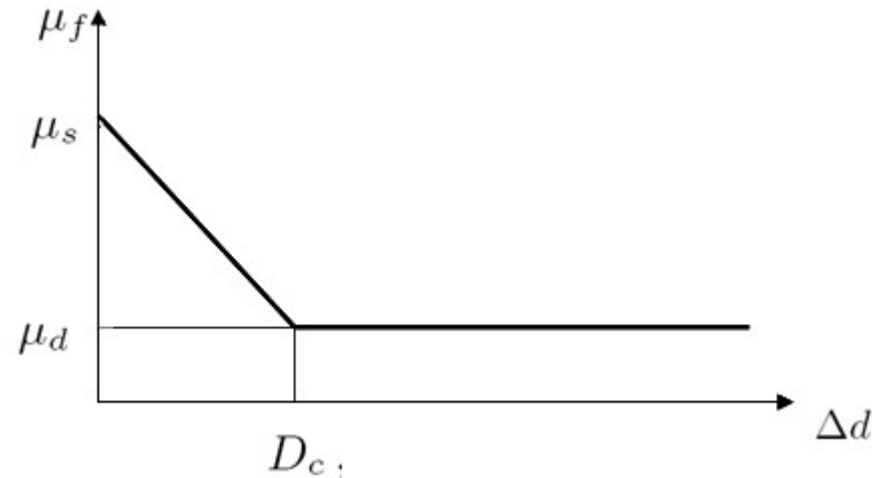
μ_f friction coefficient

σ normal stress

Δv slip rate

Δd slip

D_c critical slip distance



Linear Slip Weakening friction law
(laboratory experiments
– rate-and-state also implemented)

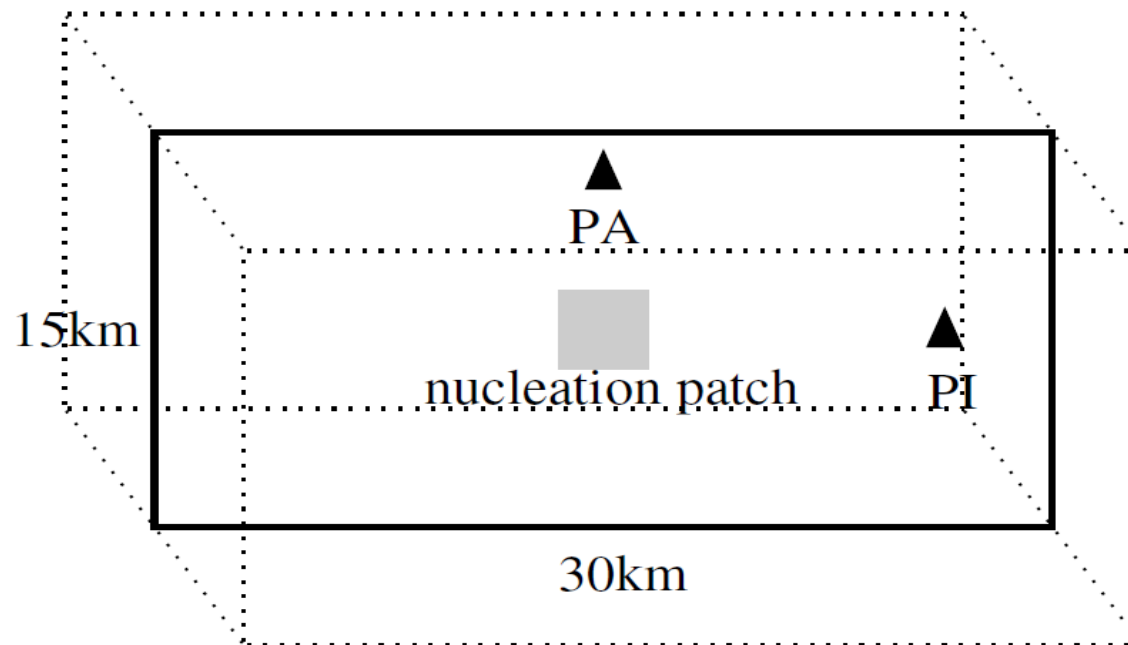
Provides:

- initial rupture
- arrest of sliding
- reactivation of slip

Verification – TPV3 SCEC Test Case

(Harris *et al.*, 2004)

- spontaneous rupture propagation on a straight fault
- homogeneous fullspace
- linear slip weakening friction



Comparison between

ADER-DG method order 4 and 200m triangles at the fault (larger tetrahedrons in bulk)

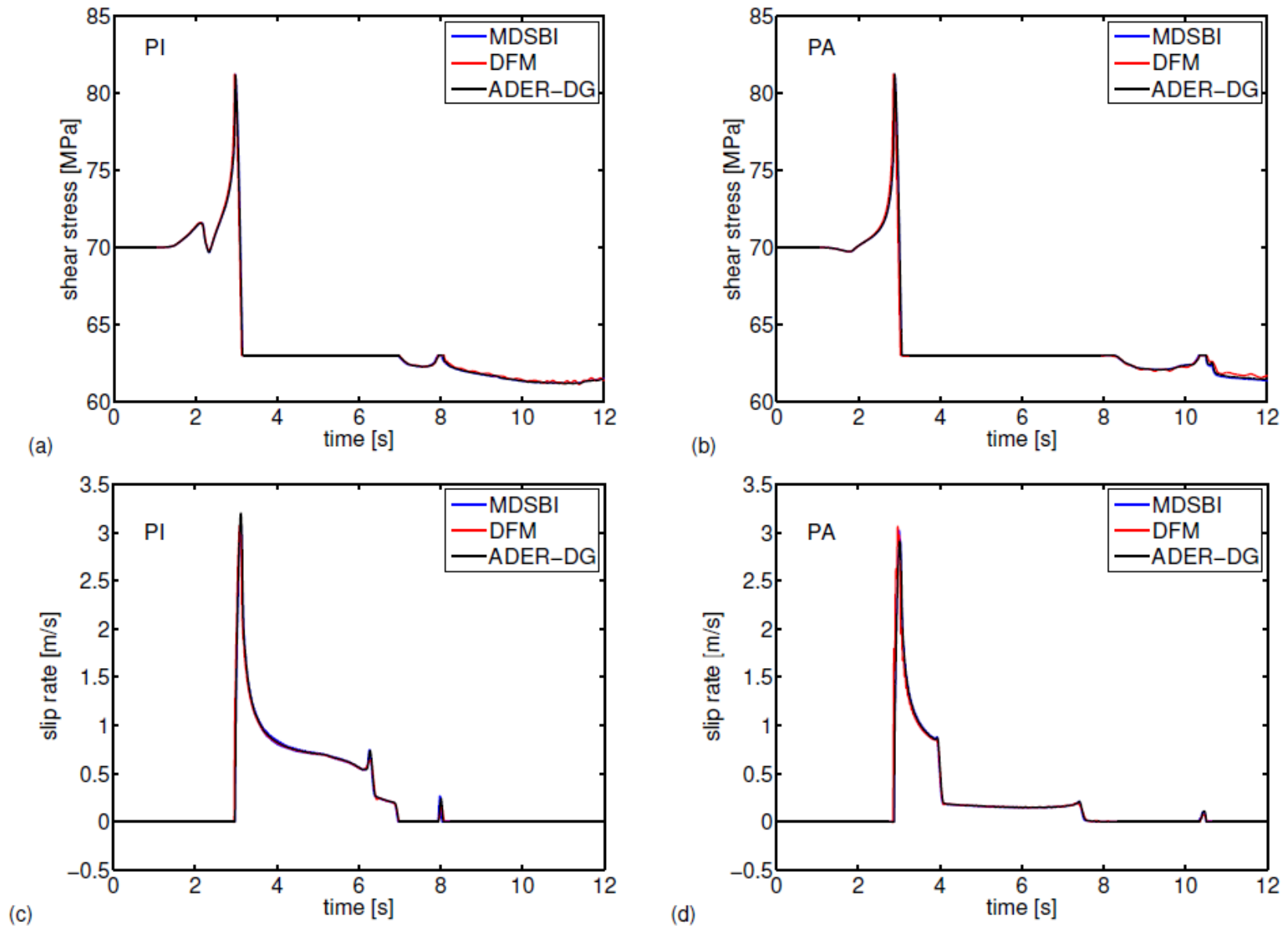
and

DFM - Finite Difference staggered-grid split node order 2 with 50m grid interval

and

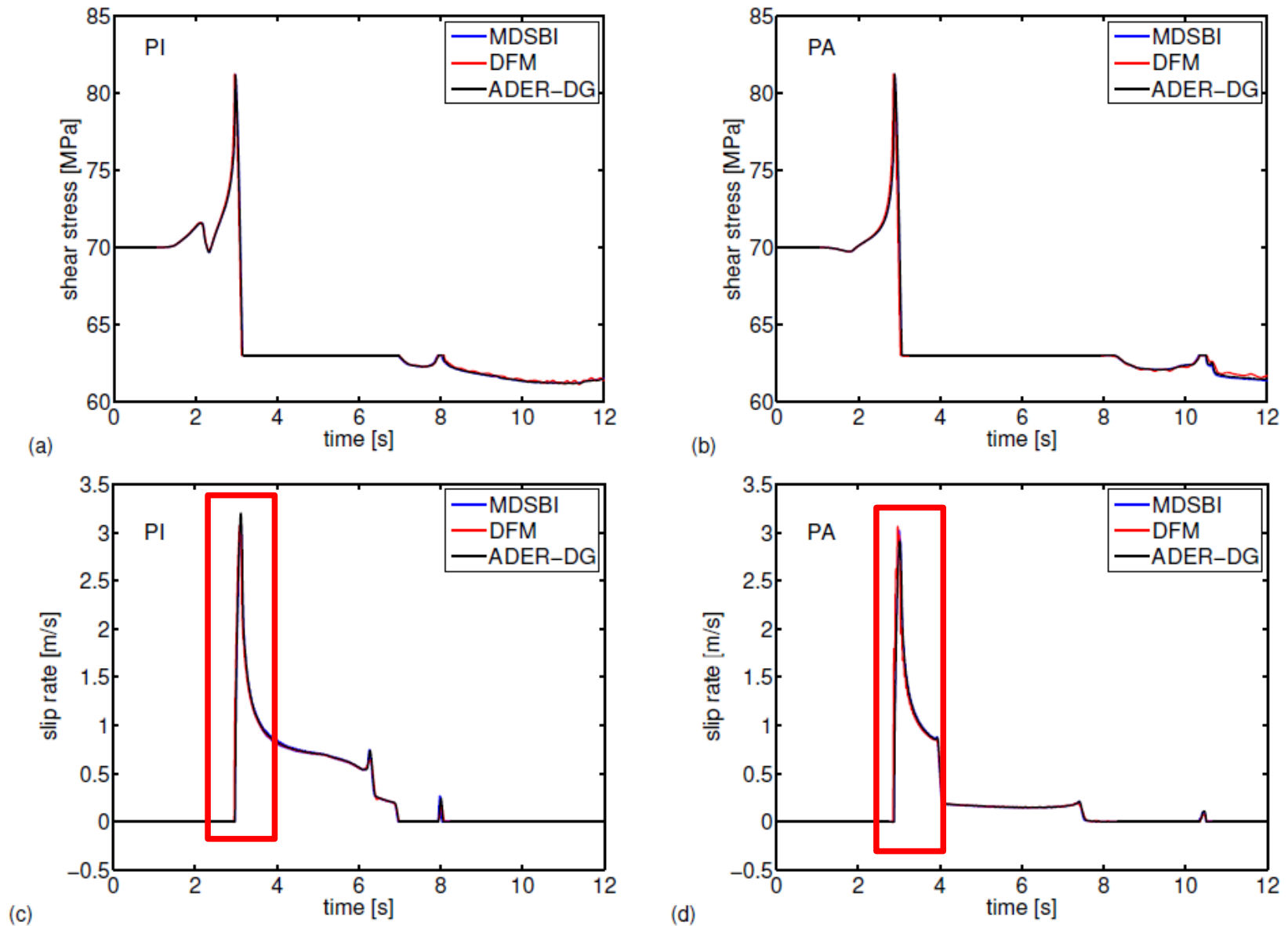
MDSBI - Multidimensional spectral boundary integral with 50m grid interval

Verification – TPV3 SCEC Test Case



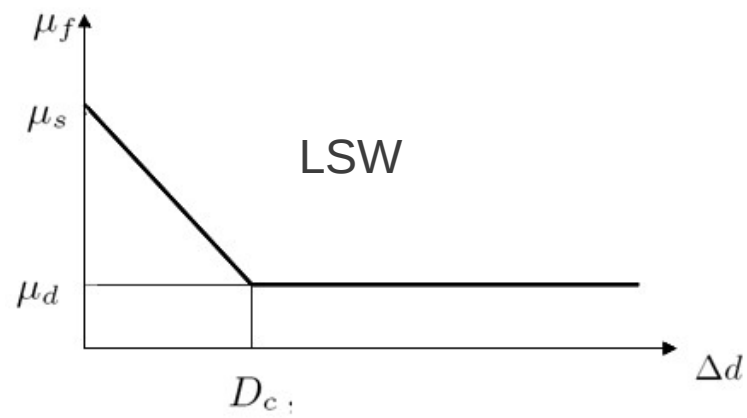
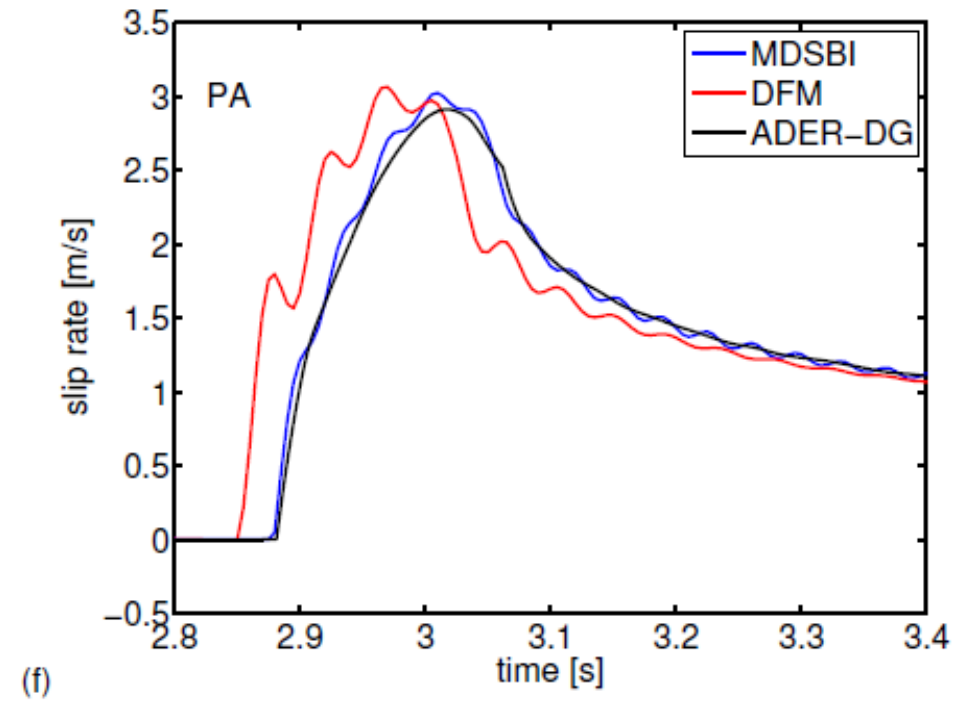
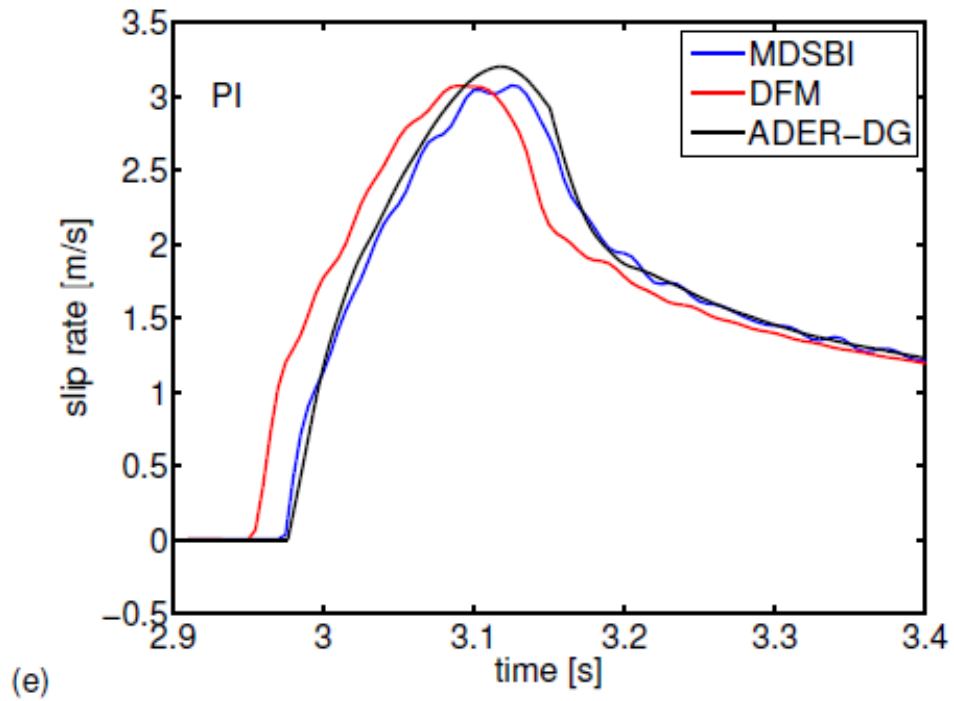
Day, S. M., L. A. Dalguer, N. Lapusta, Y. Liu (2005), Comparison of finite difference and boundary integral solutions to three-dimensional spontaneous rupture, *J. Geophys. Res.*, 110, B12307
DFM data provided by Luis Dalguer. MDSBI data computed with the code of E. Dunham (version 3.9.10).

Verification – TPV3 SCEC Test Case



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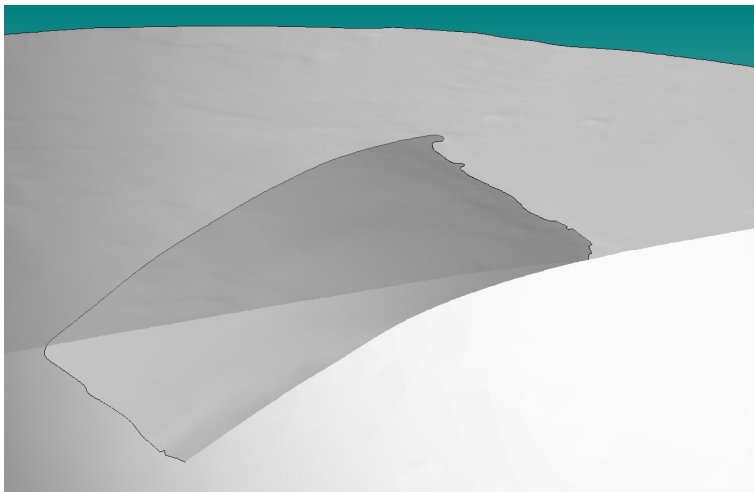
Workflow

From CAD to seismogram...

- Get geometry and model data
- Assemble CAD model
- Create mesh
- Partitioning
- Set model parameters
- Solve physical equation
- Analysis of output

Pre-processing

Post-processing



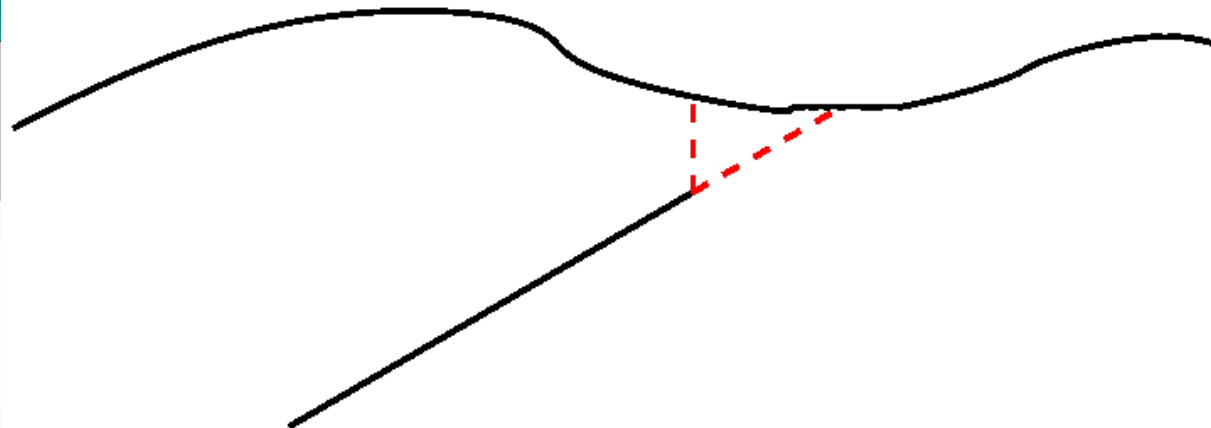
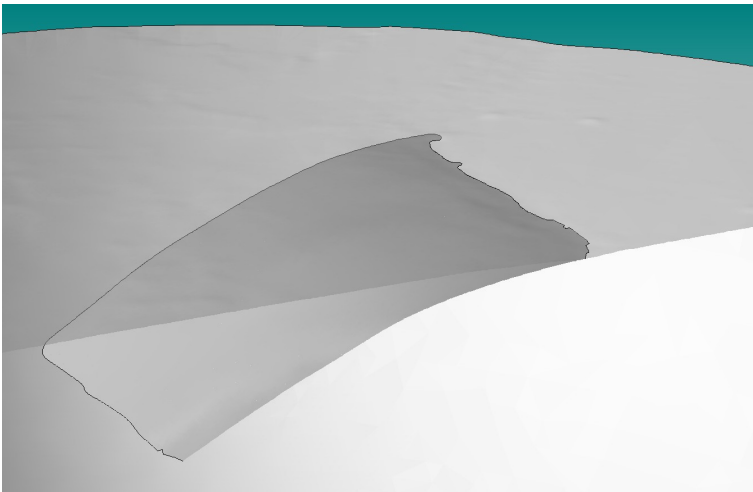
“Time to solution!”

Automated CAD generation

Current bottleneck: CAD generation can easily consume **weeks to month**

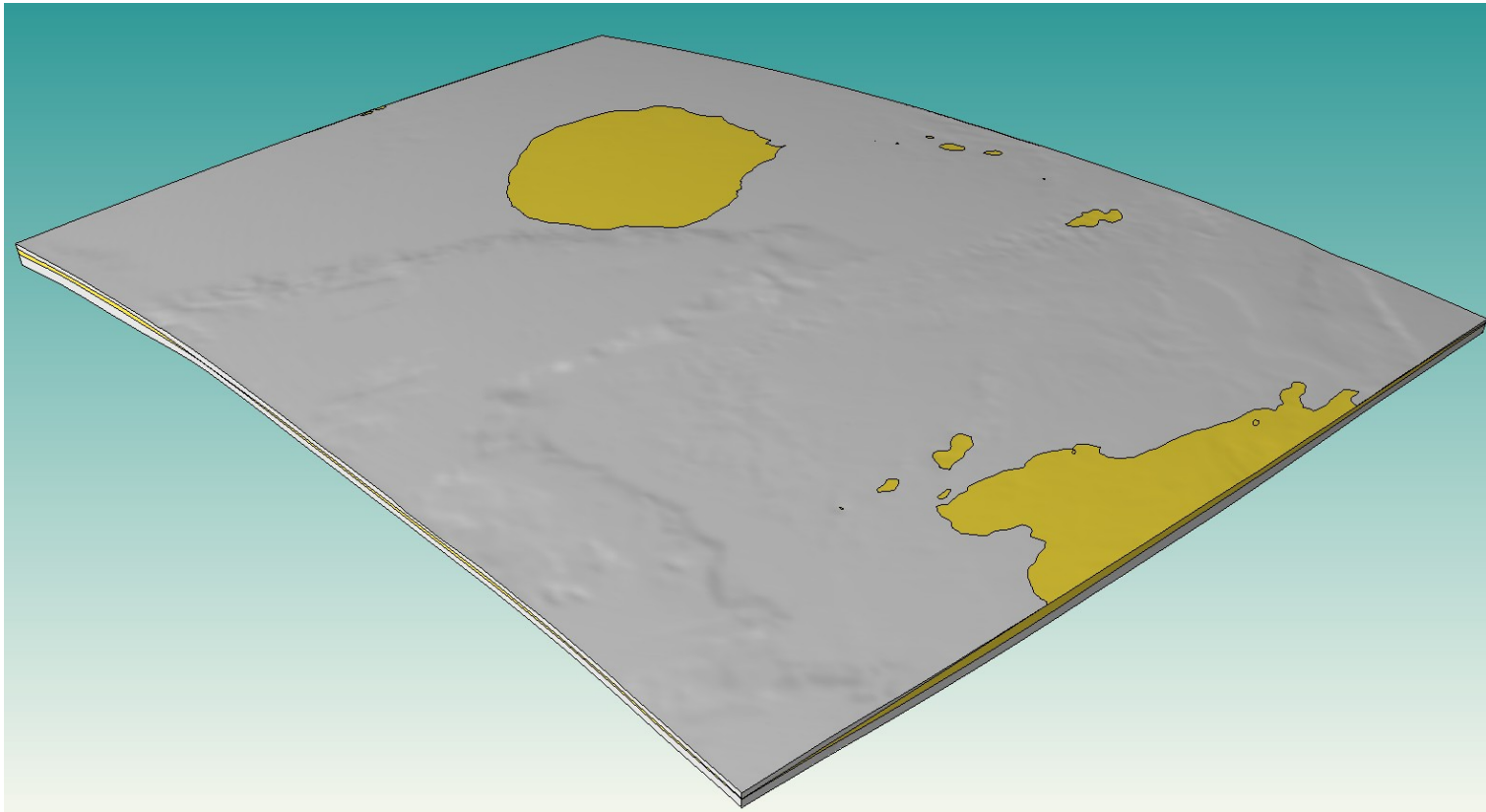
Difficulties:

- Surface reconstruction of different types of initial raw data
- Undulating 3D surfaces that merge under shallow angles, intersect
- Remove non-physical features
- Clip too small features depending on the desired mesh size
- Representation by splines as typically used by (commercial) CAD/mesh software unfortunate for geological data
- Watertight model
- Seamless integration into meshing software (avoid format conversion)



Automated CAD generation – preliminary workflow

1. Download topography/bathymetry, e.g. from NOAA's ETOPO data collection
2. Define bounding box: rectangular or spherical
3. Material interfaces: structured grids of points
4. Faults: structured grids of points, gOcad's TS format
5. Check projection
6. (Triangulated) surface generation: Poisson surface reconstruction (MeshLab)
7. Assemble model: apply union, intersection, trimming operations with Simmetrix discrete modeling tools

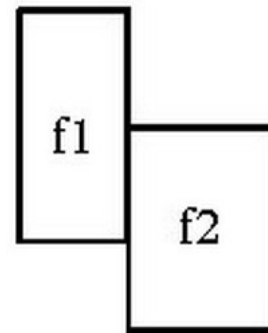


Biscay
model,
S. Wenk

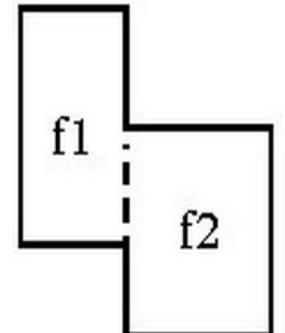
SimModeler

Customized problem definition and mesh generation interface for SeisSol
by **RPI/SCOREC/Simmetrix (C. Smith, M. Shephard)**

- Accepts e.g. Parasolid, ACIS and STL input
- Trims automatically geometry and creates a watertight model
- Meshes with millions of elements in seconds/minutes
- Mesh coarsening/refining
- Handling complex geometries (no violation)
- user-friendly interface
- Quality metrics
- Exports SeisSol format
- Non-manifold geometry required

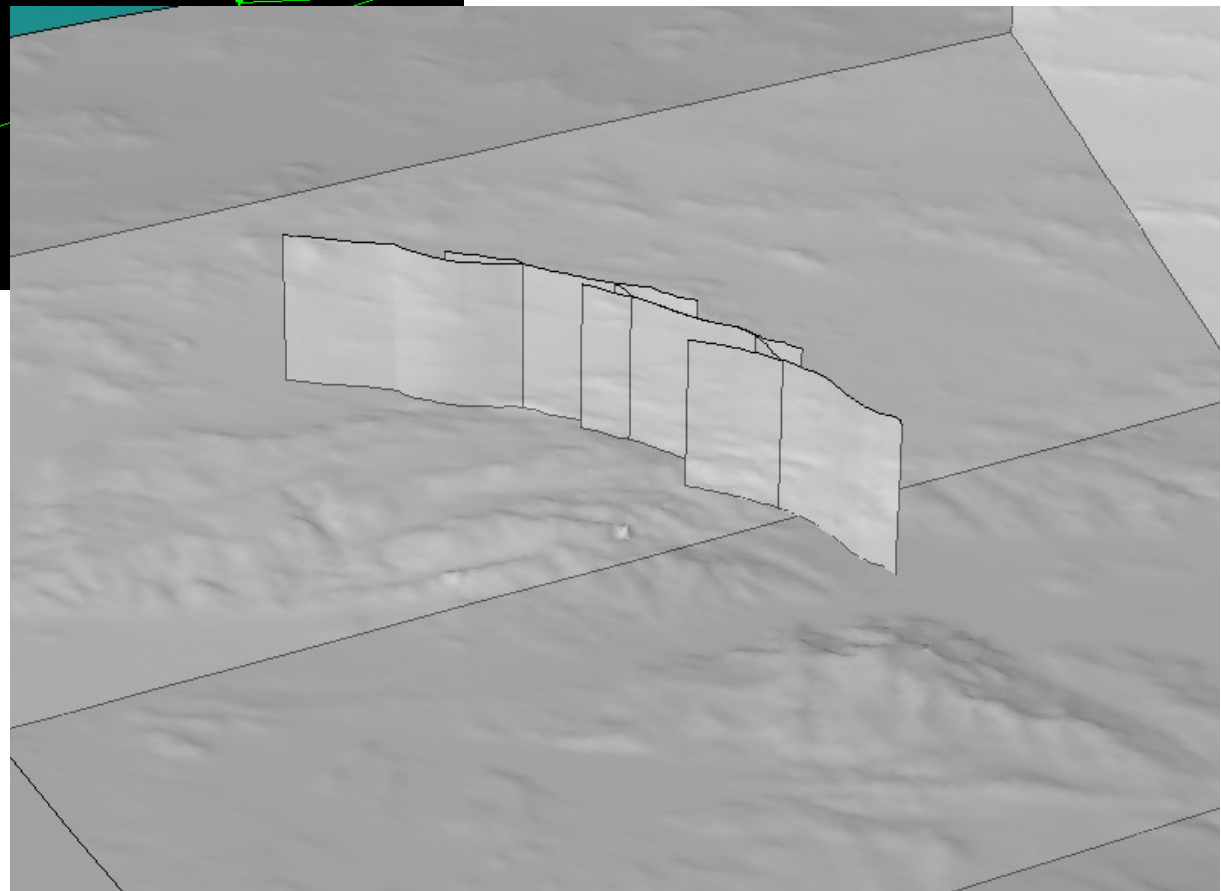
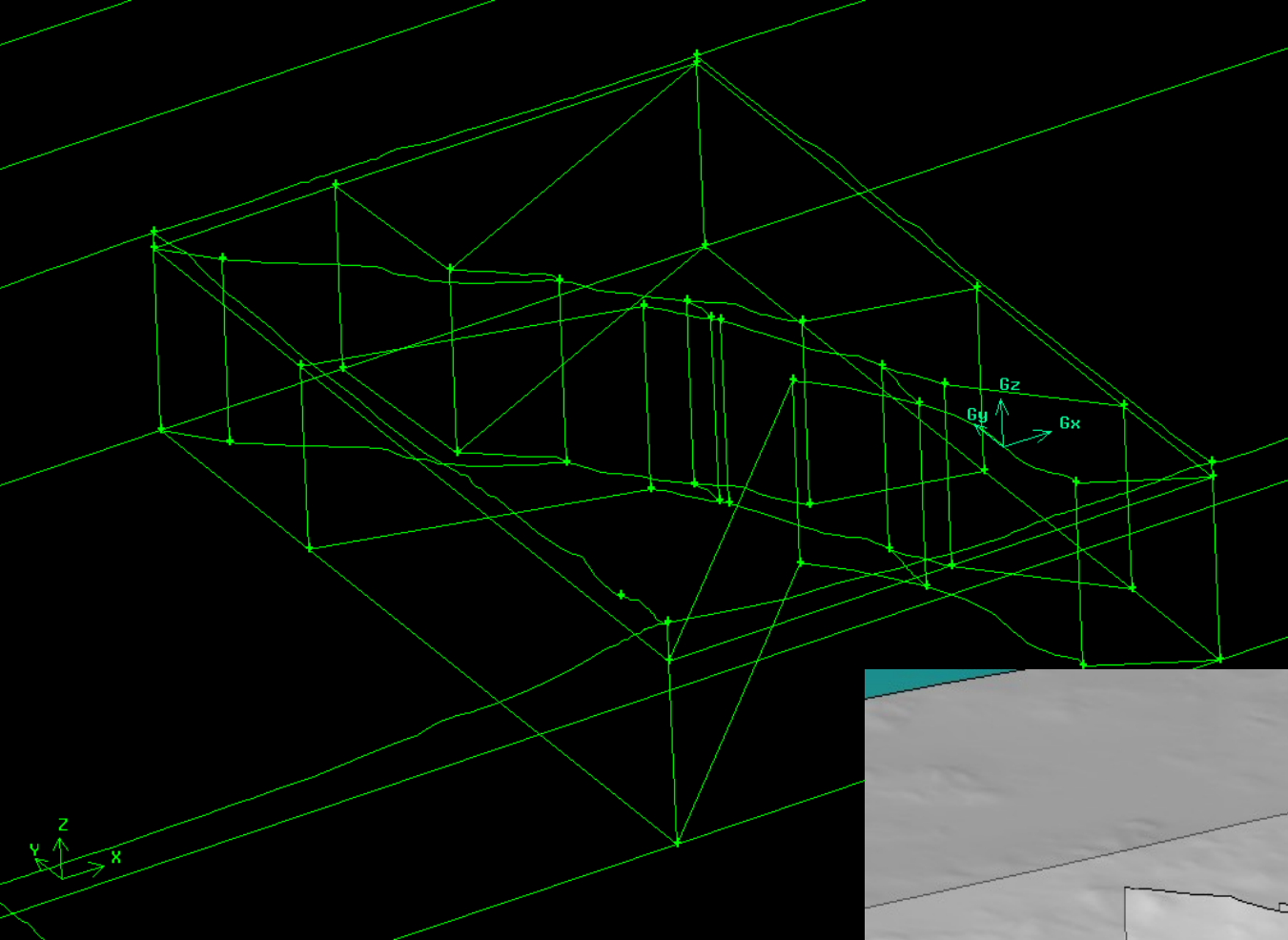


Two faces. At the intersection there are two edges overlapping.
= assembly

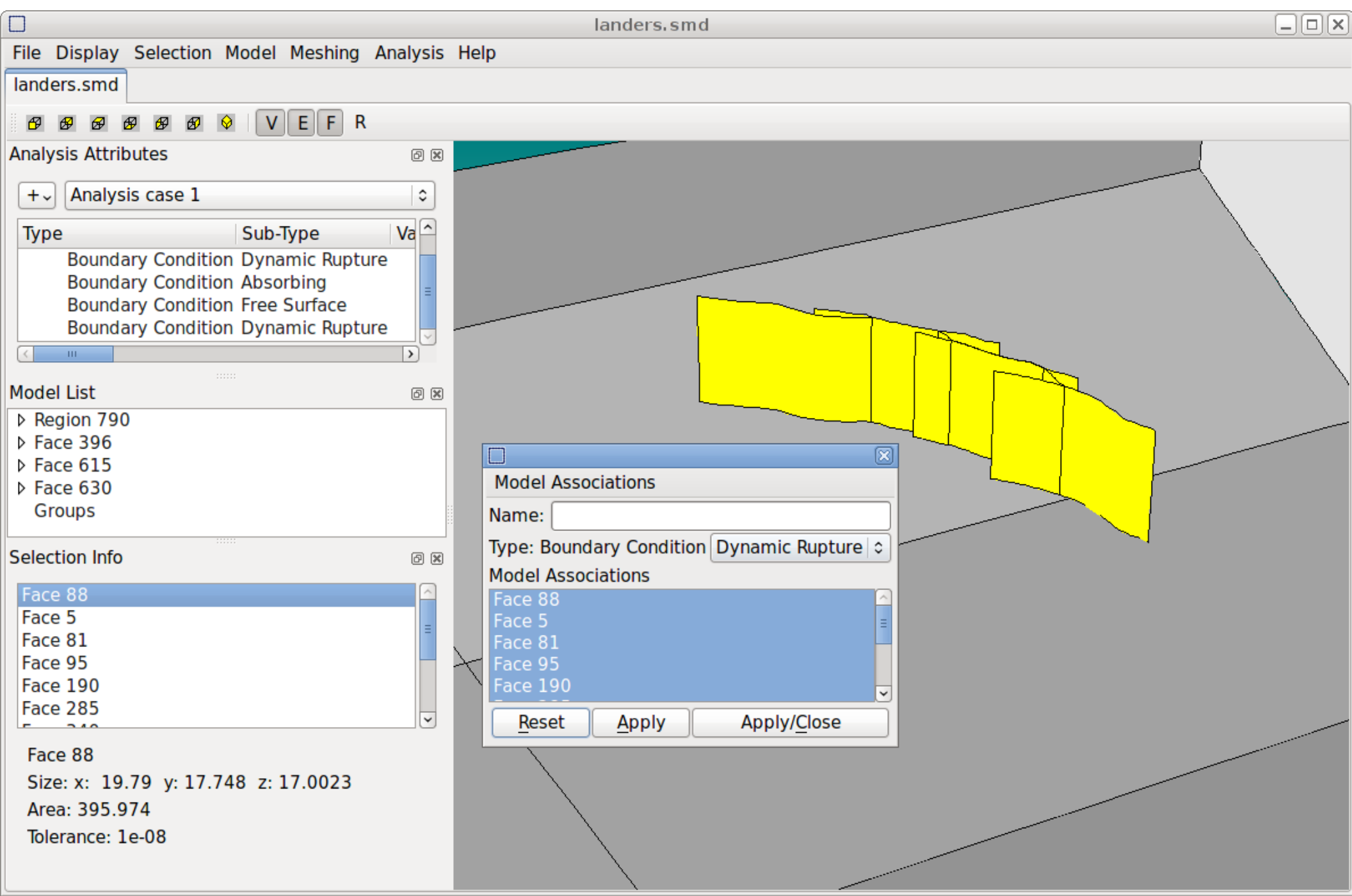


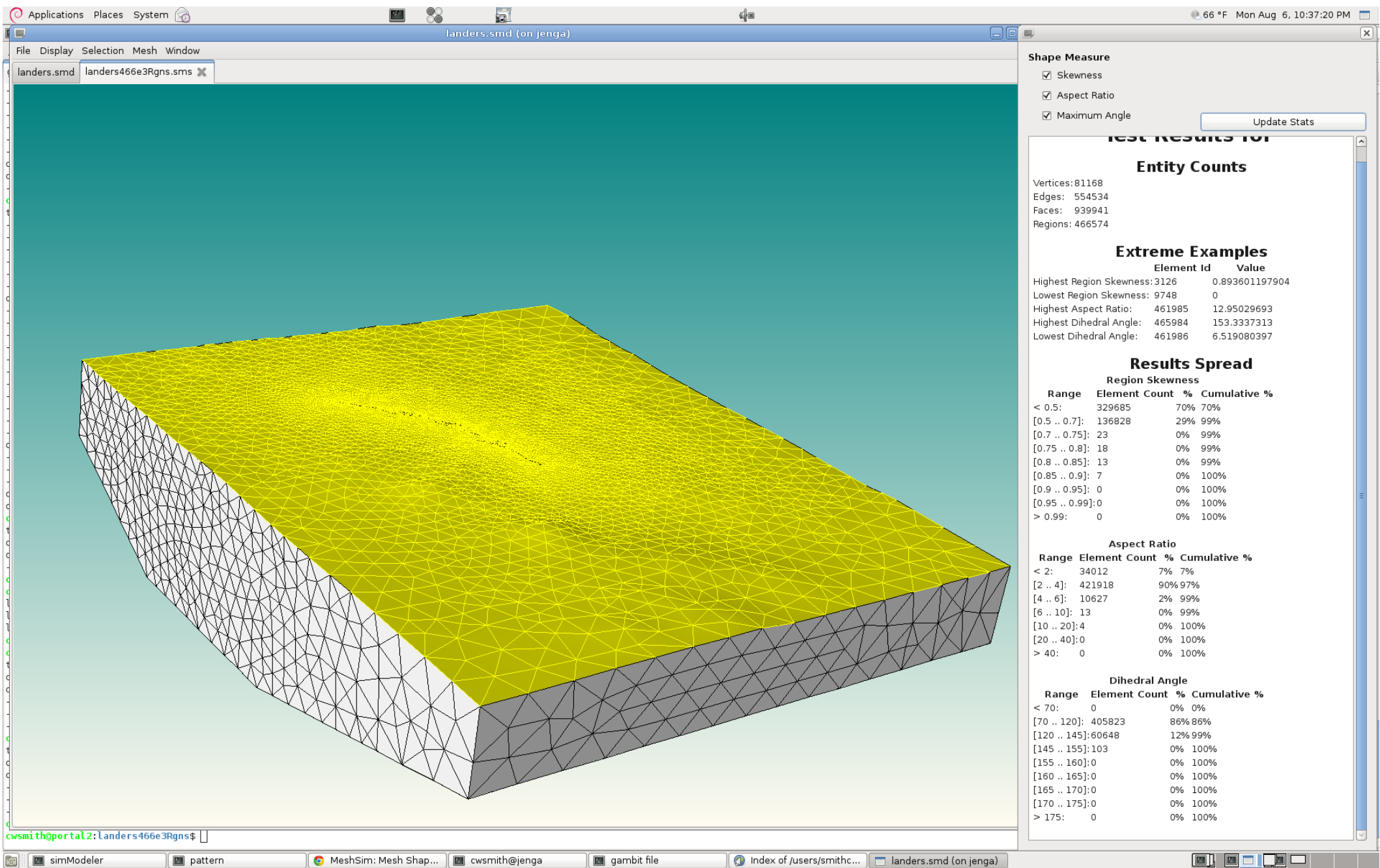
Two faces. At the intersection there is one shared edge.
= non-manifold

Gambit vs SimModeler



SimModeler





Shape Measure

- ☒ Skewness
- ☒ Aspect Ratio
- ☒ Maximum Angle

Update Stats

TEST RESULTS FOR

Entity Counts

Vertices: 81168
Edges: 554534
Faces: 939941
Regions: 466574

Extreme Examples

	Element Id	Value
Highest Region Skewness:	3126	0.893601197904
Lowest Region Skewness:	9748	0
Highest Aspect Ratio:	461985	12.95029693
Highest Dihedral Angle:	465984	153.3337313
Lowest Dihedral Angle:	461986	6.519080397

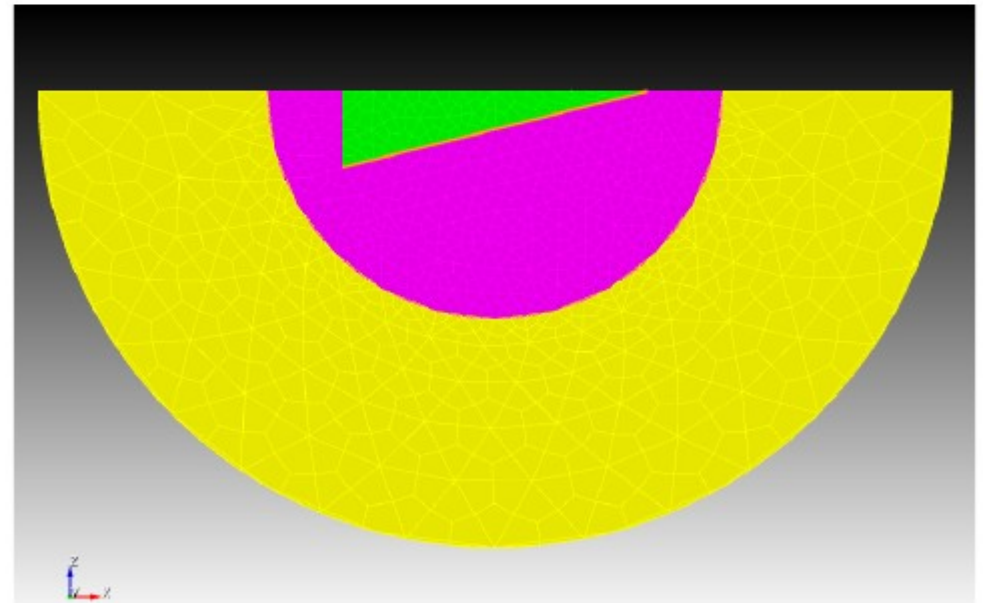
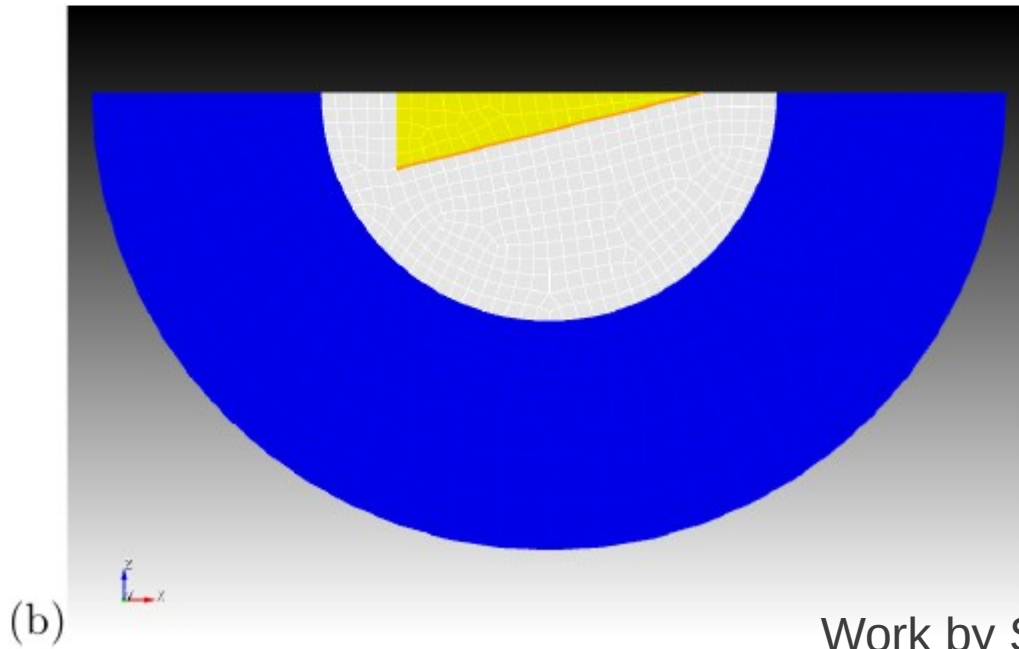
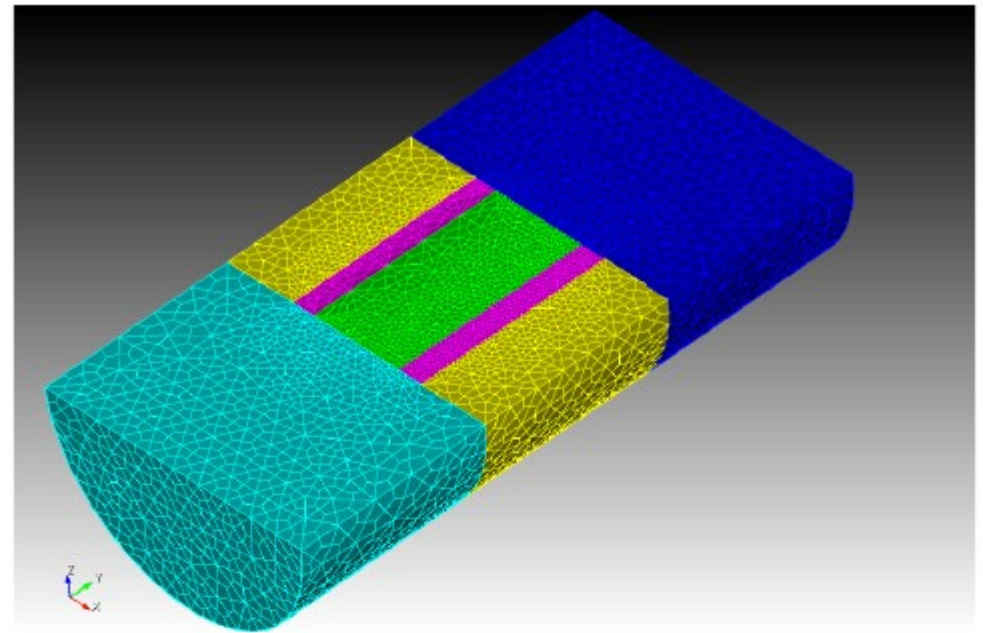
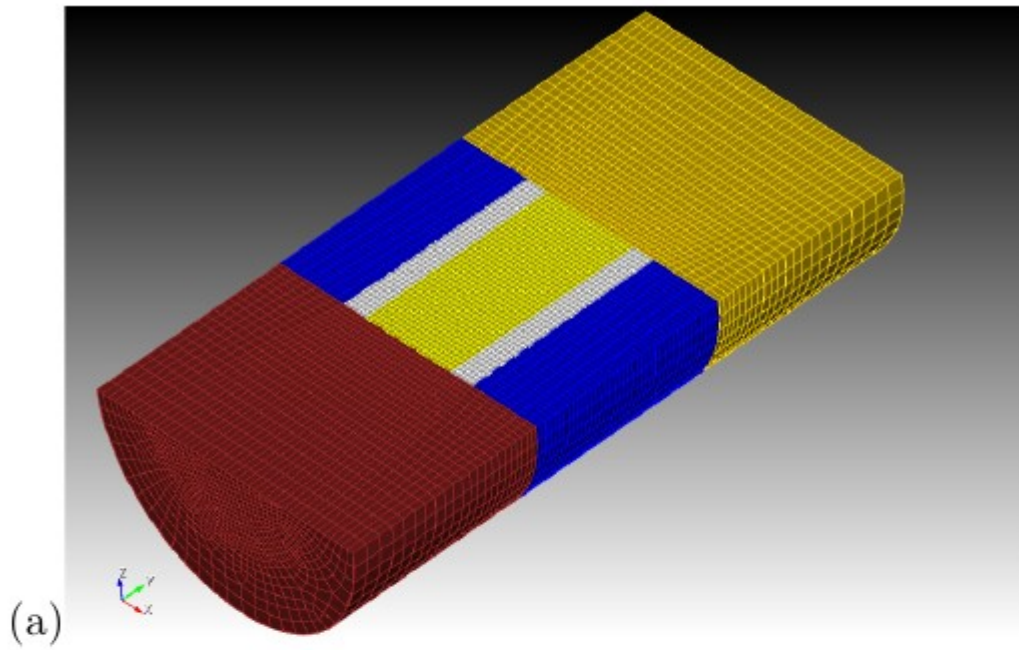
Results Spread

Region Skewness			
Range	Element Count	%	Cumulative %
< 0.5:	329685	70%	70%
[0.5 .. 0.7]:	136828	29%	99%
[0.7 .. 0.75]:	23	0%	99%
[0.75 .. 0.8]:	18	0%	99%
[0.8 .. 0.85]:	13	0%	99%
[0.85 .. 0.9]:	7	0%	100%
[0.9 .. 0.95]:	0	0%	100%
[0.95 .. 0.99]:	0	0%	100%
> 0.99:	0	0%	100%

Aspect Ratio			
Range	Element Count	%	Cumulative %
< 2:	34012	7%	7%
[2 .. 4]:	421918	90%	97%
[4 .. 6]:	10627	2%	99%
[6 .. 10]:	13	0%	99%
[10 .. 20]:	4	0%	100%
[20 .. 40]:	0	0%	100%
> 40:	0	0%	100%

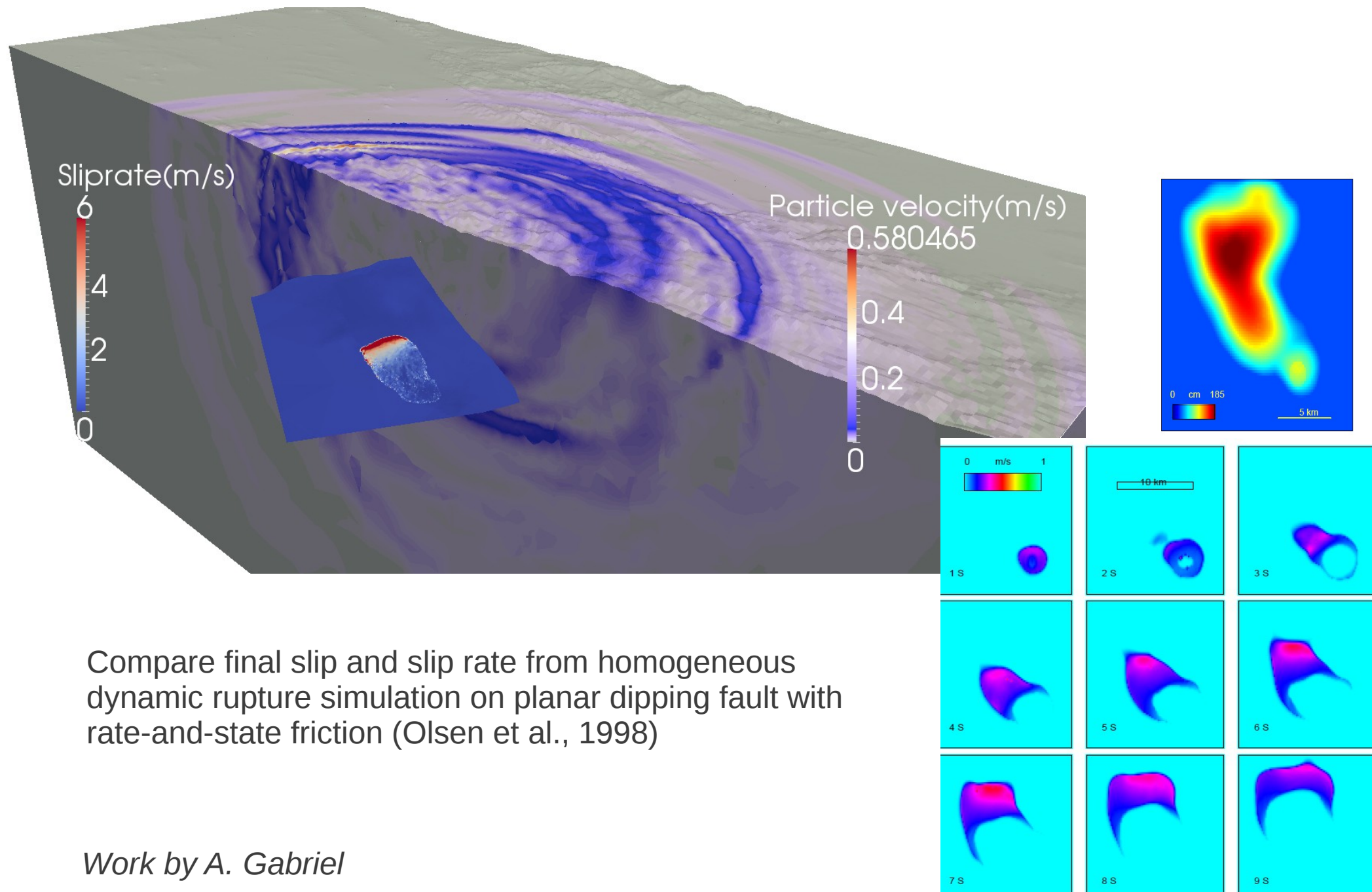
Dihedral Angle			
Range	Element Count	%	Cumulative %
< 70:	0	0%	0%
[70 .. 120]:	405823	86%	86%
[120 .. 145]:	60648	12%	99%
[145 .. 155]:	103	0%	100%
[155 .. 160]:	0	0%	100%
[160 .. 165]:	0	0%	100%
[165 .. 170]:	0	0%	100%
[170 .. 175]:	0	0%	100%
> 175:	0	0%	100%

Thex approach



Work by Surendra Nadh Somala and Jean-Paul Ampuero

Example – The Mw 6.7 1994 Northridge earthquake



Conclusion & Outlook

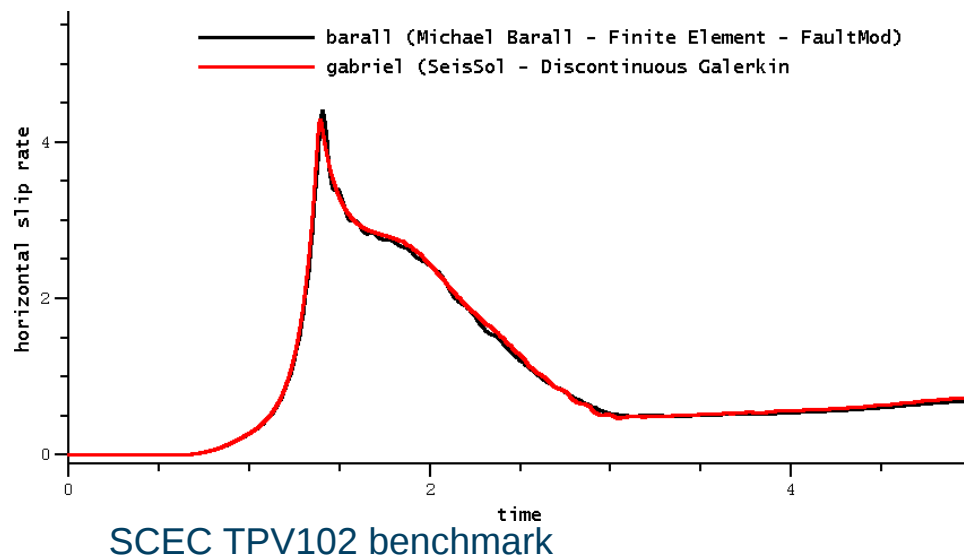
- ADER-DG solver ready, functional and benchmarked
- Bring all features into production version (under construction)
- Combine dynamic rupture with local time stepping
- Current bottleneck CAD generation (under construction)
- Use CAD for quality control
- Open Source (soon), already available through <http://verce.eu/>

<http://seissol.geophysik.uni-muenchen.de/>

Failure criterion

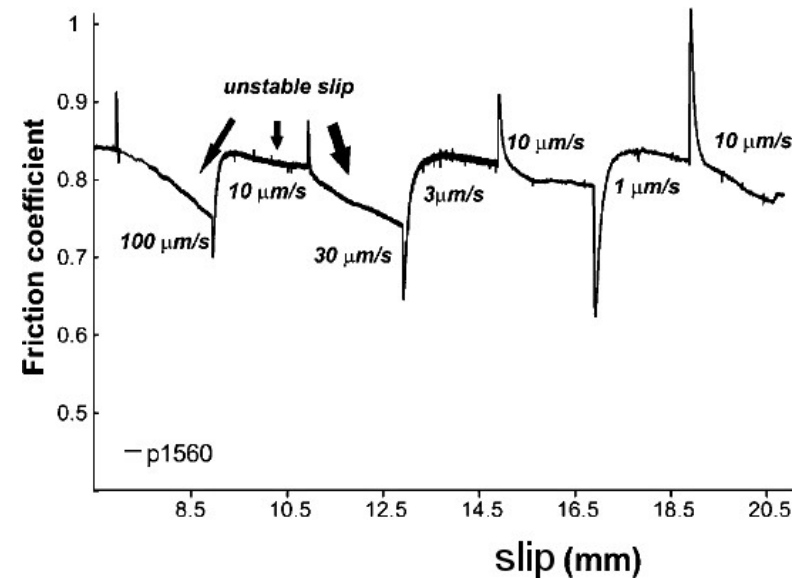
Implementation of rate-and-state friction

- Updating scheme includes Newton-Raphson search for slip rate and two iterations for state variable (Kaneko et al., 2008)



Rate-and-state dependent friction

Velocity-stepping experiment of Niemeijer et al. (2010)



$$\mu_f = \mu_0 + a \ln \frac{v}{v_0} + b \ln \frac{v_0 \theta}{D_c}$$

$$\dot{\theta} = 1 - \frac{v \theta}{D_c}$$

θ state variable

a direct effect

b evolution effect

v_0 steady-state reference velocity

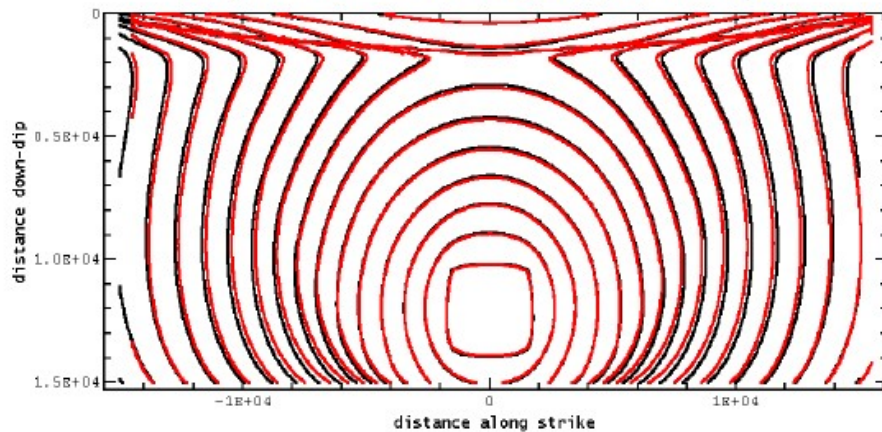
μ_0 steady-state reference friction

Dipping fault geometry

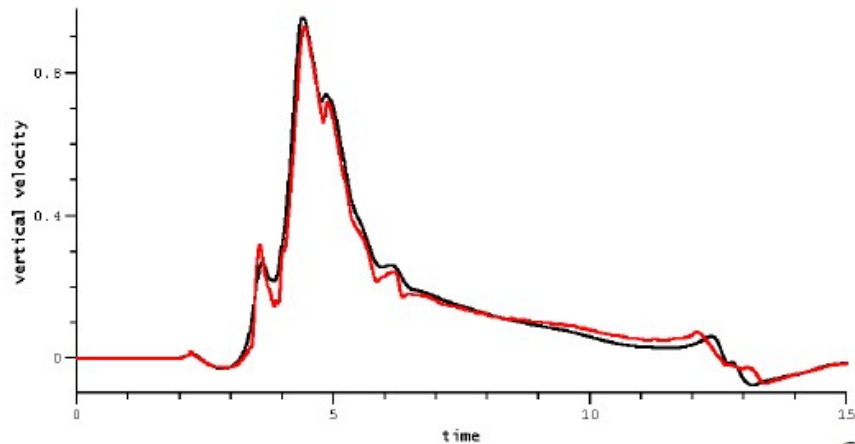
(SCEC Test Cases **TPV10** and **TPV11**)

- 60 degree dipping normal fault geometry
- Initial stress linearly depth dependent
- **Subshear** / supershear rupture conditions

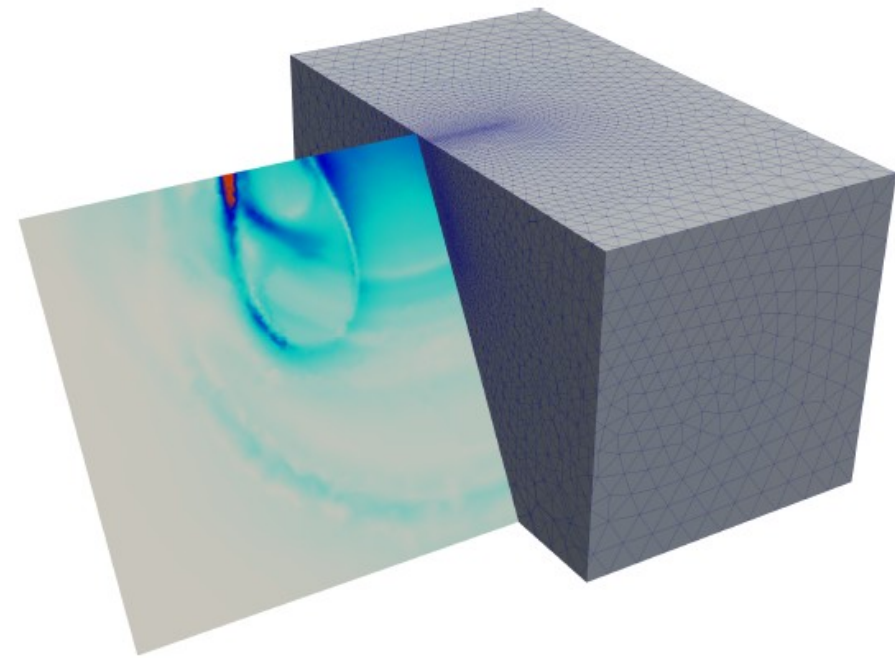
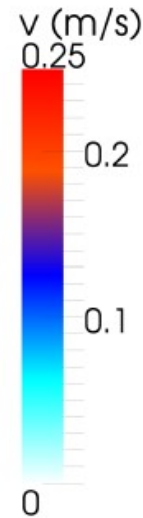
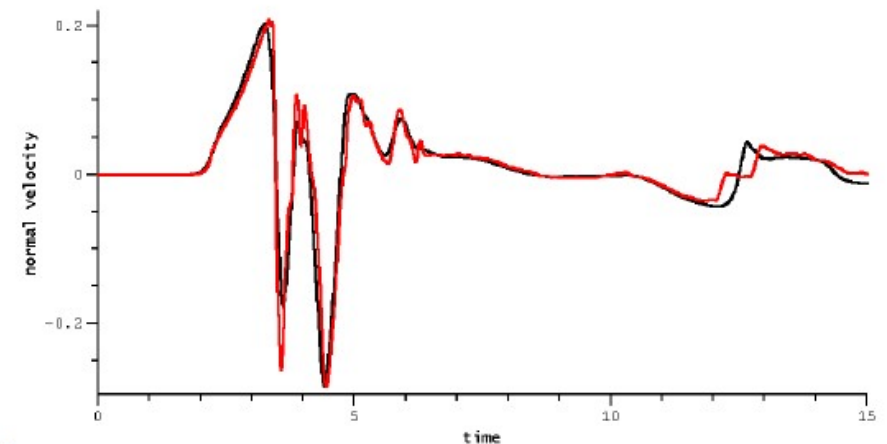
Rupture time – contour plot (each 0.5 s)



— barall (Michael Barall – Finite Element – FaultMod)
— gabriel (SeisSol – Discontinuous Galerkin (element wise))



*Off- fault station
(body 1.0 km, strike 0.0 km, depth 0.0 km)*

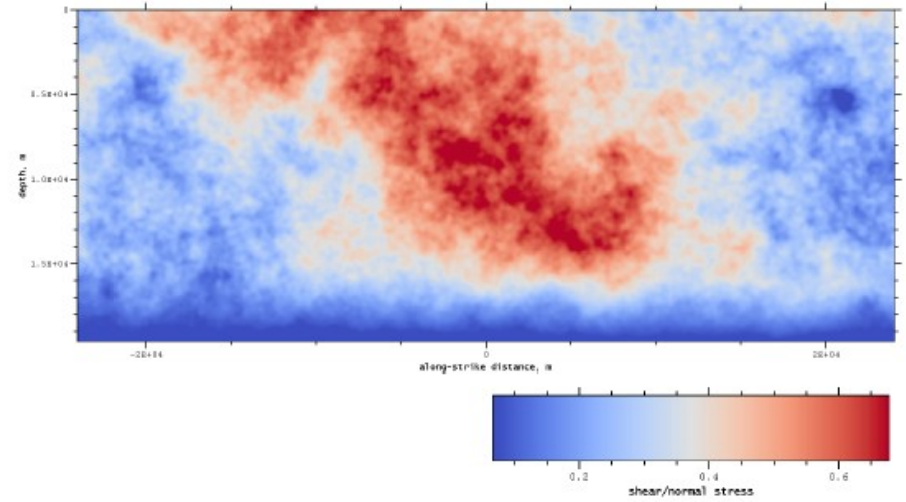


*Mesh geometry, computational domain and
particle velocity on the fault plane after ~9.6 s*

Heterogeneous background stress

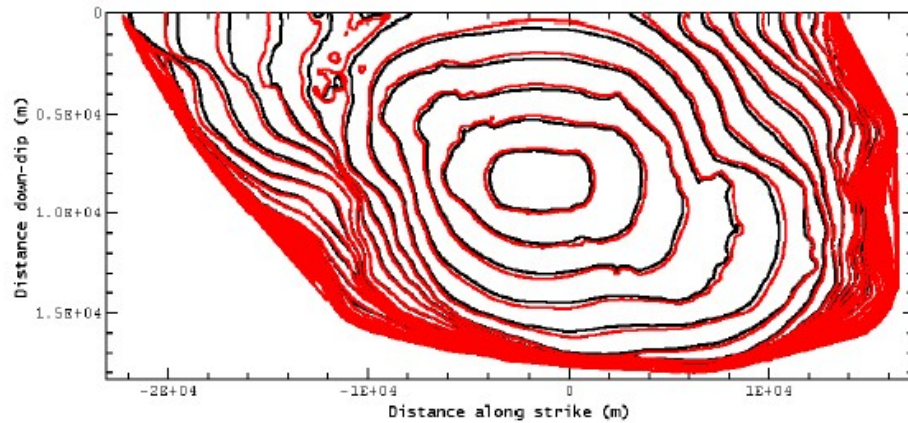
(SCEC Test Cases TPV16 and TPV17)

- Vertical strike-slip fault
- Randomly-generated heterogeneous initial stress conditions
- Trilinear interpolation to map background values on irregular distributed integration points

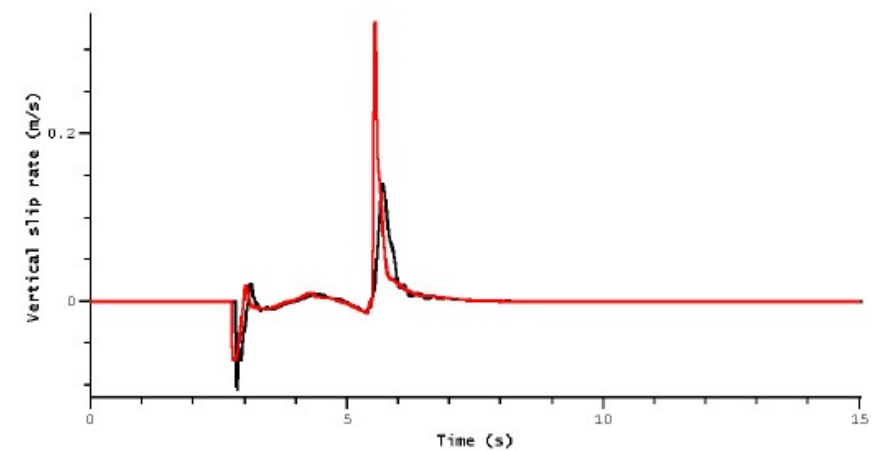
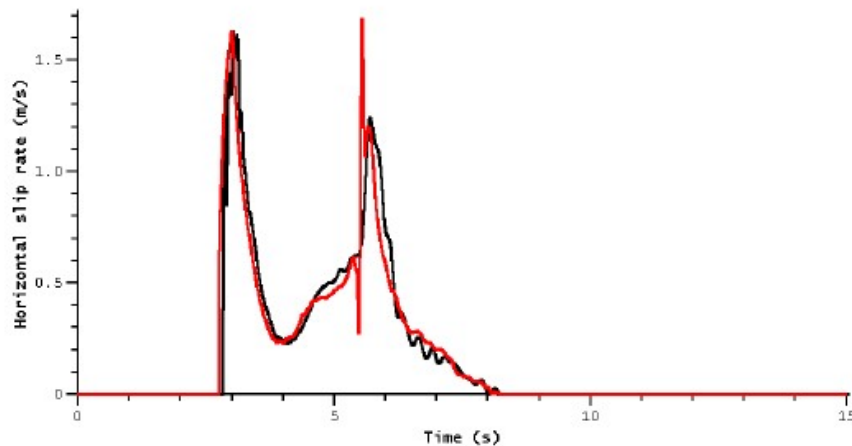


Initial shear stress on the fault plane

Rupture time – contour plot (each 0.5 s)



— barall (Michael Barall - Finite Element - FaultMod)
— pelties (Christian Pelties - Discontinuous Galerkin (GP wise))

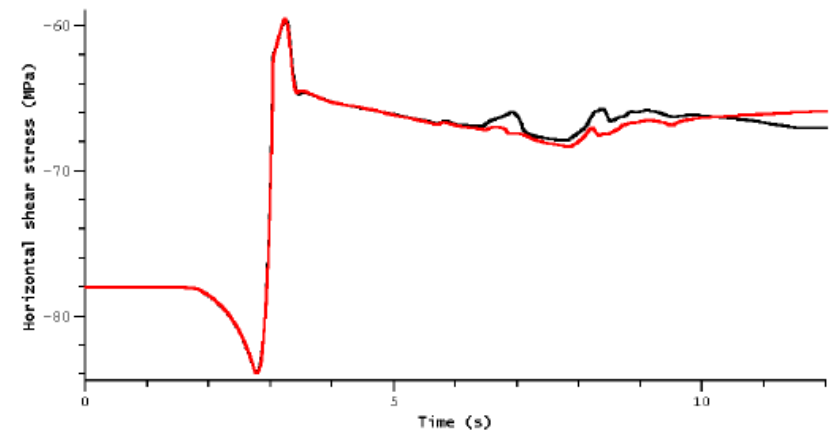
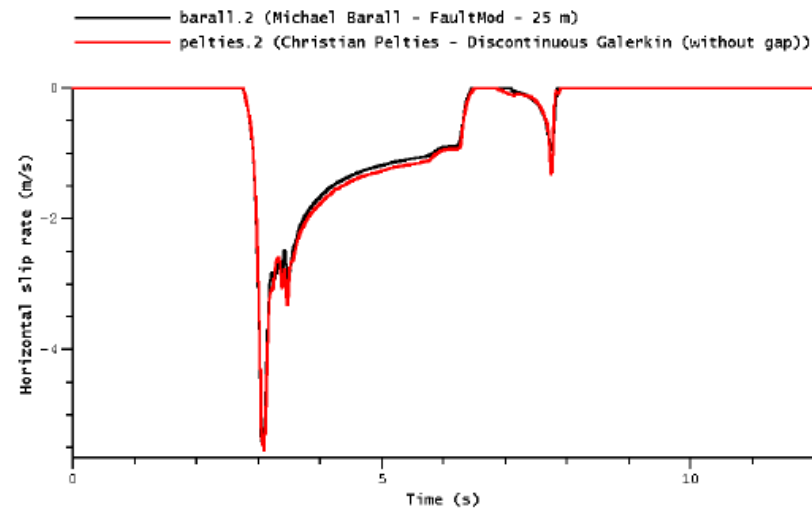
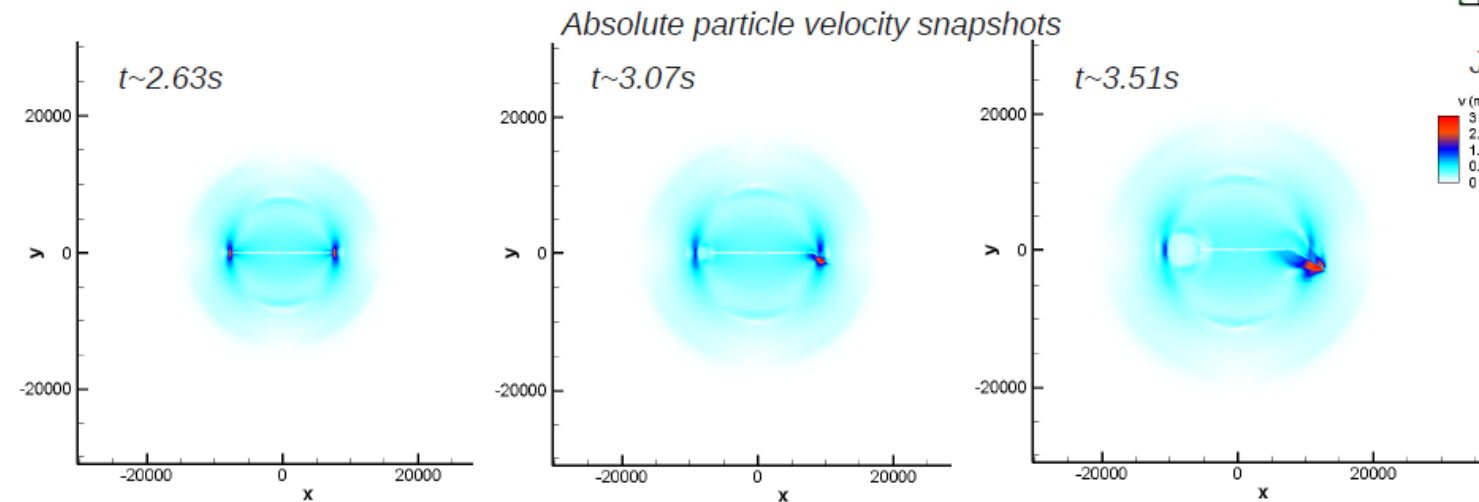
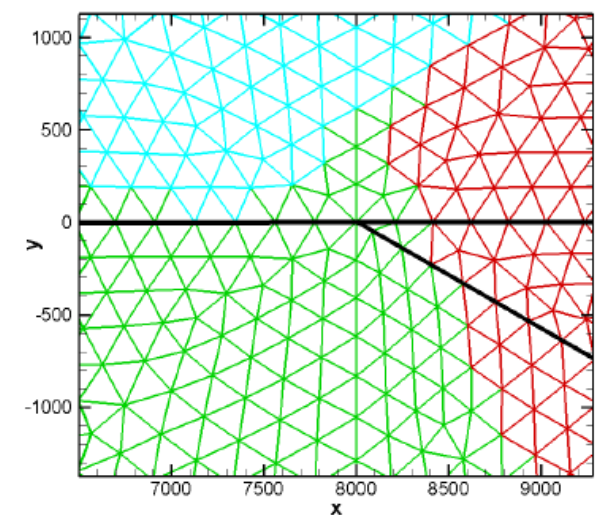


*On- fault station
(strike -9.0 km, dip 9.0 km)*

Fault branching geometry

(2D SCEC Test Cases TPV14 and **TPV15**)

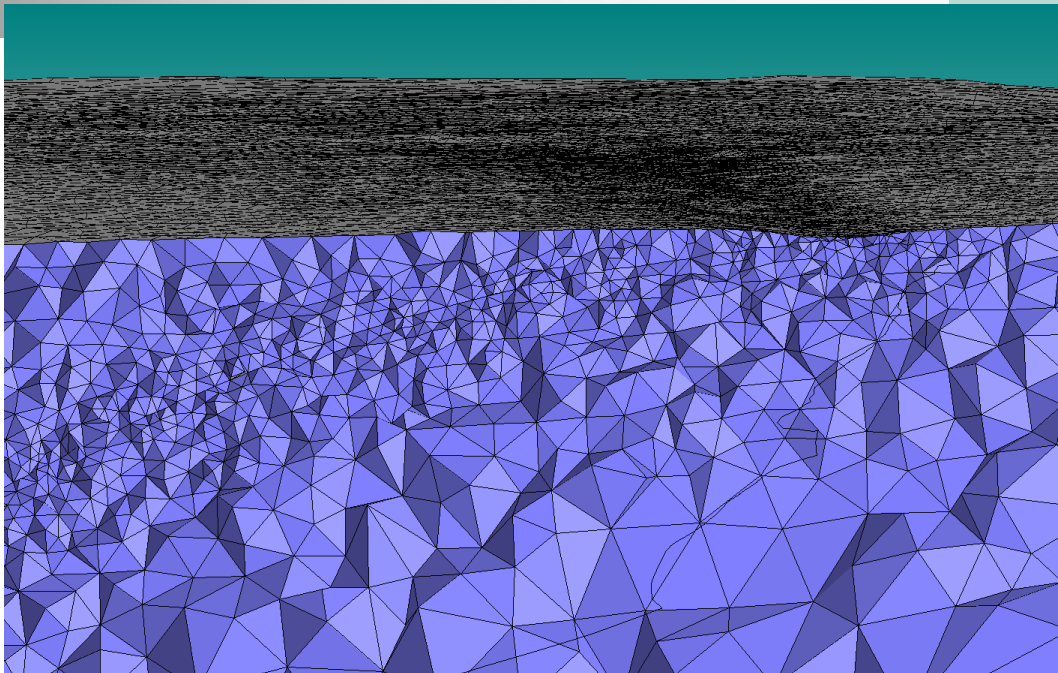
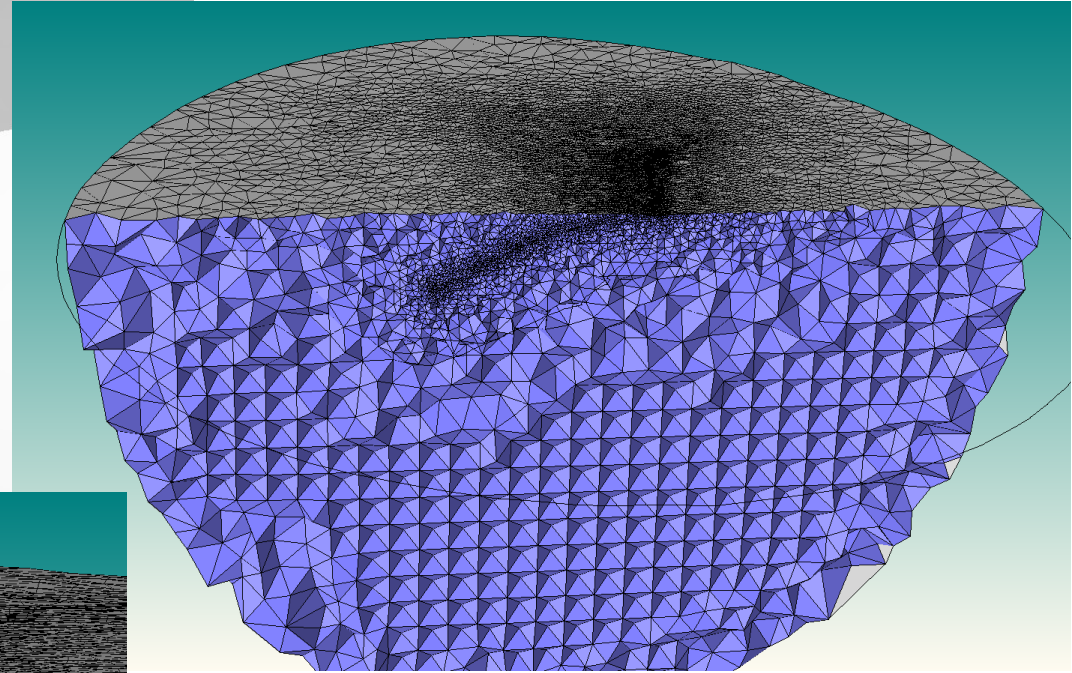
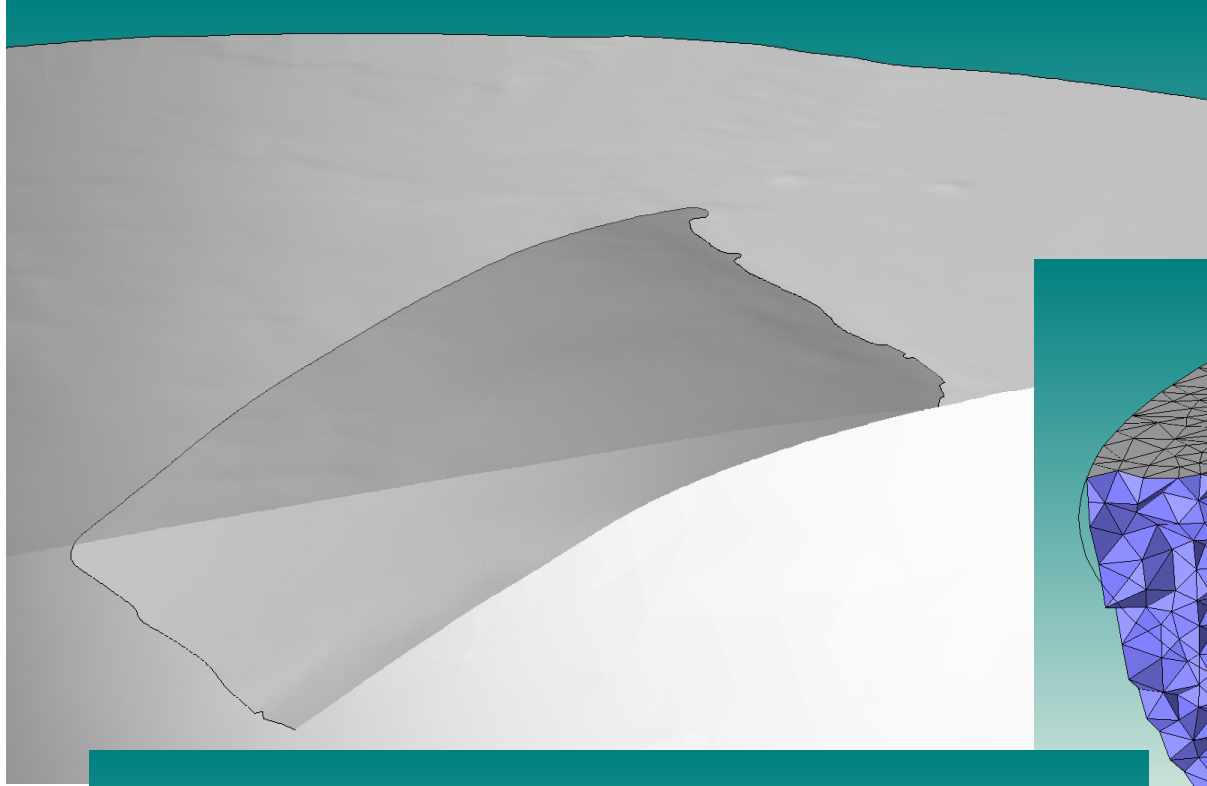
- Left-lateral, vertical, strike-slip fault with a rightward branch forming a 30 degree angle
- Slightly stress-heterogeneous
- High resolution required



On- fault station
(branch, strike 2.0 km, dip 7.5 km)

By A. NERGER

Tohoku



- CAD generation difficult
- Extremely shallow angle at trench
- Skewed elements